

MiNO Marine, LLC 4615 S. Carrollton Ave. New Orleans, LA 70119 504.218.8162 (voice) 877.674.3450 (fax)



## **1** Contents

2	ABBREVIATIONS & DEFINITIONS	
3	REFERENCES	
4	VESSEL CHARACTERISTICS	
- 5	GENERAL	
	<ul><li>5.1 PURPOSE</li><li>5.2 SUPPLEMENT TO OTHER DOCUMENTATION</li></ul>	
-	5.3 CHAIN OF COMMAND	
-	DESIGN AND OPERATIONAL LIMITS	
6		
	6.1 DRAFT	
	6.2 AIR GAP	
	6.3 WAVE HEIGHT & WIND LIMITS	
	6.4 CURRENT	
	6.5 LEG PENETRATION	
	6.6 TOWING AND ANCHORING	
	6.7 TEMPERATURE	
	6.8 MANNING REQUIREMENTS	
	6.9 SOIL CHARACTERISTICS	
	6.10 CATHODIC PROTECTION	
	6.11 INSPECTING THE LEGS AND PADS	
	<ul> <li>6.12 GLOBAL ELEVATED STRENGTH</li> <li>6.13 NAVIGATIONAL DRAFT AND DRAFT MARKS</li> </ul>	
c		
7	GUIDANCE ON OPERATING THE VESSEL	
7	7.1 Changing Modes	
7	7.2 JACKING/PRELOADING CRITERIA	
7	7.3 PRELOADING INSTRUCTIONS	
7	7.4 JACKING UP	
7	7.5 PUNCH THROUGH PROCEDURE	
7	7.6 LCG AND TCG WHILE ELEVATED:	
7	7.7 JACKING DOWN	
7	7.8 JETTING SYSTEM	
7	7.9 RECEIVING VESSELS ALONGSIDE	
8	PREPARING THE VESSEL FOR HEAVY WEATHER	
8	8.1 WEATHER MONITORING	
8	8.2 WHEN HEAVY WEATHER IS FORECAST	
9	PROCEDURES FOR DISCOVERING THE FLOODIN	NG OF A LEG
9	9.1 GENERAL DISCUSSION CONCERNING EXCESSIVE LIST	OR HEEL
10		
1	10.2 GENERAL STABILITY DISCUSSION	
-	10.3 STABILITY LOADING FORM INSTRUCTIONS	
	10.4 Hydrostatic Properties	
	10.4 TANK AND VOID CAPACITY TABLES (SEE ALSO APPEN	
	· ·	(DIX 5)
	IU O NUTALLOWABLE VERSUS MEAN DRAFT UTRVE	
1	<ul> <li>10.6 KG ALLOWABLE VERSUS MEAN DRAFT CURVE</li> <li>10.7 SAMPLE AFLOAT LOADING CONDITIONS</li> </ul>	

1	10.9 DOWNFLOODING POINTS	83
11	CRANE CAPACITY TABLES	84
12	TANK SOUNDING TABLES	
1	12.1 TANK SOUNDING TABLES ARE PROVIDED AS APPENDIX A.	
13	LOCATION OF STORED DANGEROUS SUBSTANCES	
14		95
15		
1	<ul> <li>15.1 THE FIRE CONTROL PLAN IS PROVIDED IN APPENDIX C.</li> <li>15.2 THE SAFETY PLAN IS PROVIDED IN APPENDIX D.</li> </ul>	96
	15.3 INNER JOINER DOORS	96
	LIST OF SHUTDOWN LOCATIONS	
	<ul> <li>16.1 SHUTDOWN APPLIANCE TABLE</li> <li>16.2 GUIDANCE ON RESTARTING AFTER SHUTDOWNS</li> </ul>	
17	DEWATERING AND BALLASTING	
- /	17.1 General	99
-	17.2 BILGE SYSTEM DESCRIPTION & OPERATING GUIDANCE	100
1	17.3 BALLAST SYSTEM DESCRIPTION AND OPERATING GUIDANCE.	
18		
-	<ul> <li>18.1 General</li></ul>	
19		
20		
	20.1       General         20.2       Maximum Take-Off Weight Restrictions	
	20.3 Helideck Operations	
21	EVACUATING & EMBARKATION/DISEMBARKATION PROCEDURES	
2	21.1 General	109
22	ALARMS AND MONITORING	
	22.1 FIRE ALARM	
_	22.2 GENERAL ALARM	
23	EXEMPTION REQUESTS	
23	LIGHTSHIP MONITORING PROCEDURE AND RECORD	
	24.1 GENERAL	
25		
8	25.1 GENERAL	

1/12/2024

### APPENDICES

Appendix A: Tank Tables **Appendix B: General Arrangements** Appendix C: Fire Plan Appendix D: Safety Plan Appendix E: Bilge, Ballast and Fire Piping System Drawing Appendix F: Electrical System Diagram Including Emergency Power Appendix G: Machinery Arrangement Appendix H: Fills, Vents and Sounds Appendix I: Damage Control Plan Appendix J: Tank Plan Appendix K: Letter to the Marshall Islands 0722-MI-001 & Response Appendix L: Letter to the Marshall Islands 0722-MI-002 & Response Appendix M: Letter to the Marshall Islands 0722-MI-003 & Response Appendix N: Letter to the Marshall Islands 0722-MI-004 & Response Appendix O: Letter to the Marshall Islands 0722-MI-006 and Response Appendix P: Trimmed Ballast Tank Tables

# Figures & Tables

Table 4.1. Vessel Description	
Table 4-1: Vessel Description	
Table 4-2: Principal Dimensions         Table 4-3: Lightship Characteristics Including Legs & Pads	
Table 4-4: Aggregate Mass Properties of Legs and Pads         Table 4-5: Florested Liebtship Mass Properties*	9
Table 4-5: Elevated Lightship Mass Properties*         Table 4 Guine Characteristics	
Table 4-6: Load Line Characteristics         Table 4-7: Jacking System Capacities*	
Table 4-8: Crane 1 Characteristics         Table 4-9: Crane 2 Characteristics	
Table 4-9: Crane 2 Characteristics	
Table 4-11: Personnel Capacities	
Table 4-11: Deck Cargo Capacities*	
Table 4-13: Tank Capacities       Table 4.12: Classification and December Compliance	
Table 4-12: Classification and Regulatory Compliance	
Table 4-15: Tonnage Characteristics	
Table 4-16: Mooring Loads	
Table 4-17: Helideck Characteristics	
Table 4-19: Maximum Leg Tower Reaction Forces*	
Table 4-20: Pad Max Capacities*	
Table 4-21: Motion Study Parameters (All Transit Cases)*	12
Figure 6-1: Aft Draft Marks Arrangement	23
Figure 7-1: Preload Reaction Curve	29
Figure 7-2: Elevated Weight Worksheet	
Figure 7-2: Elevated Weight Sample Calculation	
Table 10-1: Hydrostatic Properties	
Table 10-2: Tank Capacity Table	
Table 10-3: Void Capacity Table	
Figure 10-1: ABS Allowable KG Curves	54
Table 10-4: ABS Allowable KG Values	54
Figure 10-2: ABS Allowable KG Curves with Loading Conditions	
Figure 10-3: ABS Allowable KG Curves	
Table 16-1: Shutdown Appliance Locations	98
Figure 17-1: Hold Plan	
Table 18-1: Propulsion Main Equipment	
Figure 18-1: Worst-Case DP Capability Plot with Legs Retracted	
Figure 18-2: Worst-Case DP Capability Plot with Legs Extended	
Table 21-1: Typical Helicopter Dimensions	106
Table 24-1: Light ship data alterations log	114
Table 24-2: Light Ship Alterations Survey Form	
Figure 25-1: Hold Plan	
Figure 25-2: Double Bottom Plan	

## 2 Abbreviations & Definitions

- ABL Above the molded baseline
- AP Aft Perpendicular (Frame 52)
- BL Baseline vertical reference point located on a plane that passes through the deepest molded point on the hull (top of bottom shell plate)
- CL Longitudinal centerline of the vessel
- cm centimeter. 1 cm = 1/100 m
- Displacement Weight of the vessel in a specific condition of loading
- Deadweight the variable load of the vessel including, but not limited to, liquid loads, deck cargo, personnel, personal effects, stores, and spare parts. The displacement of the vessel minus the lightship weight equals the deadweight.
- FO Fuel Oil at 0.867 specific gravity
- FP Forward Perpendicular (Frame 0)
- FSC Free Surface Correction
- FSM Free Surface Moment
- ft feet
- FW Fresh Water at 1.000 specific gravity
- GAL Gallon
- HO Hydraulic Oil at 0.890 specific gravity
- KIPS Unit of weight, 1 kip equals 1000 lbs
- KG Vertical Center of Gravity above Baseline (also VCG)
- KMt Transverse Metacenter above the Molded Baseline
- kN –kilonewton (unit of force), 1 kN = 0.102 tonnes
- L Liter. 1 L = 0.2642 Gallons
- lbs pounds
- LCG Longitudinal Center of Gravity aft of the FP
- LCF Longitudinal Center of Floatation, measure aft of the FP
- Lightship the vessel complete in all respects without the variable loads

1/12/2024

- LO Lube Oil at 0.910 specific gravity
- LT Long Tons. 1 LT = 2,240 lbs.
- m Meter. 1m = 3.28 feet
- MT metric ton. 1 MT = 1000 kilograms = 9.81 kN = 1.016 Long Tons
- Molded Draft draft to the baseline of the hull. All references to draft in this manual refer to the molded draft of the hull unless noted otherwise.
- Navigational Draft draft measured to the bottom of the azimuthing thruster (0.87 meters below the molded baseline) with the legs fully retracted
- SG Specific Gravity of a liquid compared to the density of Fresh Water; SG = (Density of Liquid)/(Density of Fresh Water)
- ST Short Tons. 1 ST = 2000 lbs.
- SW Salt Water at 1.025 specific gravity
- Ton Short Ton
- t tonne, or metric ton. 1 t = 1.016 Long Tons. 1 t = 9.81 kN
- TCG Transverse Center of Gravity from CL, + Stbd, Port
- VCG Vertical Center of Gravity above Baseline (also KG)

## **3** References

- [1] MiNO Marine Report 0722-824-001 Motions Study Revision C1
- [2] 0722-ABS-011-Anchor Letter
- [3] DV1P02C03 GE Dynamic Positioning System Operation Manual

# **Detailed Revision History**

- 1. Revision C1
  - a. Revised for 17 gears per leg
- 2. Revision C2
  - a. Added Section 17.1.4 referencing Ballast Water Management Plan (BWMP)
- 3. Revision C3
  - a. Added additional loading conditions to the Afloat Operations Section
  - b. Update Afloat Stability
  - c. Added Leg Strength Cases from the Saudi Aramco VL Guidance Memo
  - d. Updated Hydrostatic Properties Table
    - i. Convert from Moment to Trim 0.01 deg to MT1mm in Hydrostatic Table
    - ii. Convert from Moment to Heel 0.01 deg to MH1mm in Hydrostatic Table
  - e. Specify maximum leg penetration, See Section 6.5
  - f. Include instructions for when to liberating the pads, See Section 6.3.3
  - g. Include helideck operations guidance.
  - h. Provide additional trimmed tank tables for ballast tanks, See Appendix P
  - i. Update Preload Curve to include 709 MT Variable Load
- 4. Revision C4
  - a. Revised maximum Leg Penetration from 10m to 15m in Section 6.5
- 5. Revision C5
  - a. Updated lightship for Asry Weight Control Report dated 21-10-2022
  - b. Included adjustment for additional gear on each leg

## 4 Vessel Characteristics

Principal characteristics and capabilities of the FALCON DIAMOND are provided in Tables 4-1 through 4-21.

Table 4-1: Vessel Description	
Name	FALCON DIAMOND
IMO Number	9769623
Flag	Marshall Islands
Туре	Mobile Offshore Unit - SEU
Builder	Triyards Holdings Limited
Designer	MiNO Marine, LLC
Keel Lay Date	December 9, 2014

Table 4-2: Principal Dimensions	
Length Overall (LOA) with Helideck	90 m
Length Overall (LOA) Hull	64.3 m
Load Line Length (L)	59.611 m
Breadth Overall	40.2 m
Breadth Molded	39.6 m
Depth Molded, Baseline to Main Deck	4.6 m
Leg Length	92.5 m
Pad Length x Width x Depth	13.6x7.8x1.8 m

### Table 4-3: Lightship Characteristics Including Legs & Pads

Lightship Displacement	5870.87 t
VCG ABL (Legs Raised)	20.11 m
LCG Aft of FP	28.00 m
TCG from CL (+ STBD / - PORT)	-0.50 m

Lightship characteristics assume legs are raised and cranes are in stowed positions. There is no permanent ballast installed onboard the vessel.

Table 4-4: Aggregate Mass Properties of Legs and Pad
--

Weight of Legs and Pads		2,153.24 t
VCG ABL (Legs Raised)	39.54	<del>39.45</del> m
LCG Aft of FP		30.60 m
TCG from CL (+ STBD / - PORT)		0.00 m

#### Table 4-5: Elevated Lightship Mass Properties\*

Tuble 4 5. Elevated Eghtship Muss Properties		
Lightship Weight of Vessel Excluding Legs and Pads	3717.63 t	
VCG ABL	8.86 m	
LCG Aft of FP 26.	49 <del>26.</del> m	
TCG from CL (+ STBD / - PORT) -0.7	<sup>/8</sup> <del>-0.75</del> m	

\*Elevated weight excludes weight of legs and Pads.

Variable load must be added to Elevated Lightship weight to determine total elevated weight.

1/12/2024

#### **Table 4-6: Load Line Characteristics**

Summer Load Line Draft, Molded ABL	3.576 m <sup>+</sup>
Load Line Displacement (Salt Water)	7,602 t
Deadweight at Load Line Draft (Afloat)	1,742 t
Maximum Variable Load (Elevated) *	454 t

\* Maximum variable load while elevated is limited to 454 t or less depending on water depth and prevailing wave height. Hook load when making heavy lifts is in addition to this 454 t.

Additional variable load with maximum of 709 t is possible with limiting water depth and wave height. See Section 6.3.8 for more information.

+ Maximum hull draft. Navigational draft is to bottom of stern thrusters (0.87 m below hull baseline).

Table 4-7: Jacking System Capacities\*

#### NOTE: THE JACKING SYSTEM CAPACITY IS THE GOVERNING LIMIT FOR ELEVATED OPERATIONS (SEE SECTION 6.11).

Maximum Jacking Rating	73.781 t/pinion
Maximum Holding Rating	86.736 t/pinion
Maximum Storm Rating	110.858 t/pinion
Number of Gears Installed	68 (17 per leg)
Total Normal Jacking Capacity	5,017 t <sup>+</sup>
Normal Jacking Capacity Per Leg	1,254 t (12,297 kN)
Total Normal Jacking Capacity with 8% Friction Margin	4,615 t
Total Normal Holding Capacity	5,898 t
Normal Holding Capacity Per Leg	1,474 t (14,456 kN)
Total Storm Capacity	7,538 t
Storm Capacity Per Leg	1,884 t (18,476 kN)

\* ABS Rules require redundancy in the event of failure of a single jacking system component. Therefore, if a jacking gear fails, elevated loads, whether jacking or holding, must be adjusted, if required, such that the per pinion ratings are not exceeded. + This value is a maximum allowable; the elevated load during jacking is to be less than the jacking capacity with friction.

#### Table 4-8: Crane 1 Characteristics

Crane Model	Nautilus Model 1000B
Boom Type	Fixed
Capacity	181.44 t
Radius (max)	42.7 m
Certification	API 2C 7 <sup>th</sup> Edition

#### Table 4-9: Crane 2 Characteristics

Crane Model	Nautilus Model 340BT-70/100	
Boom Type	Telescoping	
Capacity	54.4 t (retracted), 41.2 t (extended)	
Radius (max)	21.3 m to 30.4 m	
Certification	API 2C 7 <sup>th</sup> Edition	

#### Table 4-10: Crane 3 Characteristics

Crane Model	Nautilus Model 180B-70	
Boom Type	Fixed	
Capacity	22.6 t	
Radius (max)	21.3 m	
Certification	API 2C 7 <sup>th</sup> Edition	

### Table 4-11: Personnel Capacities

Maximum Persons Onboard	150: 30 Crew, 120 PIAC	
See manning certificates for more information.		

Table 4-11: Deck Cargo Capacities*			
Open Deck Area	1,000 m <sup>2</sup>		
Maximum Cargo Deck Loading (Main Deck, Aft of Frame 25)	5 t/m²		
Maximum Deck Loading (Exposed Main Deck, Fwd of Frame 25)	2.5 t/ m <sup>2</sup>		
Maximum Deck Loading (Enclosed Main Deck, Fwd of Frame 5)	2.5 t/ m <sup>2</sup>		
Maximum Deck Loading (Other Enclosed Main Deck, Focsle Dk)	1.5 t/ m <sup>2</sup>		
* Dock common should not be stowed directly adjacent to the incline towers			

\* Deck cargo should not be stowed directly adjacent to the jacking towers.

#### Table 4-13: Tank Capacities

Fuel Oil	320,400 L		
Fresh Water	278,800 L		
Zero Discharge Tankage	245,300 L		
Ballast	1,444,440 L		

See Appendix A for more details

### Table 4-12: Classification and Regulatory Compliance

American Bureau of Shipping	★A1, SEU, ★AMS, ★DPS-2, ★AMS ACCU,
	Restricted Service
Republic of the Marshall Islands	Mobile Offshore Unit – Self-elevating
IMO	2009 MODU 2010 Edition, MARPOL
Helideck	CAP 437 7 <sup>th</sup> Edition without refueling capabilities

### Table 4-15: Tonnage Characteristics

International Gross Tons	5271
International Net Tons	1581

### Table 4-16: Mooring Loads

Nabrico DF-490 Cast Steel Chock	25.4 t
Nabrico DF-40A Double Bitt w/ Horns	25.4 t
Nabrico DF-489 Cast Steel Open Chock	25.4 t
Fabricated Double Bitt (12" SCH 120, mooring)	25.4 t

#### **Table 4-17: Helideck Characteristics**

M	aximum D-value	22.2 m
M	aximum Takeoff Weight (Elevated)	12,600 kg
M	aximum Takeoff Weight (Afloat)	11,000 kg

\*See Section 20 for additional details about helicopter weight restrictions in the elevated and afloat modes

#### Table 4-19: Maximum Leg Tower Reaction Forces\*

Type of Force	Operational (Elevated) <sup>+</sup>	Transit (Pitch)
Max Axial Reaction	18,580 kN	7,439 kN
Max Upper Guide Reaction	9,433 kN	4,931 kN
Max Lower Guide Reaction	10,706 kN	6,575 kN

\* Data extracted from MiNO Marine Leg Strength Analysis report included in full in Appendix I to this manual. **+ Be advised that jacking system capacity is the governing limit for elevated operations (see Section 6.11).** 

Table 4-20: Pad	Max Capacities*
-----------------	-----------------

Vertical Reaction	19,568 kN <sup>+</sup>	
Design Moment	66,023 kN-m	

\* Data extracted from MiNO Marine Structural Analysis Technical Report included in full in Appendix J to this manual. **+** Be advised that jacking system capacity is the governing limit for elevated operations (see Section 6.11).

Table 4-21. Notion Study Parameters (All Transit Cases)					
Analysis Method	Frequency Domain with 3d Diffraction				
Sea Spectra	JONSWAP				
Wave Height (Significant)	2.0 m				
Mean Wave Periods	4-16 seconds; 2 second increments				
Wave Headings	180-0 Degrees; 45 degree increments				
Wind Speed	50 knots				
Maximum Vessel Displacement	7,662 t (3.6m draft)				
Vessel Forward Speed	0, 4, & 6 knots				
Leg Position	Fully Retracted (Pad bottom at Baseline)				

### Table 4-21: Motion Study Parameters (All Transit Cases)\*

\* Data extracted from MiNO Marine Motions Study (Reference [1])

## **5** General

## 5.1 Purpose

- 5.1.1 (2009 IMO MODU Code, 2010 Edition, Chapter 14) This manual has been prepared to assist the Master in the following areas:
  - The evaluation of the vessel loading conditions with respect to the required stability and anticipated environmental conditions. Operating instructions and restrictions must be followed at all times. There are Vessel Loading Forms included in this booklet to be used to determine if the vessel's displacement, center of gravity and draft are adequate to meet the required stability criteria. An Excel workbook has been provided to the vessel as an aid for the completion of these calculations. These forms calculations must be completed and documented using the forms or the approved Excel workbook provided and the stability of the vessel evaluated any time the loading of the vessel changes, such as due to a significant change in liquid loads or deck cargo.
  - Provide guidance to the operating personnel related to the following:
    - Deck cargo loading
    - Preparing the vessel for heavy weather
    - Operation when changing modes
    - Determination of flooding of the legs or pads
    - Dewatering
    - Helideck operations
    - Evacuating procedures
  - Provide general description of the vessel, including design limits with respect to environmental conditions and mode of operation.
  - Provide information and locations of:
    - Access, compartment boundaries, and watertight and weathertight closing devices
    - Emergency shutdowns
    - Flooding and jacking alarm systems
    - Fire detection and alarm systems
    - Compartment and deck access

## 5.2 Supplement to Other Documentation

- 5.2.1 This manual is intended to supplement existing documentation for the vessel operation, including, but not limited to:
  - Vessel and Company Policies, Regulations and Procedures
  - Applicable flag state and operating country laws, and international rules and regulations, including MODU and MARPOL requirements
  - Vessel Specific approved plans such as Fire Fighting and other required plans
  - Responsibilities and Duties associated with required crew licenses

## 5.3 Chain Of Command

- 5.3.1 The chain of command is detailed in the Seacor Safety Management System (SMS) Manual for the FALCON DIAMOND as follows:
  - Ship's Captain/Master SMS Chapter 5; Master's Responsibility and Authority
  - Ship's Marine Crew SMS Chapter 6; Resources and Personnel
  - Liftboat Specific Crew SMS Chapter 6; Liftboat Specific

## 6 Design and Operational Limits

## 6.1 Draft

6.1.1 The maximum allowable draft of the vessel is the assigned load line draft. The vessel shall not exceed this draft in any condition of loading while underway. In addition, at any loading condition and associated draft encountered during the voyage when the vessel is afloat, the applicable stability requirements, as detailed in this manual, must be met. Note the stern thrusters extend 0.87 m below the baseline of the vessel and are to be considered when determining navigational draft (see Section 6.12).

## 6.2 Air Gap

- 6.2.1 For normal operations the minimum air gap should be at a distance above the mean water level such that there are no wave encounters (wave slap) on the hull bottom. See Section 6.3.4 of this manual for air gap guidance when heavy weather is anticipated.
- 6.3 Wave Height & Wind Limits

Afloat – Seas shall be less than 2 meters (significant wave height) and wind less than 50 knots 6.3.1 when the vessel is in the intact condition. The legs should be fully retracted during normal transit moves. While 2 meters is a general guide on maximum wave height for vessel survivability, normal working conditions are 1.8 m seas. The Master must be aware that seas consisting of smaller waves could be worse in terms of vessel responses, particularly leg whipping in roll or pitch. This is because the vessel is sensitive to both the height of waves and their period. The vessel's heading relative to prevailing seas and the vessel's speed also affect the vessel's response. The Master must consider all these factors when operating afloat and deciding whether or not it is prudent to slow down or stop and elevate until more favorable conditions for transit prevail. For this vessel, maximum pitch response, and thus maximum forward/aft leg whipping, will likely occur at wave periods in the range of 3 to 5 seconds. Similarly, maximum roll response, and thus maximum port/starboard leg whipping, will likely occur at wave periods in the range of 7 to 9 seconds. These are approximate period ranges only and depend on other factors previously cited. As a general guide, if the vessel's roll and/or pitch response while operating in any given sea approaches 4 to 6 degrees of pitch or roll, then adverse leg whipping is probably occurring and the Master should alter relative heading, speed, or stop and elevate until the adverse conditions have subsided. It is the Master's primary responsibility to ensure safe navigation of the vessel to safeguard personnel, transported cargo, the vessel and the environment. Stop Work Authority must be used when there is a potential of an adverse effect, regardless of wave height or wind speed.

The MiNO Marine Motions Study report (Reference [1]) showing the maximum allowable transit condition is based on the vessel afloat with legs fully retracted, with a 6 degree maximum roll/pitch angle at the vessel's natural roll/pitch period.

Stability calculations have been performed which demonstrate that if loaded in accordance with Section 10, the vessel will stay afloat with any single watertight compartment flooded or under emergency conditions, provided that seas are minimal and winds are less than or equal to 50 knots.

- 6.3.2 Changing Modes Seas shall be 2 meters or less (significant wave height) when changing modes and the same guidance in Section 6.3.1 applies. Moreover, the Master must also consider the potential of the pads slamming on the sea floor when tagging the pads, or lowering the legs into position in preparation for tagging. The Master must also consider sea floor conditions when assessing the potential damaging effects of pad slamming.
- 6.3.3 Liberating the Pads The vessel is equipped with a pad jetting system allowing jetting of each pad to assist with pad liberation. Uplift on each pad is required in order to liberate the pads and an uplift force of no more than 1,200 kN is recommended. Jetting may be used along with uplift at the Master's discretion. See Section 7.8 for jetting operation guidance.
- 6.3.4 Elevated Cases Reviewed by ABS Refer to the Leg Strength Cases Summary table in Section
  6.3.7 which summarizes the design cases reviewed by ABS. Referring to that letter, Cases 1
  through 6 represent maximum design conditions where the vessel is elevated in 50-70 kt winds,
  2 kts current, and up to 10 meter waves depending on water depth, with the cranes in their
  stowed positions. Maximum variable load in these cases is 454 t.

Cases 7 and 8 represent maximum design conditions with the primary crane lifting 181 tonnes at the most adverse slew angle, and with an additional 454 tonnes VL onboard. Maximum wave height is 2 meters with 35 kt winds. See Appendix I for more details.

Cases 9 and 10 represent maximum design survival in safe harbor conditions with all cranes stowed, 454 tonnes variable load onboard the vessel, and with the vessel subjected to 100 kt winds with 2 kts current. Safe harbor water depth is 30 meters (including storm surge) or less. The maximum wave height is 10 meters. See Appendix I for more details.

Case 11 represents the maximum preload case which is derived from the loads encountered when the vessel is in 70 m of water, with 454 tonnes of variable load onboard.

Cases 12 and 13 represent conditions with all cranes stowed, 709 tonnes variable load onboard the vessel, and with the vessel subjected to 50 kt winds with 2 kts current. Water depth is 46 meters or less. The maximum wave height is 10 meters.

Cases 14 and 15 represent maximum design survival in safe harbor conditions with all cranes stowed, 709 tonnes variable load onboard the vessel, and with the vessel subjected to 100 kt winds with 2 kts current. Water depth is 30 meters or less. The maximum wave height is 10 meters.

A summary table of the elevated load cases is presented in Section 6.3.8.

In all of the cases described above, the elevated center of gravity (LCG and TCG) must be near the center of the leg rectangle. Weights onboard should be adjusted to achieve an elevated weight TCG near centerline. If the loading condition of the vessel results in an elevated weight LCG forward of the leg center, refer to Section 6.3.6.

- 6.3.5 Elevated in Survival Condition In winds up to 100 knots, the vessel should find safe refuge in 30 m of water (including storm surge) or less and elevate to an air gap sufficiently above the wave tops so as to avoid waves slapping the bottom of the vessel, including hull appendages such as the z-drives or skegs. Storm surge should be monitored, and air gap adjusted accordingly. Air gap should not exceed 9 meters above the mean water level. When the LCG of the elevated weight is between 27.m and 30.6m aft of Frame 0 and the TCG is near centerline, the maximum allowable wave height in these conditions is 10 m. Maximum allowable variable load in this condition is 454 t. Refer to Cases 9 and 10 in the ABS Review Letter included in Appendix I.
- 6.3.6 Crane Operation Cranes cannot be operated while afloat. Crane manufacturer limits applicable to the type of lift being conducted must be observed. The appropriate load chart given the type of lift and weather conditions must be used. Refer to Sections 6.3.3 and 7.5 of this manual for more requirements governing crane operations. SEACOR Marine management should be consulted prior to engaging in unusual lifting operations.
- 6.3.7 Elevated LCG In most loading conditions, the elevated LCG will be forward of the leg center. The elevated weight LCG shall be between 27.2m and 30.6m aft of Frame 0.
  In water depths greater than 60m, the location of the LCG may result in a reduced allowable maximum wave height limit from 10m to 7m. See section 7.5 for further details.
  For water depths or forecast wave heights not mentioned, consult SEACOR Marine management concerning appropriate operational limits.

## 6.3.8 Leg Strength Cases Summary Chart

	Elevated Mode - Operating									
				Operating - I	No Crane Use				Operating with Crane	
Design Load Case	Case 1A	Case 1B	Case 1C	Case 2	Case 3	Case 4	Case 5	Case 6	Case 7	Case 8
Water Depth w/ Surge (m)	70	70	60	70	40	40	70	70	70	70
Maximum Wave Height (m)	10	7	10	10	10	10	6.25	6	2	2
Associate Wave Period (s)	7 to 14	7 to 14	7 to 14	7 to 14	7 to 14	7 to 14	7 to 14	7 to 14	7 to 14	7 to 14
Wind Velocity (knots)	50	50	50	50	50	50	70	70	35	35
Surface Current (knots)	2	2	2	2	2	2	2	2	2	2
Bottom Current (knots)	2	2	2	2	2	2	2	2	2	2
Air Gap (m)	7.5	7.5	7.5	7.5	9	9	7.5	7.5	7.5	7.5
Leg Penetration (m)	3	3	3	3	3	3	3	3	3	3
Variable Load (MT)	454	454	454	454	454	454	454	454	454	454
Leg & Pad Weight (MT)	2153	2153	2153	2153	2153	2153	2153	2153	2153	2153
Estimated Lightship minus L&P (MT)	3698	3698	3698	3698	3698	3698	3698	3698	3698	3698
Total Elevated Load (MT)	4152	4152	4152	4152	4152	4152	4152	4152	4333*	4333*
Max Pad Fixity Conditions -(ft-kips/rad x 10^6)	1.5	1.5	1.5	Pinned	1.5	Pinned	1.5	Pinned	1.5	Pinned
P-delta	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Dynamic Amplification	Yes	Yes	Yes	No	Yes	No	Yes	No	Yes	No
Significant Wave Height (m)	5.56	3.89	5.56		1		3.47			
Modal Wave Period (s)	7.21	7.21	7.21		6		6.53			
LCG (m aft of F0)	30.6	27.2	27.2	30.6	30.6	30.6	30.6	30.6	30.6	30.6

	]	Elevated Mode - Survival/Preload		97	Additional Variable Load				
<u>.</u>			Severe Storm		Preload	Operating - No Crane Use		Severe	e Storm
	Design Load Case	Case 9A	Case 9B	Case 10	Case 11	Case 12	Case 13	Case 14	Case 15
	Water Depth w/Surge (m)	30	30	30	70	46	46	30	30
	Maximum Wave Height (m)	10	10	10	0	10	10	10	10
	Associate Wave Period (s)	7 to 14	7 to 14	7 to 14	7 to 14	7 to 14	7 to 14	7 to 14	7 to 14
	Wind Velocity (knots)	100	100	100	0	50	50	100	100
	Surface Current (knots)	2	2	2	0	2	2	2	2
	Bottom Current (knots)	2	2	2	0	2	2	2	2
	Air Gap (m)	9	9	9	9	7.5	7.5	7.5	7.5
	Leg Penetration (m)	3	3	3	3	3	3	3	3
	Variable Load (MT)	454	454	454	454	709	709	709	709
	Leg & Pad Weight (MT)	2153	2153	2153	2153	2153	2153	2153	2153
	Estimated Lightship minus L&P (MT)	3698	3698	3698	3698	3698	3698	3698	3698
	Total Elevated Load (MT)	4152	4152	4152	4152	4407	4407	4407	4407
Max	x Pad Fixity Conditions -(ft-kips/rad x 10^6)	1.5	1.5	Pinned	Pinned	1.5	Pinned	1.5	Pinned
	P-delta	Yes	Yes	Yes	No	Yes	Yes	Yes	Yes
	Dynamic Amplification	Yes	Yes	No	No	Yes	No	Yes	No
	Significant Wave Height (m)				1	1			
	Modal Wave Period (s)				-	I			
	LCG (m aft of F0)	30.6	27.2	30.6	30.6	28.7	28.7	28.7	28.7
8	S								
S Mil	NO Marine, LLC								

## 6.4 Current

- 6.4.1 The maximum current considered while elevated in 50 kts wind is 2 knots. In safe harbor subject to 100 knot winds, the maximum current considered is also 2 knots. These currents are based on the worst-case design conditions. For higher currents, consult with Seacor Marine management.
- 6.5 Leg Penetration
- 6.5.1 The vessel has been designed to operate in a variety of soil conditions from soft mud to hard sand. Penetration may vary widely depending on the site's geotechnical characteristics. Penetration up to 15m is allowed.
- 6.6 Towing and Anchoring
- 6.6.1 The vessel is self-propelled; towing is not normally required. If non-emergency towing of the vessel is required, a towing plan shall be developed to suit the requirements of the tow. If an emergency tow is required, refer to Emergency Towing Manual.
- 6.6.2 An anchor is provided for emergency anchoring purposes. Normal mooring of the vessel will be by lowering legs and elevating or by mooring lines from vessel bitts to shore. Limiting factors on mooring by elevating are same as normal elevated environmental limits. The anchoring system is sized to hold the vessel in current of up to 4.86 knots and simultaneous winds up to 48.6 knots. See also Reference [2] "0722-ABS-011-Anchor Letter."

## 6.7 Temperature

- 6.7.1 The minimum air and sea water temperature the vessel may operate in is a lowest mean daily average of 0° C. The maximum air temperature the vessel may operate in is 45° C at 100% relative humidity and 54° C at 45% relative humidity. The maximum sea temperature that the vessel may operate in is 35° C.
- 6.7.2 The vessel is not intended to operate in ice, afloat or elevated.
- 6.7.3 The vessel is intended to operate primarily in warm climates; as defined by the Republic of the Marshall Islands, warm climates are the zone between 30° North and 30° South latitudes.
   Immersion or exposure suits need not be carried when operating in warm climates.

### 6.8 Manning Requirements

6.8.1 The vessel's manning requirements are dependent on Route and are detailed in the vessel's Minimum Safe Manning Certificate.

### 6.9 Soil Characteristics

6.9.1 The soil characteristics used in the ABS approved global leg strength analysis are as follows: undrained soil shear strength at soil surface ranged from 80 psf to 120 psf with shear strength rates of increase with penetration ranging from 46 psf/ft to 50 psf/ft.

## 6.10 Cathodic Protection

- 6.10.1 The vessel is fitted with an Impressed Current Cathodic Protection (ICCP) system which protects the hull from galvanic corrosion. The pads are fitted with anodes to provide similar protection. The ICCP system need not be active when the vessel is elevated as described in this manual.
- 6.10.2 Cathodic potential readings shall be taken periodically from representative positions and evaluated to confirm that the cathodic protection system is operating within design limits.
- 6.10.3 Anodes are to be periodically examined for depletion and if excessive depletion of anodes are found they are to be replaced if found necessary.

## 6.11 Inspecting the Legs and Pads

- 6.11.1 The interior of the leg can be accessed from a watertight hatch at the top. Vertical ladders with platforms at regular intervals provide access throughout the length of the leg. The leg interiors can be inspected during required dry-dockings. Surveying the legs should include a comprehensive visual examination of the structure as well as surface nondestructive examination of critical locations. Special attention should be given to jetting system structures and piping for evidence of cracking or leaks.
- 6.11.2 The exterior of the pad can be inspected to ensure the watertight integrity of the pad. Examinations of the pads can be carried out in conjunction with the examinations of the vessel's bottom. Hull bottom inspections as well as pad inspections can be performed while the vessel is afloat by an approved underwater inspection in lieu of dry-docking. Surveying the pads should include a comprehensive visual examination of the structure as well as surface nondestructive examination of critical locations. Upon completion of the underwater inspection ABS is to be notified confirming the inspection results (i.e. any damage found, extensive areas of corrosion, areas of substantial corrosion, areas of substantial deterioration, or no damages that may or may not affect classification). The pads are fitted with an effective means of corrosion control. Likewise, internal examination requirements are treated similar to inaccessible voids treated with corrosion-inhibiting coatings (float coat). If pad flooding is suspected, drain plugs can be removed from the pad in dry dock to confirm watertightness or presence of fluids.

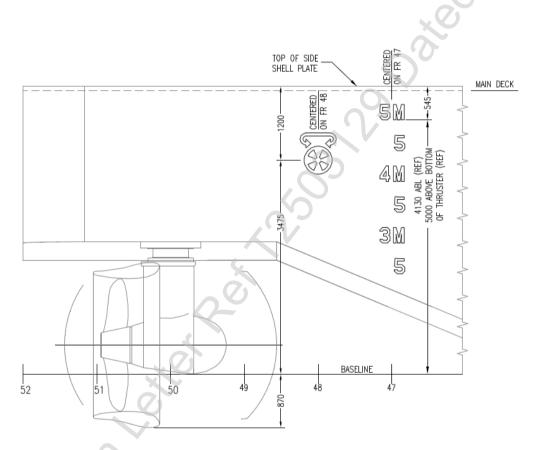
## 6.12 Global Elevated Strength

- 6.12.1 Elevated operations of the vessel are governed by the capacity of the jacking system. The jacking system load monitoring system should be checked regularly to ensure the maximum loads described in Table 4-6 are not exceeded.
- 6.12.2 The design capacity of the hull, legs, and pads are in excess of the capacity of the jacking system and shall <u>NOT</u> be used as limiting loads for elevated operations.

## 6.13 Navigational Draft and Draft Marks

6.13.1 The stern thrusters (located at Frame 50) extend 0.87 m below the baseline of the hull and shall be considered in determining the navigational draft of the vessel to determine if water depths are acceptable for afloat operations.

6.13.2 Aft draft marks installed on the vessel are referenced to the bottom of the stern thrusters to assist in determining navigational draft (see drawing 0722-602-001 Hull Markings, excerpt provided below). Instructions for afloat operations that describe how the navigational draft in way of the stern thrusters is calculated are provided in Section 10. The aft draft marks provide accurate navigational drafts to the bottom of the thruster when trim and heel are zero (0). It is the Master's responsibility to ensure water depth is sufficient for afloat operation without risk of the stern thrusters striking bottom.





- 6.13.3 Aft draft marks can be converted to molded hull drafts by subtraction 0.87m from the observed draft.
- 6.13.4 Forward draft marks are located 320mm aft of Frame 4 and are referenced to the baseline of the hull. See drawing 0722-602-001 Hull Markings for further details.

1/12/2024

## 7 Guidance on Operating the Vessel

## 7.1 Changing Modes

### 7.1.1 General

- 7.1.1.1 See Section 6.3.2 for wave height guidance while changing modes.
- 7.1.1.2 All cargo must be secured prior to changing modes. The cranes shall be stowed in their respective cradles when changing modes.
- 7.1.1.3 When changing modes, the vessel shall be in an acceptable loading and watertight condition as required when the vessel is afloat. Temporary submergence of the load line is permitted while preloading.
- 7.1.1.4 At the discretion of the Master, personnel not directly involved in the operation of the vessel when changing modes shall muster in a pre-designated muster area assigned by the Master. All personnel shall be briefed on safety procedures associated with the jacking processes and shall have Flag State approved Personal Floatation Devices (PFD) accessible and ready for use when the vessel is changing modes.
- 7.1.1.5 When moving the vessel, the legs shall be completely raised when practical. The vessel must not be moved until the legs are well clear of the bottom and any obstructions.
- 7.1.1.6 The legs should never be used to stop or slow the vessel's motion and the pads shall never be dragged on the bottom. When in the elevated position (excluding preloading and evaluation phases of jacking), the minimum air gap from the mean water level to the bottom of the vessel's hull plating shall be sufficient to keep the waves from contacting the hull.
- 7.1.1.7 If unusual noises are heard from the legs' rack and pinion assemblies during jacking, stop jacking as soon as safely possible. Determine the cause of the noises before corrective action is taken.
- 7.1.1.8 The Impressed Current Cathodic Protection (ICCP) system should be turned off prior to jacking of the ship.

## 7.2 Jacking/Preloading Criteria

- 7.2.1 Preloading of the vessel, as described using the preloading guidance contained in this section, is required when elevating the vessel in all cases except when the Master determines preloading is not necessary. The Master may determine that preloading is not required when the location is in harbor and anticipated operations and weather conditions do not suggest preloading is required or when the vessel must make an emergency stop during transit to elevate, for example, to avoid leg whipping during excessive wave action during transit. There may be other unforeseen instances where it would be appropriate to not preload when elevated and when in doubt the Master should consult with SEACOR Marine management for appropriate preloading action.
- 7.2.2 There may be cases where site specific assessments and preload requirements for the particular site, expected crane operations, and worst-case weather are other than what are described in the preload instructions provided in this Manual. In such cases the Master should consult with SEACOR Marine management to obtain specific preloading instructions.
- 7.2.3 ABS allowable limits on jacking and holding loads, leg axial reactions, and pad loading should be adhered to when jacking the unit and holding position while elevated. Real-time jacking system loads are reported by the Jacking Control Screen and should be monitored regularly.
- 7.2.4 Preloading the legs and pads is intended to be performed after the vessel's hull is out of the water and has cleared the wave tops, but before jacking to the final elevation. The Master can take on preload ballast if required prior to elevating the vessel, provided the afloat condition complies with the Stability Operating Instructions and provided that the aggregate load being jacked, when jacking commences, adheres to the LCG and TCG guidance explained in Section 7.5 of this Manual. When the vessel is afloat, the Master shall ensure all Stability Operating Instructions, including those concerning slack tanks, are followed at all times. See also 7.1.1.3.

## 7.3 Preloading Instructions

7.3.1 The preload reaction curve presented in Figure 7-1 is suitable for preloading the vessel when anticipated weather is expected to be up to the maximum design conditions for each water depth as described in Sections 6.3.3 and 6.3.4 of this manual. These design conditions include normal operations (wind speeds up to 50 knots), normal lifting operations (wind speeds up to 35 knots), and weathering of a severe storm (winds up to 100 knots).

- 7.3.2 Note that the preload reaction curve reports the required axial reaction in the leg at the lower guide level (tower bottom) and no manual adjustments are required to this reaction curve for water depth, leg/pad weight/buoyancy, etc. In most cases the elevated weight of the vessel (excluding variable load) is sufficient to generate the required preload axial reaction at each leg. The maximum allowable preload axial leg reaction in any case is the storm-survival load given in Figure 7-1.
- 7.3.3 Identify maximum anticipated vessel weight, LCG, and TCG in elevated condition for the load case under investigation. Use the ELEVATED WEIGHT WORKSHEET in Figure 7-2 with the following instructions:
  - 7.3.3.1 Complete the DECK CARGO LOADING FORM in accordance with Section 10.3.1 of the Operations Manual.
  - 7.3.3.2 Complete the TANK LOADING FORM in accordance with Section 10.3.3 of the Operations Manual.
  - 7.3.3.3 The lightship weight and centers of gravity (less legs and pads) are listed in Section 4 of this report. These values have been included in the first row of the VESSEL LOADING FORM along with the appropriate moments.
  - 7.3.3.4 Enter the weight of the Crew, Effects, and Stores for the entire vessel crew in Column 1 on the appropriate row. The appropriate LCG, TCG and VCG have been pre-entered onto the form. Determine the vertical, longitudinal, and transverse moments by multiplying the weight in Column 1 by the LCG, TCG or VCG in Columns 2, 4 or 6, respectively. Enter the resulting moments in the appropriate Columns 3, 5 or 7 for the longitudinal, transverse, and vertical moments, respectively.

- 7.3.3.5 Determine the weight of the Offshore Workers to be on board the vessel by multiplying the number of workers by 0.173 t (173 kg) per worker. Enter this value in Column 1 on the appropriate row. The associated LCG, TCG or VCG for the Offshore Workers have been pre-entered onto the form. Determine the longitudinal, transverse, and vertical moments by multiplying the weight in Column 1 by the LCG, TCG or VCG and enter the resulting moments in Columns 3, 5 and 7 for the longitudinal, transverse and vertical moments, respectively.
- 7.3.3.6 Enter the total deck cargo weight from the DECK CARGO LOADING FORM in Column 1 on the appropriate row. Enter the total deck cargo longitudinal and transverse moments from the DECK CARGO LOADING FORM onto the appropriate row in Columns 3 and 5, respectively.
- 7.3.3.7 Enter the total tank liquids weight from the TANK LOADING FORM in Column 1 on the appropriate row. Enter the total tank loads' longitudinal and transverse moments from the TANK LOADING FORM onto the appropriate row in Columns 3 and 5, respectively.
- 7.3.3.8 Determine the vessel's total elevated weight by summing Column 1 and entering this value in Column 1 of the TOTALS row and calculation item (3). Determine the total moments by summing the longitudinal and transverse moments and entering these values in the TOTALS row in Columns 3 and 5, respectively.
- 7.3.3.9 Determine the vessel's elevated LCG and TCG as shown in calculation items (1) and (2), respectively, from the ELEVATED WEIGHT WORKSHEET.
- 7.3.3.10 Determine the value of half the elevated weight per calculation item (4) in the ELEVATED WEIGHT WORKSHEET.
- 7.3.3.11 Confirm that required preload can be achieved and that the elevated weight, LCG, and TCG are within allowable limits as described on the ELEVATED WEIGHT WORKSHEET.
- 7.3.4 The maximum elevated weight is 4407 MT. The required preload should be calculated per the instructions in Section 7.3 water . LCG and TCG constraints described in Section 7.5 shall be maintained at all times.
- 7.3.5 After tagging all four pads, preloading will commence by raising one pair of diagonally opposed legs until the load sensors in the jacking system of the active legs show a load equal to the desired reaction. The remaining two legs are then jacked down until the desired preload reaction is achieved. In the final stage of preloading, the original pair of legs should be lowered

until the elevated weight is evenly spread over all four legs, and the vessel can proceed with jacking up and out of the water. Detailed preloading instructions are as follows:

- 7.3.5.1 Determine the maximum reaction per leg from Figure 7-1 based on water depth and anticipated environmental condition: Storm Survival or Normal Operating.
- 7.3.5.2 Given the vessel weight and necessary maximum reactions, determine if the vessel has adequate weight for preloading. (See section 7.3.2)
- 7.3.5.3 Ballast as necessary to achieve the necessary weight to preload.
- 7.3.5.4 Initially, legs should be lowered simultaneously and evenly until the pads are tagged. Each leg should be lowered further if needed to ensure tilt is minimized. The jacking system sensors can assist in determining the jacking system loads during tagging.
- 7.3.5.5 Identify the initial lower guide reactions for each of the forward and aft legs individually from installed Hydraquip sensors.
- 7.3.5.6 Choose alternating pairs of legs to begin preloading: Forward Port with Aft Starboard or Forward Starboard with Aft Port.
- 7.3.5.7 Evenly raise one pair of diagonally-opposed legs until the maximum reaction on remaining legs is achieved. Adjustments are to be made to compensate for vessel LCG and TCG. For example if the Forward Port and Aft Starboard legs remain in location while the Forward Starboard and Aft Port leg are raised, one leg may achieve the necessary preload reaction before the other. If the Forward Port leg achieves the maximum reaction ahead of the Aft Starboard leg, the Forward Starboard leg should then remain in place while only the Aft Port leg is raised to achieve the desired preloading.
- 7.3.5.8 After achieving the necessary reaction on the Forward Port and Aft Starboard legs, lower the Forward Starboard and Aft Port legs until the desired reaction is achieved on these two legs. Again, adjustments are to be made to compensate for vessel LCG and TCG.
- 7.3.5.9 If ballast was brought onboard to achieve the required preload reaction, it should be discharged before the vessel is fully elevated unless the elevated weight and LCG and TCG constraints are satisfied.
- 7.3.5.10 Lower the Forward Port and Aft Starboard legs in order to evenly spread the weight over all four legs and proceed with jacking up and out of the water.



Figure 7-1: Preload Reaction Curve

ELEVATED WEIGHT WORKSHEET

	$N \rightarrow 1$	2	3	4	5
	WEIGHT	LCG	L-MOM	TCG	T-Mom
tem	(MT)	(m aft FRO)	(MT-m)	(m from CL, +STBD)	(MT-m)
IGHTSHIP LESS LEGS & PADS	3717.63	26.49	98,472	-0.78	-2,906
IGHTSHIP ADJUSTMENTS					<u> </u>
REW, EFFECTS, AND STORES					
OFFSHORE WORKERS, EFFECTS, AND STORES					
TOTAL DECK CARGO (from DECK CARGO LOADIN	IG				5
FORM) TANK LIQUIDS IN VESSEL'S TANKS (from TANK LOADING FORM)					
			_		
			-		
			-		
TOTA	ALS:				
		Elevated Weight Cal	<u>culations</u>		
(1) LCG = (Total Col. 3 / Total Col.	1) =	/	-	m aft of FR 0	
(2) TCG = (Total Col. 5 / Total Col. 1	L) =	/	_	m from CL (+STBD)	
(3) WEIGHT <del>-</del>	= Total Column 1 =		мт	V	
Storm Survival (S) or Nor	mal Operation (N)	=			
	Water Depth	_	— m		
	water Depth				
			<u>()</u> .		
Required Preload (per le			kN		
(4) Half of Elevated Weig	;ht = (3) / 2 * 9.81 =		KN		
CHECK ELEVATED WEIGHT CONSTRAINTS:					
		<u> </u>			
1) Is half of the elevated weig	ht greater than the r	equired preload?			
	YES	Vessel is read	y for preloading		
	NO	Additional we	ight is required for p	reloading	
		Add ballast or va	riable load and check aga	ain	
2A) Is the total elevated weig	ht (exlcuding crane h	ook load) less than 410	50 MT?		
	YES				
		Elevated weig	ht is permissible. Se	ee 2B.	
	NO	Elevated weig If no, see 3A.	ht is permissible. So	ee 2B.	
		If no, see 3A.		vated weight and check elevated weight a	gain
		If no, see 3A.			gain
2B) Is the LCG between 27.2m	NO	<b>If no, see 3A.</b> Decrease variable	e load to reduce total ele		gain
2B) Is the LCG between 27.2m	NO n and 30.6m aft of Fra YES	If no, see 3A. Decrease variabl ame 0; and is the TCG	e load to reduce total ele	vated weight and check elevated weight a	gain
2B) Is the LCG between 27.2m	NO	If no, see 3A. Decrease variabl ame 0; and is the TCG Elevated LCG	e load to reduce total ele near centerline?	vated weight and check elevated weight a	gain
2B) Is the LCG between 27.2m	NO n and 30.6m aft of Fra YES	If no, see 3A. Decrease variabl ame 0; and is the TCG Elevated LCG Elevated LCG	e load to reduce to tal ele near centerline? and TCG are permiss and TCG are NOT pe	vated weight and check elevated weight a	
2B) Is the LCG between 27.2m	NO n and 30.6m aft of Fra YES	If no, see 3A. Decrease variabl ame 0; and is the TCG Elevated LCG Elevated LCG In water depths g	e load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe reater than 60m, if the LC	vated weight and check elevated weight a ible rmissible	
2B) Is the LCG between 27.2m	NO n and 30.6m aft of Fra YES NO	If no, see 3A. Decrease variable ame 0; and is the TCG of Elevated LCG Elevated LCG In water depths g Shfit weights as r	e load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe reater than 60m, if the LC equired to achieve requir	vated weight and check elevated weight a <b>ible</b> G is forward of 30.6m aft of Fr. 0, the max	
2B) Is the LCG between 27.2m 3A) Is the total elevated weig	NO n and 30.6m aft of Fra YES NO	If no, see 3A. Decrease variable ame 0; and is the TCG Elevated LCG Elevated LCG In water depths g Shfit weights as r cook load) less than 440	e load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe reater than 60m, if the LC equired to achieve requir	vated weight and check elevated weight a <b>ible</b> <b>rmissible</b> G is forward of 30.6m aft of Fr. 0, the max ed LCG and TCG positions	
2B) Is the LCG between 27.2m 3A) Is the total elevated weig	NO h and 30.6m aft of Fra YES NO ht (exlcuding crane h	If no, see 3A. Decrease variable ame 0; and is the TCG of Elevated LCG In water depths g Shfit weights as of nook load) less than 444 Elevated weig	e load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe reater than 60m, if the LC equired to achieve requir 17 MT?	vated weight and check elevated weight a <b>ible</b> <b>rmissible</b> G is forward of 30.6m aft of Fr. 0, the max ed LCG and TCG positions <b>se 3B.</b>	
2B) Is the LCG between 27.2m 3A) Is the total elevated weig	NO and 30.6m aft of Fra YES NO ht (exlcuding crane h YES	If no, see 3A. Decrease variable ame 0; and is the TCG Elevated LCG In water depths g Shfit weights as r took load) less than 440 Elevated weig Elevated weig	e load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe reater than 60m, if the LC equired to achieve requir D7 MT? tht is permissible. So th is NOT permissible.	vated weight and check elevated weight a <b>ible</b> <b>rmissible</b> G is forward of 30.6m aft of Fr. 0, the max ed LCG and TCG positions <b>se 3B.</b>	wave height is reduced to 7π
2B) Is the LCG between 27.2m 3A) Is the total elevated weig	NO and 30.6m aft of Fra YES NO ht (exlcuding crane h YES	If no, see 3A. Decrease variable ame 0; and is the TCG Elevated LCG In water depths g Shfit weights as r took load) less than 440 Elevated weig Elevated weig	e load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe reater than 60m, if the LC equired to achieve requir D7 MT? tht is permissible. So th is NOT permissible.	vated weight and check elevated weight a <b>ible</b> <b>rmissible</b> G is forward of 30.6m aft of Fr. 0, the max ed LCG and TCG positions <b>ee 3B.</b> <b>ie.</b>	wave height is reduced to 7n
2B) Is the LCG between 27.2m 3A) Is the total elevated weig	NO NO NO ht (exlcuding crane h YES NO	If no, see 3A. Decrease variable ame 0; and is the TCG Elevated LCG In water depths g Shfit weights as r took load) less than 440 Elevated weig Elevated weig Decrease variable	e load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe reater than 60m, if the LC equired to achieve requir 17 MT? tht is permissible. So tht is NOT permissible e load to reduce total ele	vated weight and check elevated weight a <b>ible</b> <b>rmissible</b> G is forward of 30.6m aft of Fr. 0, the max ed LCG and TCG positions <b>ee 3B.</b> <b>ie.</b>	wave height is reduced to 7n
2B) Is the LCG between 27.2m 3A) Is the total elevated weig 3B) Is the LCG between 28.7m	NO	If no, see 3A. Decrease variable ame 0; and is the TCG Elevated LCG In water depths g Shfit weights as i toook load) less than 444 Elevated weig Elevated weig Decrease variable ame 0; and is the TCG	e load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe reater than 60m, if the LC equired to achieve requir 07 MT? (ht is permissible. So (ht is NOT permissible e load to reduce total ele near centerline?	vated weight and check elevated weight a <b>ible</b> <b>rmissible</b> G is forward of 30.6m aft of Fr. 0, the max ed LCG and TCG positions <b>ee 3B.</b> <b>e.</b> vated weight and check elevated weight a	wave height is reduced to 7n
2B) Is the LCG between 27.2m 3A) Is the total elevated weig 3B) Is the LCG between 28.7m	NO	If no, see 3A. Decrease variable ame 0; and is the TCG Elevated LCG In water depths g Shrfit weights as in oook load) less than 440 Elevated weig Decrease variable ame 0; and is the TCG Elevated LCG	e load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe reater than 60m, if the LC equired to achieve requir 07 MT? (ht is permissible. So (ht is NOT permissible e load to reduce total ele near centerline? and TCG are permiss	vated weight and check elevated weight a <b>ible</b> <b>rmissible</b> G is forward of 30.6m aft of Fr. 0, the max ed LCG and TCG positions <b>ee 3B.</b> <b>e.</b> vated weight and check elevated weight a <b>ible</b>	wave height is reduced to 7n
2B) Is the LCG between 27.2m 3A) Is the total elevated weig 3B) Is the LCG between 28.7m	NO	If no, see 3A. Decrease variable ame 0; and is the TCG Elevated LCG In water depths g Shfit weights as in ook load) less than 440 Elevated weig Decrease variable ame 0; and is the TCG Elevated LCG Elevated LCG	e load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe reater than 60m, if the LC equired to achieve requir 07 MT? tht is permissible. So tht is NOT permissible to load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe	vated weight and check elevated weight a <b>ible</b> <b>rmissible</b> G is forward of 30.6m aft of Fr. 0, the max ed LCG and TCG positions ee <b>3B</b> . e. vated weight and check elevated weight a <b>ible</b> <b>rmissible</b>	wave height is reduced to 7n
2B) Is the LCG between 27.2m 3A) Is the total elevated weig 3B) Is the LCG between 28.7m	NO	If no, see 3A. Decrease variable ame 0; and is the TCG Elevated LCG In water depths g Shfit weights as r ook load) less than 440 Elevated weig Decrease variable ame 0; and is the TCG Elevated LCG Elevated LCG Shfit weights as r	e load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe reater than 60m, if the LC equired to achieve requir 07 MT? tht is permissible. So tht is NOT permissible e load to reduce total ele near centerline? and TCG are permiss and TCG are NOT pe equired to achieve requir	vated weight and check elevated weight a <b>ible</b> <b>rmissible</b> G is forward of 30.6m aft of Fr. 0, the max ed LCG and TCG positions <b>ee 3B.</b> <b>e.</b> vated weight and check elevated weight a <b>ible</b>	wave height is reduced to 7m

Figure 7-2: Elevated Weight Worksheet

Ø

1/12/2024

ELEVATED WEIGHT WORKSHEET - 454 MT Variable Load  $COLUMN \rightarrow$ 1 2 3 4 5 WEIGHT LCG L-MOM TCG T-Mom (m from CL, +STBD) (MT-m) (MT) (m aft FRO) (MT-m) Item LIGHTSHIP LESS LEGS & PADS 3717.63 26.49 98,472 -0.78 2.906 LIGHTSHIP ADJUSTMENTS 4.00 0.00 31.25 125 0 CREW, EFFECTS, AND STORES 0.00 5.00 17.43 87 0 OFFSHORE WORKERS, EFFECTS, AND STORES 20.00 17.43 349 0.00 0 TOTAL DECK CARGO (from DECK CARGO LOADING FORM) 1055 222.88 51.10 11390 4.73 TANK LIQUIDS IN VESSEL'S TANKS (from TANK LOADING FORM) 5337.03 950.34 202.12 4.70 26.41 TOTALS 4,171.63 115,760 -901 Elevated Weight Calculations (1) LCG = (Total Col. 3 / Total Col. 1) = 115,760 4,171.63 27.75 m aft of FR 0 (2) TCG = (Total Col. 5 / Total Col. 1) = \_\_\_\_\_\_ 4,171.63 -0.22 m from CL (+STBD) (3) WEIGHT = Total Column 1 = 4.171.63 MT Storm Survival (S) or Normal Operation (N) Ν 40 Water Depth m **k**N Required Preload (per leg) from Figure 7-1 17,725.00 20,461.85 KN (4) Half of Elevated Weight = (3) / 2 \* 9.81 = CHECK FLEVATED WEIGHT CONSTRAINTS: 1) Is half of the elevated weight greater than the required preload? YES Vessel is ready for preloading NO Additional weight is required for preloading Add ballast or variable load and check again 2A) Is the total elevated weight (exlcuding crane hook load) less than 4160 MT? YES x Elevated weight is permissible. See 2B. NO If no, see 3A. Decrease variable load to reduce total elevated weight and check elevated weight again 2B) Is the LCG between 27.2m and 30.6m aft of Frame 0: and is the TCG near centerline? YES х Elevated LCG and TCG are permissible NO \_\_\_\_ Elevated LCG and TCG are NOT permissible In water depths greater than 60m, if the LCG is forward of 30.6m aft of Fr. 0, the max wave height is reduced to 7m Shfit weights as required to achieve required LCG and TCG positions 3A) Is the total elevated weight (exlcuding crane hook load) less than 4407 MT? YES Elevated weight is permissible. See 3B. NO \_\_ Elevated weight is NOT permissible. Decrease variable load to reduce total elevated weight and check elevated weight again 3B) Is the LCG between 28.7m and 30.6m aft of Frame 0; and is the TCG near centerline? Elevated LCG and TCG are permissible YES \_\_\_\_ Elevated LCG and TCG are NOT permissible NO \_\_\_\_ Shfit weights as required to achieve required LCG and TCG positions Water depth limit is 46m. See Leg Strength Cases Summary Chart. Figure 7-2: Elevated Weight Sample Calculation – 454 MT VL

1/12/2024

ELEVATED WEIGHT WORKSHEET - 709 MT Variable Load  $COLUMN \rightarrow$ 1 2 3 4 5 WEIGHT LCG L-MOM TCG T-Mom (m from CL, +STBD) (MT-m) (MT) (m aft FRO) (MT-m) Item LIGHTSHIP LESS LEGS & PADS 3717.63 26.49 98,472 -0.78 2.906 LIGHTSHIP ADJUSTMENTS 0.00 4.00 31.25 125 0 CREW, EFFECTS, AND STORES 0.00 5.00 17.43 87 0 OFFSHORE WORKERS, EFFECTS, AND STORES 20.00 17.43 349 0.00 0 TOTAL DECK CARGO (from DECK CARGO LOADING FORM) 530.74 52.78 28,014 3.91 2.075 TANK LIQUIDS IN VESSEL'S TANKS (from TANK LOADING FORM) 149.26 3.948 735 26.45 4.92 TOTALS 4,426.63 130,995 -96 Elevated Weight Calculations (1) LCG = (Total Col. 3 / Total Col. 1) = 130,995 4,426.63 29.59 m aft of FR 0 (2) TCG = (Total Col. 5 / Total Col. 1) = \_\_\_\_\_96 4,426.63 -0.02 m from CL (+STBD) (3) WEIGHT = Total Column 1 = 4.426.63 MT Storm Survival (S) or Normal Operation (N) Ν 40 Water Depth m - kN Required Preload (per leg) from Figure 7-1 17,725.00 21,712.62 KN (4) Half of Elevated Weight = (3) / 2 \* 9.81 = CHECK FLEVATED WEIGHT CONSTRAINTS: 1) Is half of the elevated weight greater than the required preload? YES Vessel is ready for preloading NO Additional weight is required for preloading Add ballast or variable load and check again 2A) Is the total elevated weight (exlcuding crane hook load) less than 4160 MT? YES Elevated weight is permissible. See 2B. NO If no, see 3A. Decrease variable load to reduce total elevated weight and check elevated weight again 2B) Is the LCG between 27.2m and 30.6m aft of Frame 0; and is the TCG near centerline? YES Elevated LCG and TCG are permissible NO \_ Elevated LCG and TCG are NOT permissible In water depths greater than 60m, if the LCG is forward of 30.6m aft of Fr. 0, the max wave height is reduced to 7m Shfit weights as required to achieve required LCG and TCG positions 3A) Is the total elevated weight (exlcuding crane hook load) less than 4407 MT? Х\_ YES Elevated weight is permissible. See 3B. NO \_ Elevated weight is NOT permissible. Decrease variable load to reduce total elevated weight and check elevated weight again. 3B) Is the LCG between 28.7m and 30.6m aft of Frame 0; and is the TCG near centerline? YES \_\_\_\_X\_\_\_ Elevated LCG and TCG are permissible Elevated LCG and TCG are NOT permissible NO \_\_\_\_\_ Shfit weights as required to achieve required LCG and TCG positions Water depth limit is 46m. See Leg Strength Cases Summary Chart. Figure 7-2: Elevated Weight Sample Calculation – 709 MT VL

### 7.4 Jacking Up

- 7.4.1 The following shall be used by the Master as guidance for elevating the vessel. ABS allowable limits on jacking and holding loads, leg axial reactions, and pad loading listed in Table 4-7, Table 4-19 and Table 4-20 should be adhered to when jacking the unit and holding position while elevated. Note that the values given in Table 4-7 represent the capabilities of the jacking system and are the governing values on axial loading. The jacking system load monitoring interface shall be used to confirm actual values are consistent with allowable limits.
- 7.4.2 To the Master's satisfaction, the bottom condition with respect to the soil type, levelness, and potential obstructions should be determined before elevating the vessel.
- 7.4.3 All four legs should be lowered simultaneously.
- 7.4.4 Once the pads have contacted the bottom and the vessel is supported by the legs, the vessel should be leveled by moving the legs individually. During preloading small tilt angles are acceptable. However, once preloading is complete, the vessel should be leveled again and the vessel should be kept level at all times while jacking.
- 7.4.5 Deploy the overboard pumps.
- 7.4.6 Once the vessel's hull has cleared the wave tops, the elevation shall be stopped for preloading, evaluation of the footing, and to allow the pads to settle into the bottom. Preloading shall be performed per the instructions in this manual.
- 7.4.7 It is recommended that the required preload reaction should be held on each diagonal of 2 legs under preload weight for a period of at least 3 hours without further settling, unless specifically instructed otherwise by SEACOR Marine management. This settling period should be extended at the discretion of the Master when spotting the vessel near underwater or environmental hazards.
- 7.4.8 If, after the settling period and evaluation of the footing, the bottom conditions are determined inadequate for continued elevation, for example, if a leg continues penetrating or if the vessel cannot be made level, the preloading ballast (if any) shall be discharged and the vessel jacked down. After the preload ballast has been dumped (if any) care should be taken to ensure a stable afloat condition if the vessel will move to a different location. The Master may use the stability and loading forms in Section 10 of this manual for this purpose.

- 7.4.9 If, after the settling in period and evaluation of the footing, the master determines the bottom conditions are adequate for continued elevating, the preloading ballast (if any) shall be discharged and the vessel may be elevated to the final elevated location. The vessel shall be kept level while elevating. Care should be taken prior to jacking that the elevated load condition is such that ABS leg axial load limits will not be exceeded. The Jacking Load Form contained in Appendix J to this manual may be used by the Master to determine these loads. LCG and TCG limits as described in Section 7.5 should be observed and the Master may choose to reposition variable loads to achieve a suitable elevated loading condition.
- 7.4.10 If at any time during the jacking or evaluation process, the vessel develops a heel or trim or if one leg has to be moved significantly more than the others to keep the vessel level, the jacking shall be stopped as soon as safely possible and the cause of the heel or trim determined before corrective action is taken. If a cause cannot be determined, or the cause is not correctable (i.e. poor bottom conditions), the vessel shall be jacked down to a safe position with minimal air gap until a corrective plan is developed. Watertight integrity shall be maintained. Personnel not directly involved with assessing the vessel's condition after a rapid settling event has occurred shall muster in a pre-designated area assigned by the Master and shall have Flag State approved Personnel Floatation Devices (PFD) accessible and ready for use. If further danger to personnel exists, evacuation of nonessential personnel and up to abandon ship of all personnel should be considered. The Master should consult with SEACOR Marine management for further instructions regarding vessel inspection and recovery. See

## 7.5 Punch Through Procedure

- 7.5.1 Stop all activities immediately and conduct an urgent assessment of the situation.
  - 7.5.1.1 Verify the watertight integrity. Check the doors and hatches for leaks. Examine the hull and other compartments to prevent further water intrusion.
  - 7.5.1.2 Vacate the Engine Room (ER) and seal the doors on the way out.
  - 7.5.1.3 Activate "Sliding watertight door system" to isolate port and starboard compartments of the ER.
  - 7.5.1.4 If water ingress cannot be contained, the abandon ship procedure should be initiated.
- 7.5.2 If possible, attempt to measure the air gap on both sides of the barge, to ascertain the depth of a punch through.

7.5.3 Should the punch through be minor, meaning that the hull is either above the water or partially submerged with buoyancy keeping it afloat, the crew should try to re-establish balance and level

the hull.

- 7.5.3.1 This can be accomplished by offloading the ballast (if any) and freshwater from the punch-through side of the barge, thereby reducing the weight on that side.
- 7.5.3.2 Transferring fuel from one side to another may also be an option to redistribute weight away from the affected area.
- 7.5.3.3 Elevate the unimpacted legs (those not involved in the punch through) as this action will effectively lower the hull closer to a balanced level. These legs' jacking systems are less likely to have sustained damage.
- 7.5.3.4 The jacking system operator should avoid attempting to level the hull by lowering the legs involved in the punch through. Such an action could further damage the jacking system and raise the hull, which contradicts the goal of reducing the air gap to a safe level.
- 7.5.3.5 If the jacking system fails to move the legs, activate the emergency jacking panel.
- 7.5.4 However, if the punch through is severe, the Master should evacuate the personnel and seek assistance. A severe punch through is characterized by:
  - 7.5.4.1 Partial submergence of the hull and inability to contain water intrusion into machinery spaces.
  - 7.5.4.2 The hull being tilted at an angle that makes leveling impossible.
  - 7.5.4.3 Total loss of power with no viable means of restoration. Inability to move the legs or operate the pumps.
- 7.6 LCG and TCG While Elevated:
- 7.6.1 In general, while elevated, LCG and TCG of the combined hull and any variable loads should be maintained coincident with the geometric center of the rectangle formed by the legs. The leg rectangle center is located 30.6m aft of the bow (Frame 0), on centerline. While elevated in heavy weather, (wind speeds above 50 knots) or in storm survival mode, the LCG should be 30.6m aft of the bow. The TCG should be on centerline during heavy weather.
- 7.6.2 The TCG should always be maintained near centerline as described above. In water depths less than 60m, an LCG range of 27.2m to 30.6m aft of Frame 0 is acceptable; (with up to 50 knots winds and a 10 meter maximum wave). In water depths greater than 60m, the maximum wave height is reduced to 7 meters unless then LCG is located near the leg rectangle center. If operating in water depths exceeding 60m and forecasted maximum wave heights exceeds 7 meters, contact SEACOR Marine management for specific guidance.

- 7.6.3 During heavy lift crane operations (181 tonnes hook load), the LCG of the hull plus any variable load but excluding the influence of the crane and hook load weights and moments, should be located near the leg rectangle center. The TCG of the hull plus any variable load but excluding the influence of the crane and hook load weights and moments should be on centerline. Shifts in the combined LCG and TCG under the influence of the heavy lift are accounted for in leg strength calculations. The master should consult with SEACOR Marine management to plan for maximum lift operations.
- 7.6.4 These LCG and TCG guidelines are aimed at ensuring that elevated loads do not get so unbalanced as to overload any particular leg while the vessel is experiencing harsh weather (see Sections 6.3.3 and 6.3.4), or when making a maximum 181 t lift in weather suitable for such lifts (see Section 6.3.5).
- 7.6.5 When in doubt, or when engaging in operations not specifically addressed by this manual, consult with SEACOR Marine management for suitable loading instructions.
- 7.7 Jacking Down
- 7.7.1 The following shall be used by the Master as guidance for lowering the vessel:
  - 7.7.1.1 Secure watertight and weather tight closures for afloat operation.
  - 7.7.1.2 Secure cranes and deck cargo for afloat operations.
  - 7.7.1.3 If the vessel's loading has changed while elevated, ensure the new loading condition meets the stability requirements in Section 10 of this Manual.
  - 7.7.1.4 Ensure the ballast used for preloading (if any) has been discharged.
  - 7.7.1.5 One submersible pump shall remain deployed while jacking down to charge the firemain.
  - 7.7.1.6 Turn on the Impressed Current Cathodic Protection (ICCP) system.
  - 7.7.1.7 When jacking down and before the vessel is afloat, the vessel should be kept level. Once afloat, the legs should be raised simultaneously.
  - 7.7.1.8 If difficulty is experienced freeing the pads from the sea floor, see Section 7.7
  - 7.7.1.9 Once afloat, the cause of any heel or trim shall be determined and corrective action taken before getting underway. If the corrective action requires moving deck cargo with the vessel's cranes, the vessel must be elevated before the cranes are used.

### 7.8 Jetting System

- 7.8.1 The following shall be used by the Master as guidance for freeing the pads from the sea floor if unable to lift legs via normal efforts.
  - 7.8.1.1 Submerge vessel hull as needed.
  - 7.8.1.2 Ensure seacocks are open, sea chests are flooded, and there is a supply of water to main fire pump.
  - 7.8.1.3 Deploy both submersible pumps.
  - 7.8.1.4 Isolate both submersible pumps to supply water to the jetting system. Keep fire pump connected to the fire system.
  - 7.8.1.5 Determine which pad is to be jetted and connect the jetting system to the appropriate leg port.
  - 7.8.1.6 Engage jetting system while raising the leg slowly.
- 7.9 Receiving Vessels Alongside
- 7.9.1 The vessel shall be elevated and preloaded prior to bringing a vessel alongside. Wind speeds shall be less than 30 kts and waves less than 2 meters. Fenders shall be deployed, and vessel made fast to the satisfaction of the master. Use of a DP vessel without the need for mooring lines is preferred.

## 8 Preparing the Vessel for Heavy Weather

## 8.1 Weather Monitoring

- 8.1.1 When elevated in open water, the weather forecast must be monitored regularly and a heavy weather action plan developed that considers the forecast, current weather conditions, water depth, and vessel limitations. Specific considerations the Master should evaluate in heavy weather action planning include:
  - 8.1.1.1 The maximum wind speed for normal operations is 70 knots with a maximum current of 2 knots. If winds are expected to exceed 70 knots, the vessel should seek safe harbor as described herein.
  - 8.1.1.2 The maximum environmental limits for the storm survival condition include: maximum 100 knots of wind speed, 2 knots current, 10 m maximum seas and maximum 30 m water depth (including storm surge).
  - 8.1.1.3 The maximum wave height limits, as described in Section 6.3, apply.
  - 8.1.1.4 Specific attention should be paid to forecasts that predict sea states higher than 1 to 2 m (significant wave height), as 2 m is the maximum allowable afloat sea state for vessel survivability described in Section 6.3.
  - 8.1.1.5 Estimated time to prepare the vessel for jacking down and getting underway.
  - 8.1.1.6 Estimated time and route to harbor of safe refuge or relocation move. The vessel shall not require more than 12 hours to reach such refuge.
- 8.2 When Heavy Weather is Forecast
- 8.2.1 The vessel requires no special modifications to meet severe storm conditions except those practices mentioned below. When determining the time required to prepare for heavy weather, the following factors should be considered:
  - 8.2.1.1 Time to jack up or down or change air gap; to be based on a nominal jacking speed of 1.2 meters per minute (4 feet per minute)
  - 8.2.1.2 Time to preload per Section 7.4.7 (if possible)
  - 8.2.1.3 Time to transit to harbor of safe refuge, assuming a conservative average speed against wind and waves (if required)
  - 8.2.1.4 Time to secure cranes, deck cargo, and hatches/doors as required.

- 8.2.2 If wave height and wind predications do not exceed the elevated environmental limits for normal operations:
  - 8.2.2.1 Determine the timeline for the weather event, including when the seas are anticipated to exceed the limits discussed in Section 6.3.1, when the maximum wind and seas are expected, and when the seas will subside to the limits discussed in Section 6.3.1 and 6.3.2.
    - 8.2.2.1.1 The vessel is to remain elevated once the seas exceed the limits specified in Section 6.3.1 and 6.3.2, or the response of the vessel, when subject to a certain wave height and period combination, is such that serious damage to the legs or towers due to whipping is likely.
  - 8.2.2.2 Determine if the current location will be adequate for the predicted wind and seas. If not adequate, prepare relocation plan.
  - 8.2.2.3 Secure cranes and deck cargo. Secure all watertight and weather tight openings not required for vessel operation.
  - 8.2.2.4 If a relocation move is necessary, it must be accomplished before the seas exceed the limits discussed in Section 6.3.1 and 6.3.2.
  - 8.2.2.5 If staying on location, ensure that the elevated load condition (lightship plus variables loads) is balanced to the same degree as when the vessel was elevated (see Section 7.5 for LCG and TCG limits).
- 8.2.3 If wave height or wind predications exceed the elevated environmental limits for normal operations:
  - 8.2.3.1 Determine the timeline for the weather event, including when the seas are anticipated to exceed the limits discussed in Section 6.3.1 and 6.3.2, when the maximum wind and seas are expected, and when the seas will subside to the limits discussed in Section 6.3.1 and 6.3.2, or less.
  - 8.2.3.2 Determine route and estimated time to harbor of safe refuge. The vessel shall not require more than 12 hours to reach such refuge.
  - 8.2.3.3 Secure cranes and deck cargo. Secure all watertight and weather tight openings not required for vessel operation.
  - 8.2.3.4 Jack vessel down and proceed to harbor of safe refuge. This entire operation must be completed before the seas reach the limits discussed in Section 6.3.1 and 6.3.2, or the

winds exceed 50 knots. All personnel not essential to the vessel operation during the inclement weather should be removed from the vessel when practicable.

8.2.3.5 In lieu of returning to dock, the liftboat can withstand storm conditions while jacked in 30 m of water including storm surge. See 7.3.5 of this manual for additional requirements when operating in the elevated survival condition.

XIC RO

## 9 Procedures for Discovering the Flooding of a Leg

- 9.1 General Discussion Concerning Excessive List or Heel
- 9.1.1 When afloat, the heel and trim of the vessel shall be minimized. The Stability Loading Forms presented in Section 10 of this manual may be used to estimate the heel and trim of specific loading conditions. Every effort should be made to determine the causes of unexpected heel or trim before corrective action is taken.
  - 9.1.1.1 Sound all tanks to ensure they are at the anticipated levels. Reevaluate loading conditions if discrepancies are found.
  - 9.1.1.2 Check all compartments and voids for water, and de-water if required. Determine cause of flooding before proceeding. If the cause is indeterminate, the compartment or void shall be frequently monitored while underway.
  - 9.1.1.3 Verify deck cargo arrangements and weights. If deck cargo requires relocation utilizing the vessel's cranes, the vessel must be elevated before the cranes are used.
- 9.1.2 If the cause of the excessive list or heel cannot be determined by the above, it may be due to a flooded leg or pad. Whether verified or not, the vessel shall be assumed to be in a damaged condition due to the flooded leg or pad, and an emergency action plan shall be developed and implemented. The following shall be considered by the Master when developing an emergency action plan:
  - 9.1.2.1 All personnel shall don approved Personnel Floatation Devices for the duration of the emergency. At the Master's discretion, personnel not required for the operation of the vessel shall muster at their predetermined muster locations.
  - 9.1.2.2 If possible, elevate the vessel immediately while an emergency action plan is developed. If elevation is not possible, the vessel shall be moved to a location where elevation is possible, and the vessel jacked up to a position above the wave tops.

- 9.1.2.3 If when afloat in the damaged condition, the average port and starboard draft amidships (at the load line marks) is less than or equal to the required load line draft, the vessel may proceed to a harbor of safe refuge or other protected waters where the damage can be evaluated. During the voyage, tanks, voids, and hull compartments shall be frequently monitored for leaks. If uncontrolled flooding is noted, the vessel shall be elevated as soon as safely possible and the cause of the flooding determined before proceeding.
- 9.1.2.4 If when afloat in the damaged condition, the average port and starboard draft amidships (at the load line marks) is greater than required load line draft, the vessel is not in compliance with its stability requirements for operation afloat and cannot operate afloat, except to execute emergency maneuvering. The vessel should be elevated immediately, consistent with safe jacking procedures, and the proper emergency authorities notified. Afloat operations are <u>not</u> allowed until an accepted plan is developed for vessel movement. The requirements of this plan, and the involvement of outside regulatory agencies or private interests, is dependent on the specifics of the casualty and is outside the scope of this manual.

## **10 Stability Information**

- 10.1.1 The vessel shall be loaded according to the instructions below and on the Stability Loading Forms or Excel workbook included in this manual.
- 10.1.2 Compliance with the stability criteria does not ensure immunity against capsizing regardless of the circumstances, nor absolve the Master from his responsibilities. The Master should therefore exercise prudence and good seamanship having regard to the season of the year, weather forecasts and the navigational zone. The Master should take the appropriate action, speed and course warranted by the prevailing circumstances. In addition to the instructions included in this operations manual, the Master must also comply with the latest revision of SEACOR Marine's Safety Management System requirements for safe navigation. Care should be taken that the cargo allocated to the ship is capable of being stowed so that compliance with the criteria can be achieved. Before a voyage commences care should be taken to ensure that the cargo and sizable pieces of equipment have been properly stowed or lashed as per the vessel-specific cargo securing manual to minimize the possibility of both longitudinal and lateral shifting while at sea, under the effect of acceleration caused by rolling and pitching. (Regulatory cite IMO Resolution A.739 2.3.1)
- 10.1.3 After loading and prior to departure and at other times necessary to assure the safety of the vessel, the Master shall determine that the vessel complies with all applicable stability requirements and enter a statement of verification in the log book. The vessel may not depart until it is in compliance with these requirements. Any stability calculations made in support of the determination must be retained on board the vessel for the duration of the voyage.
- 10.1.4 Vessel route is restricted. Operation on exposed waters is permitted only when operating not more than twelve hours from a harbor of safe refuge or a location where the vessel may elevate to survive 100 knots wind. Since the vessel's route is based on other considerations in addition to stability, the Master is cautioned that the route may be further limited.
- 10.1.5 The maximum summer salt water load line average molded draft is 3.576m ABL. This corresponds to a displacement of 7,602 t. The Master shall, upon departure on an ocean or coastwise voyage, enter in the vessel's logbook a statement of the position of the load line markings, port and starboard, relative to the surface of the water in which the vessel is floating. If the density of the water in which the vessel is floating is compensated for, this density shall also be noted in the vessel's logbook.

- 10.1.6 Main deck hatches and weather doors to the deckhouse and machinery spaces shall be kept closed and fully secured at all times when underway, except when actually used for transit under safe conditions.
- 10.1.7 The trim and list of the vessel shall be kept to a minimum at all times.
- 10.1.8 Cross connections between all port and starboard tanks shall be closed at all times when the vessel is underway, including applicable valves in the ballast manifold.
- 10.1.9 The vessel is designed to meet a one compartment standard of flooding as detailed in 0722-851-001 "Seacor Marine" ", LLC M300-4 Liftboat Stability Support Calculations" Watertight transverse bulkheads, required in association with the flooding stability criterion, are located at Frames 5, 11, 17, 30, 34, 40 and 46. In addition, the longitudinal engine room bulkhead between Frames 17 and 30 is required as part of the flooding stability standard. Changes to these bulkheads, or to the tank, void, and compartment boundary bulkheads below the main deck that would affect their watertight integrity, require the authorization and supervision of ABS and the flag state authority.
- 10.1.10 When afloat, deck cargo must be positively secured against shifting prior to leaving protected waters.
- 10.1.11 Freeing ports must be kept unobstructed at all times.
- 10.1.12 The vessel is equipped with cranes not for operation while afloat. While afloat, the cranes shall be stowed in their respective cradles.
- 10.1.13 The vessel's bilges and voids shall be kept pumped to minimum content at all times.
- 10.1.14 The Master shall make every effort to determine the cause of any list of the vessel before taking corrective action.
- 10.1.15 Any changes made to the vessel after the Inclining Experiment that could alter the lightship characteristics needs to be recorded in Section 24 of this manual. All changes should be reported to SEACOR Marine, LLC management. No fixed ballast or other such weights shall be added, removed, altered, and/or relocated without the authorization and supervision of ABS and the flag state authority.
- 10.1.16 The stability of the vessel should be checked periodically throughout a voyage as fuel is consumed and ballast added, or at any time the loading of the vessel is modified.

- 10.1.17 Nominal maximum cargo height above main deck has been assumed at 9 m. Consult SEACOR Marine, LLC management if unusually tall cargo will be carried.
- 10.2 General Stability Discussion
- 10.2.1 Stability must be evaluated prior to departure and at any time during the voyage where the vessel's loading is changed.
- 10.2.2 To determine the stability for a specific loading condition, the three (3) stability loading forms must be completed. These forms can be completed using the provided Excel workbook as an aid to the Master's calculations. The Excel workbook's calculations are to be verified by manual calculations periodically. These forms are:
  - 10.2.2.1 DECK CARGO LOADING FORM This form is used to record the weight, LCG, TCG, and VCG of the deck cargo. The total weight and longitudinal, transverse, and vertical moments of the deck cargo are calculated on this form and transferred to the VESSEL LOADING FORM. This form is also used to record and sum the liquid weight and FSM of any temporary deck tanks carried on the cargo deck.
  - 10.2.2.2 TANK LOADING –This form is used to record tank soundings and the corresponding weight, LCG, TCG, VCG, and FSM of the liquid carried in the vessel's tanks. The longitudinal, transverse, and vertical moments are determined in this form. The moments, summed weight, and summed FSMs are to be transferred to the VESSEL LOADING FORM.
  - 10.2.2.3 VESSEL LOADING FORM This form is used to calculate the vessel's total weight (displacement), VCG, LCG, and TCG for the particular loading condition. Mean Draft is determined, and the draft and VCG are checked against the Allowable VCG versus Draft curve included in this manual. This form may also be used to calculate the vessel's list, trim, and the drafts at the BOW and TRANSOM. Draft can also be calculated at the location of the stern thrusters, which extend 0.87 m below the baseline. When using these loading forms be sure to include any alterations/corrections to lightship. See Section 24 of this manual for further instructions.

# 10.2.3 A Curve of Allowable VCG versus Draft is included to be used for evaluating the stability of a particular loading condition. The Master must verify that the vessel's condition falls within the allowable operating range of this plot before beginning a voyage or changing the vessels loading condition during a voyage (See Stability Operating Instructions, Section 10).

ter et

#### 10.3 Stability Loading Form Instructions

- 10.3.1 Instructions for determining the weight, and the vertical, longitudinal, and transverse moments of the deck cargo using the DECK CARGO LOADING FORM:
  - 10.3.1.1 Verify the weight of each item of deck cargo as it is loaded. Enter the weight in Column 1, the LCG aft of the headlog (Frame 0) in Column 2, the TCG from the vessel CL in Column 4, and the VCG above the Main Deck in Column 6
  - 10.3.1.2 Temporary deck tanks require two entries on the DECK CARGO LOADING FORM, one for the weight, VCG, LCG, and TCG of the empty tank and a separate line item for the liquid weight, VCG, LCG, and TCG. Enter the free surface moment (FSM) of the liquid in Column 10. See section 10.2.2 for a discussion of determining the FSM for temporary deck tanks.
  - 10.3.1.3 Sum the weights in Column 1 to obtain the total weight of the deck cargo. Enter this total on the DECK CARGO LOADING FORM and the VESSEL LOADING FORM.
  - 10.3.1.4 The VCG entered on the DECK CARGO LOADING FORM is the distance above the Main Deck plating. To convert the VCG to the distance above BL, 4.6m (Column 6 + Column 7 on the DECK CARGO LOADING FORM). Multiply each weight in Column 1 by its corresponding VCG above BL (Column 8) to determine the vertical moment. Enter this moment on the corresponding line in Column 9. Sum the vertical moments in Column 9 to obtain the total vertical moment for all deck cargo. Enter this value on the DECK CARGO LOADING FORM and the VESSEL LOADING FORM.
  - 10.3.1.5 Multiply each weight in Column 1 by its corresponding LCG in Column 2 to obtain the longitudinal moment and enter this value in Column 3. Sum the longitudinal moments in Column 3 to obtain the total longitudinal moment for all deck cargo. Enter this value on the DECK CARGO LOADING FORM and the VESSEL LOADING FORM.
  - 10.3.1.6 Multiply each weight in Column 1 by its corresponding TCG in Column 4 to obtain the transverse moment and enter this value in Column 5. Note the starboard moments are positive and the port moments are negative. Sum the transverse moments in Column 5 to obtain the total transverse moment for all deck cargo. Enter this value on the DECK CARGO LOADING FORM and the VESSEL LOADING FORM.

10.3.1.7 Sum the deck tanks' FSM moments in Column 10 to obtain the total deck cargo FSM. Enter this value on the DECK CARGO LOADING FORM and the VESSEL LOADING FORM.

- 10.3.2 Instructions for determining the FSM of Temporary Deck Tanks:
  - 10.3.2.1 Liquids may be carried on the cargo deck in temporary deck tanks consistent with the vessel's stability requirements, statutory restrictions, and applicable hazardous material, noxious liquid substance, and pollution regulations.
  - 10.3.2.2 The maximum free surface moment (FSM) for each temporary deck tank anticipated to carry liquids at any time during the voyage must be determined. This maximum FSM value must be included on the DECK CARGO LOADING and VESSEL LOADING forms. The maximum FSM is specific to the tank and liquid carried and may be determined by independent calculation, provided by the tank supplier, or, for specific tank geometries, can be calculated using the DECK TANK FSM CALCULATION WORKSHEET included in this manual.
  - 10.3.2.2.1 The DECK TANK FSM CALCULATION WORKSHEET can be used to determine the maximum FSM for rectangular or cylindrical tanks oriented as shown on the worksheet. Instructions for determining the maximum FSM are included with the worksheet.
- 10.3.3 Instructions for completing the TANK LOADING FORM:
  - 10.3.3.1 The instructions required for completing the TANK LOADING FORM are included with the form.
- 10.3.4 Instructions for determining the vessel's total weight (displacement) LCG, TCG and VCG and using the VESSEL LOADING FORM:
  - 10.3.4.1 The lightship weight and centers of gravity are listed in Section 4 of this report. These values have been included in the first row of the VESSEL LOADING FORM along with the appropriate moments.
  - 10.3.4.2 Enter the weight of the Crew, Effects, and Stores for the entire vessel crew in Column 1 on the appropriate row. The appropriate LCG, TCG and VCG have been pre-entered onto the form. Determine the vertical, longitudinal, and transverse moments by multiplying the weight in Column 1 by the LCG, TCG or VCG in Columns 2, 4 or 6, respectively. Enter the resulting moments in the appropriate Columns 3, 5 or 7 for the longitudinal, transverse, and vertical moments, respectively.

- 10.3.4.3 Determine the weight of the Offshore Workers to be on board the vessel by multiplying the number of workers by 0.173 t (173 kg) per worker. Enter this value in Column 1 on the appropriate row. The associated LCG, TCG or VCG for the Offshore Workers have been pre-entered onto the form. Determine the longitudinal, transverse, and vertical moments by multiplying the weight in Column 1 by the LCG, TCG or VCG and enter the resulting moments in Columns 3, 5 and 7 for the longitudinal, transverse and vertical moments, respectively.
- 10.3.4.4 Enter the total deck cargo weight from the DECK CARGO LOADING FORM in Column 1 on the appropriate row. Enter the total deck cargo longitudinal, transverse, and vertical moments from the DECK CARGO LOADING FORM onto the appropriate row in Columns 3, 5 and 7, respectively.
- 10.3.4.5 Enter the sum of the total temporary deck tanks FSM from the DECK CARGO LOADING FORM and the total FSM from the TANK LOADING FORM in the appropriate row in Column 7.
- 10.3.4.6 Enter the total tank liquids weight from the TANK LOADING FORM in Column 1 on the appropriate row. Enter the total tank loads' longitudinal, transverse, and vertical moments from the TANK LOADING FORM onto the appropriate row in Columns 3, 5 and 7, respectively.
- 10.3.4.7 Determine the vessel's total weight by summing Column 1 and entering this value in Column 1 of the TOTALS row. Determine the total moments by summing the longitudinal, transverse, and vertical moments and entering these values in the TOTALS row in Columns 3, 5 and 7 respectively.
- 10.3.4.8 Determine the vessel's LCG, TCG or VCG as shown in calculation items (1), (2) and (3), respectively, from the Vessel Loading Form.
- 10.3.4.9 Determine the mean draft of the vessel, calculation item (5), using the Hydrostatic Properties table, Table 11-1. When the vessel's displacement (total weight) falls between two lines on the Hydrostatic Table, the draft may be determined by linear interpolation or, alternately, by using the value that corresponds to the next highest displacement in the table. For example, a displacement of 7164 t has a corresponding draft (saltwater) of 3.4 m ABL.

- 10.3.4.10 Using the mean draft value determined above, plot the loading condition's draft, and VCG on the Allowable VCG versus Draft curve. This plotting is accomplished by drawing a vertical line up from the mean draft value and a horizontal line over from the VCG value. The plotted point is the intersection of these lines. This point must fall below the curve, indicating the loading condition meets the applicable stability requirements. If the plotted point falls **above the curve**, the loading condition <u>does not meet</u> the applicable stability requirements and the loading condition must be revised by removing deck cargo from the boat, moving heavy items closer to the deck, or increasing below deck tonnage, so long as the load line draft is not exceeded. The new loading condition must be re-evaluated, and the new point plotted and checked on the Allowable VCG versus Draft curve. The stability criteria must be met before the vessel can sail. Any changes to the vessel's loading condition made during a voyage must be checked using the above procedures before they are implemented.
- 10.3.4.11 Included on the VESSEL LOADING FORM are optional calculations to be used for determining the trim and heel of the loading condition as well as the drafts at the FP and AP. The hydrostatic values used for these calculations are from the Hydrostatic Properties table using the same method as was used to determine the mean draft.
- 10.3.4.12 The VESSEL LOADING FORM also includes calculations for determining the navigational draft at the stern thruster units.

## **10.4 Hydrostatic Properties**

#### Table 10-1: Hydrostatic Properties

Note: 1) Distances are measured from Frame 0 & baseline.	2) Submerged portions of the leg	s & pads are buoyant and included in hydrostatics.

ALCON				Doc No: 0722-010-005-C5							_	1-25					
.0.4 H	lydrosta	atic Pro	operti	es												10	
							Table	e 10-1: Hy	drostatic	Properties						21	
lata, 1)	Distanc	oc oro n	0000118	d from F	rama 0	9. haca	line 2)	Submor	and nort	ions of t		& pads ar		at and in			
Draft	Distanc	LCB	VCB	WPA	LCF	KMT	KML	BMT		WSA		MH .01 deg					
	MT	m	m	m <sup>2</sup>	m	m	m	m	m	m <sup>2</sup>	MT	MT-m	MT-m	MT-m	MT-m	MT-m	MT-m
m 2.00	3725	29.8	1.1	2300.5	31.4	80.9	180.6	79.9	179.5	3549.5	2.36	51.91	5191	7.51	116.68	11668	10.71
2.10	3963	29.9	1.1	2357.2	32.0	79.1	180.0	77.9	175.5	3629.1	2.42	53.89	5389	7.80	124.94	12494	11.47
2.20	4207	30.0	1.2	2384.4	32.3	76.6	176.7	75.4	175.6	3680.4	2.44	55.39	5539	8.01	128.89	12889	11.83
2.30	4451	30.1	1.3	2387.9	32.2	72.7	167.9	71.4	166.7	3708.7	2.45	55.47	5547	8.02	129.47	12947	11.89
2.40	4696	30.2	1.3	2391.5	2391.5 32.2 69.1 160.0 67.8	158.7	3736.9	2.45	55.55	5555	8.04	130.04	13004	11.94			
2.50	4941	30.3	1.4	2395.0	32.1	65.9	152.8	64.5	151.5	3765.1	2.45	55.62	5562	8.05	130.62	13062	11.99
2.60	5187	30.4	1.4	2398.3	32.1	62.9	146.3	61.5	144.9	3793.2	2.46	55.70	5570	8.06	131.17	13117	12.04
2.70	5433	30.5	1.5	2401.4	32.1	60.3	140.3	58.8	138.9	3821.3	2.46	55.75	5575	8.07	131.67	13167	12.09
2.80	5679	30.6	1.5	2404.5	32.0	57.8	134.9	56.3	133.4	3849.4	2.46	55.80	5580	8.07	132.19	13219	12.14
2.90	5926	30.6	1.6	2408.3	32.0	57.8	130.0	54.0	128.4	3877.8	2.47	55.89	5589	8.09	132.82	13282	12.19
3.00 3.10	6173 6420	30.7 30.7	1.6 1.7	2412.1 2415.7	31.9 31.9	53.6 51.7	125.5 121.3	52.0 50.0	123.9 119.6	3906.3 3934.4	2.47 2.48	55.98 56.06	5598 5606	8.10 8.11	133.45 134.05	13345 13405	12.25 12.31
3.20	6668	30.7	1.7	2415.7	31.9	50.0	121.5	48.2	119.0	3962.6	2.48	56.13	5613	8.11	134.64	13464	12.31
3.30	6916	30.8	1.8	2422.7	31.8	48.4	117.4	46.6	112.0	3990.8	2.48	56.20	5620	8.13	135.23	13523	12.42
3.40	7164	30.8	1.9	2426.1	31.8	46.9	110.5	45.0	108.6	4019.0	2.49	56.28	5628	8.14	135.80	13580	12.47
3.50	7413	30.9	1.9	2429.5	31.7	45.5	107.3	43.6	105.4	4047.2	2.49	56.35	5635	8.15	136.36	13636	12.52
3.60	7662	30.9	2.0	2432.8	31.7	44.2	104.4	42.2	102.4	4075.3	2.49	56.43	5643	8.16	136.93	13693	12.57
3.70	7912	30.9	2.0	2435.0	31.6	42.9	101.5	40.9	99.4	4102.7	2.50	56.46	5646	8.17	137.30	13730	12.61
3.80	8161	30.9	2.1	2437.1	31.6	41.7	98.7	39.7	96.6	4129.9	2.50	56.49	5649	8.17	137.66	13766	12.64
3.90	8411	31.0	2.1	2439.3	31.6	40.6	96.2	38.5	94.0	4157.2	2.50	56.53	5653	8.18	138.04	13804	12.67
4.00	8661	31.0	2.2	2441.3	31.6	39.6	93.7	37.4	91.5	4184.3	2.50	56.57	5657	8.18	138.38	13838	12.70
4.10	8912	31.0	2.2	2443.0	31.5	38.6	91.4	36.4	89.2	4211.3	2.50	56.61	5661	8.19	138.67	13867	12.73
4.20 4.30	9162	31.0	2.3	2444.7	31.5	37.7	89.2 87.1	35.4	86.9	4238.3	2.51	56.65	5665	8.20	138.96	13896	12.76
4.30																	
4.40															-		
4.60											1						
.40 .50	9413 9663 9914 10165	31.0 31.0 31.0 31.1	2.3 2.4 2.4 2.5	2446.3 2447.9 2449.5 654.6	31.5 31.5 31.5 13.6	36.8 36.0 35.2 6.5	87.1 85.1 83.2 8.7	34.5 33.6 32.8 4.0	84.8 82.7 80.8 6.2	4265.3 4292.3 4319.3 6142.8	2.51 2.51 2.51 0.67	56.68 56.72 56.75 7.12	5668 5672 5675 712	8.20 8.21 8.21 1.03	139.24 139.52 139.80 10.98	13924 13952 13980 1098	12.78 12.81 12.84 1.01
	35		/														

# 10.5 Tank and Void Capacity Tables (see also Appendix J)

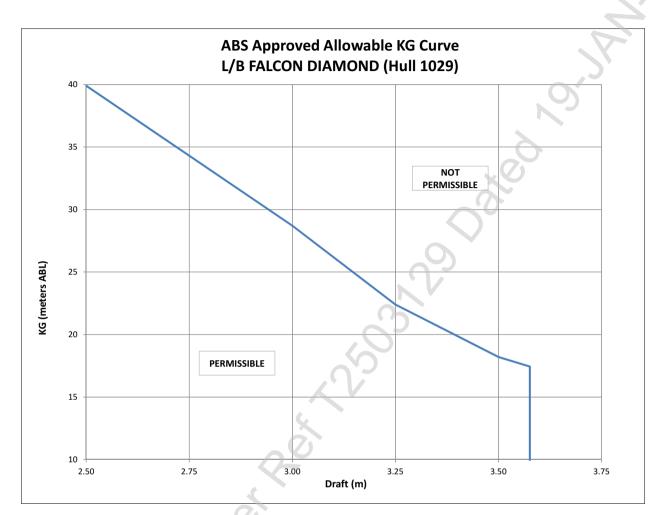
arine, LLC AMOND	•	erating Mar o: 0722-01			Janı	uary 12, 2024	1			20
k and Void Capacit	ty Tables (see								A	
			1			1		FOLAT		
	Permeability	Spec.	Weight	Volume	LCG	TCG	VCG	FSMT	FSML	
	++	Grav.	MT	m^3	m (+ AFT	m (+ Stbd	m	m*M-	m*M-	
		1			of FP)	OCL)	(+ABL)	tons	tons	
Ballast 1P	0.98	1.025	178.772	174.412	3.756	-4.721	2.737	435	166	
Ballast 1S	0.98	1.025	178.772	174.411	3.756	4.721	2.737	435	166	
Ballast 2P	0.98	1.025	164.170	160.166	38.401	-15.881	2.417	191	72	
Ballast 2S	0.98	1.025	164.170	160.166	38.401	15.881	2.417	191	72	
Ballast 3P	0.98	1.025	311.745	304.141	51.563	-4.774	2.353	533	300	
Ballast 3S	0.98	1.025	311.745	304.141	51.563	4.774	2.353	533	300	
Ballast 4P	0.98	1.025	69.830	68.127	58.595	-14.462	3.135	28	112	
Ballast 4S	0.98	1.025	81.020	79.044	58.604	14.184	3.162	40	128	
Fuel Day Tank Port	0.98	0.867	10.767	12.419	24.000	-13.200	3.500	2	2	
Fuel Day Tank Stbd	0.98	0.867	10.767	12.419	24.000	13.200	3.500	2	2	
Dirty Oil Tank	0.98	0.867	13.209	15.235	29.400	0.000	0.600	12	12	
Fuel Oil Port	0.98	0.867	128.071	147.717	22.700	-16.106	2.327	161	61	
Fuel Oil Stbd	0.98	0.867	128.071	147.717	22.700	16.106	2.327	161	61	
Fresh Water Port	0.98	1.000	139.421	139.421	30.000	-17.168	2.069	279	238	
Fresh Water Stbd	0.98	1.000	139.421	139.421	30.000	17.168	2.069	279	238	
Grey Water Stbd	0.98	1.000	9.541	9.541	21.600	5.984	0.637	9	4	
Lube Oil Stbd	0.98	0.910	6.932	7.618	25.800	0.900	0.601	2	6	
Oily Water Port	0.98	1.000	7.618	7.618	25.800	-0.900	0.601	2	7	
Zero Discharge 1P	0.98	1.000	48.419	48.419	4.207	-17.848	2.801	14	33	
Zero Discharge 1S	0.98	1.000	48.419	48.419	4.207	17.848	2.801	14	33	
Zero Discharge 2P	0.98	1.000	69.331	69.331	58.508	-17.979	3.192	27	107	
Zero Discharge 2S	0.98	1.000	69.331	69.331	58.508	17.979	3.192	27	107	

Table 10-2: Tank Capacity Table

	Dermos	1					VCC		TCA 4
	Permea bility	Spec. Grav.	Weight	Volume	LCG	TCG	VCG	FSMT	FSM
	Sincy	Grav.	MT	m^3	m (+	m (+ Stbd	m	m*M-	m*M
					AFT of	OCL)	(+ABL)	tons	tons
					FP)			6	
Void 1P	0.98	1.025	48.155	46.981	3.977	-14.687	2.825	12	39
Void 1S	0.98	1.025	48.155	46.981	3.977	14.687	2.825	12	39
Void 2P	0.98	1.025	158.868	154.993	13.200	-4.698	0.628	1066	2400
Void 2S	0.98	1.025	158.868	154.993	13.200	4.698	0.628	1066	2400
Void 3P	0.98	1.025	154.405	150.639	13.200	-10.798	2.376	17	600
Void 3S	0.98	1.025	154.405	150.639	13.200	10.798	2.376	17	600
Void 4P	0.98	1.025	155.145	151.361	13.199	-14.001	3.258	82	1048
Void 4S	0.98	1.025	155.145	151.361	13.199	14.001	3.258	82	1048
Void 5P	0.98	1.025	130.283	127.105	13.199	-18.072	3.275	51	898
Void 5S	0.98	1.025	130.283	127.105	13.199	18.072	3.275	51	898
Void 6P	0.98	1.025	202.770	197.825	28.578	6.886	0.629	2926	4333
Void 6S	0.98	1.025	193.000	188.293	28.931	6.932	0.628	2906	3865
Void 7P	0.98	1.025	23.818	23.237	25.800	-17.168	2.069	48	1
Void 7S	0.98	1.025	23.818	23.237	25.800	17.168	2.069	48	1
Void 8P	0.98	1.025	18.722	18.266	34.800	-18.899	2.443	1	2
Void 8S	0.98	1.025	18.722	18.266	34.800	18.899	2.443	1	2
Void 9P	0.98	1.025	210.349	205.218	38.400	-4.774	2.328	355	89
Void 9S	0.98	1.025	210.349	205.218	38.400	4.774	2.328	355	89
Void 10P	0.98	1.025	315.468	307.773	44.400	-4.774	2.328	533	300
Void 10S	0.98	1.025	315.468	307.774	44.400	4.774	2.328	533	300
Void 11P	0.98	1.025	205.148	200.145	45.560	-10.797	2.386	22	1425
Void 12P	0.98	1.025	156.734	152.911	47.976	-14.004	3.243	82	1049
Void 12S	0.98	1.025	156.734	152.911	47.976	14.004	3.243	82	1049
Void 13P	0.98	1.025	131.268	128.066	47.968	-18.075	3.259	51	894
Void 13S	0.98	1.025	131.268	128.066	47.968	18.075	3.259	51	894
Void 14S	0.98	1.025	47.562	46.403	45.417	10.792	0.683	22	1422

1/12/2024

## 10.6 KG Allowable versus Mean Draft Curve



#### Figure 10-1: ABS Allowable KG Curves

	ALLOWA	ABLE KG CUR	<b>VE</b>
	Displacement	DRAFT	KG <sub>A</sub>
	(MT)	(m)	(m)
	4941	2.50	39.9
X	6173	3.00	28.7
5	6792	3.25	22.4
5	7413	3.50	18.2
	7602	3.576	17.44
	Table 10 4 AP	C Alleria bla 10	

Table 10-4: ABS Allowable KG Values

See Stability Support Calculations.

Š

## 10.7 Sample Afloat Loading Conditions

- 10.7.1 The following sample loading conditions have been developed as examples of typical afloat conditions: (Note: Elevated conditions must comply with the requirements and limits discussed in Sections 6, 7, and 8 of this Manual.)
  - Minimum Operating Condition (MOC) Lightship (The weight of the ship including hull, machinery, outfit, equipment, and liquids in machinery), 10% fuel & fresh water, ballasted to minimize trim and heel
  - Light Deck Cargo (LDC) Light Deck Cargo (100 MT); approximately 35% fuel & fresh water, deck cargo
  - 3. Loaded Condition Afloat (LCA)
    - LCA\_454 454 MT variable load; approximately 35% fuel & fresh water, deck cargo
    - LCA\_709 709 MT variable load; approximately 35% fuel & fresh water, deck cargo
  - 4. Load Line Condition (LL) Maximum operating draft
  - 5. Helideck Operations (HDO)
    - HDO\_454 454 MT variable load; approximately 35% fuel & fresh water, deck cargo, and helicopter
    - HDO\_709 709 MT variable load; approximately 35% fuel & fresh water, deck cargo, and helicopter

Allowable VCG vs. Draft Curve with the loading conditions are plotted on the following page.

1/12/2024

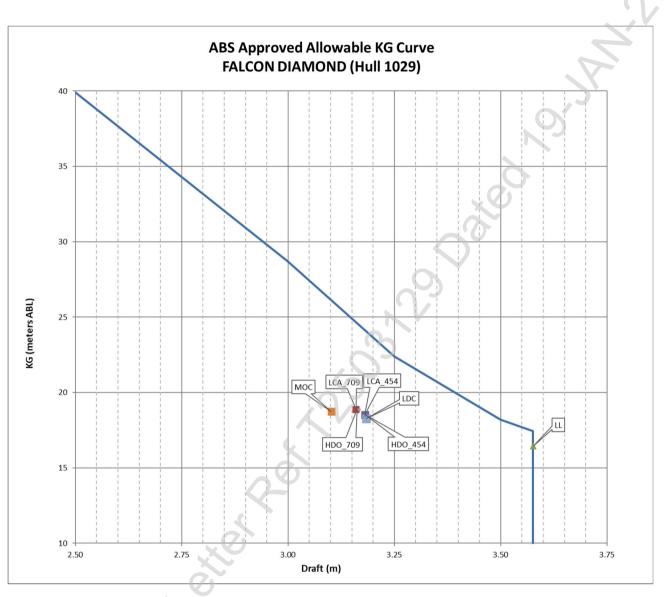


Figure 10-2: ABS Allowable KG Curves with Loading Conditions

# **CONDITION 1: Minimum Operating Condition**

ondition: FALCON DIAMOND - (1) MINIMUM OPERATI		ON					$\sim$
COLUMN →	1	2	3	4	5	6	7
e m	WEIGHT (MT)	LCG (m aft FR0)	L-MOM (MT-m)	TCG (m from CL, +STBD)	T-Mom (MT-m)	VCG (m ABL)	V-MOM (MT-m)
IGHTSHIP	5870.87	28.00	164,361	-0.50	-2,906	20.11	118086.
IGHTSHIP ADJUSTMENTS	4.00	31.25	125	0.00	0	8.15	33
REW, EFFECTS, & STORES	5.00	17.43	87	0.00	0	13.60	68
FFSHORE WORKERS, EFFECTS, & STORES	20.00	17.43	349	0.00	0	13.60	272
OTAL DECK CARGO (from DECK CARGO LOADING							
ORM)	0.00	0.00	0	0.00	0	0.00	0
ANK LIQUIDS IN VESSEL'S TANKS (from TANK DADING FORM)	525.59		26,571		1,642		1,236
OTAL FSM OF ALL SLACK TANKS (from TANK LOADING ORM and DECK CARGO LOADING FORM)			<u> </u>				909
TOTALS:	6,425.46		191,492		-1,264		120,605
	Vessel	Loading Calculat	<u>ions</u>				
(1) LCG = (Total Col. 3 / Total Col. 1) =	191,492	/ 6,425.46	= 29.80	m aft of FR	0		
(2) TCG = (Total Col. 5 / Total Col. 1) =	-1,264	/ 6,425.46	= -0.20	m from CL (+	+STBD)		
(3) KG = VCG = (Total Col. 7 / Total Col. 1) =	120,605	/ 6,425.46	= 18.77	m ABL	NOTE: INCL	UDES FSE	
(4) DISPLACEMENT = Total	Column 1 =	6,425.46	MT				
(5) MEAN SW WATER DRAFT (from Hydrostatic Pro	operties) =	3.10	m ABL				
		Loading condition	d/or decrease dec orms and check KC	k cargo or take ot Gagain.	her corrective	action.	
HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy	(6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9)	= 62.40 = 30.73 = 12.31 = 121.25 = 10.40	m m aft of FR MT-m m ABL MT-m m aft of FR	0	л.		
(12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) )</u> (15) MEAN DRAFT @ TRANSOM ( <b>15A)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4</b> ]	$R = (1) - (7)$ $(10) \times 1000 ]$ $((6) - (11))$ $(6)$ $= (13) + (14)$	= <u>-0.93</u> = <u>-0.57</u> = <u>3.38</u> = <u>2.81</u>	_ m _ m (+Aft/-Fv _ m ABL _ m ABL _ <b>m ABL</b>	vd)		Average Dra d TRANSOM	fts
(17) MOMENT TO HEEL 1mm, MH1mm (from Hy	(16) BEAM (drostatics) drostatics)	8.11	m MT-m m ABL MT-m			Calculate	

				TANK LOADI	NG FORM					
Condition: FALCON DIAMOND -	(1) Minimum O	perating Condit	ion							
COLUMN →	0	1	2	3	4	5	6	7	8	9
	FILL	WEIGHT	LCG m at	ft of FR 0	TCG (m +/	/- from CL)	VCG (m abo	ve BASELINE)	TRANS FSM	LONG'L FSM
TANK	(%)	(MT)	LCG	L-MOM	TCG (+Stbd)	T-MOM	VCG	V-MOM	(MT-m)	(MT-m)
	Enter Value	Enter Value	Enter Value	Col 1 X Col 4	Enter Value	Col 1 X Col 6	Enter Value	Col 1 X Col 2	Enter Value	Enter Value
Ballast #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Stbd	100	311.75	51.56	16,074.51	4.77	1,488.27	2.35	733.54	0.00	0.00
Ballast #4 Port	100	69.83	58.60	4,091.69	-14.46	-1,009.88	3.14	218.92	0.00	0.00
Ballast #4 Stbd	100	81.02	58.60	4,748.10	14.18	1,149.19	3.16	256.19	0.00	0.00
Zero Discharge #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Day Tank Port	10	1.08	24.00	25.84	-13.20	-14.21	2.51	2.70	2.00	2.00
Day Tank Stbd	10	1.08	24.00	25.84	13.20	14.21	2.51	2.70	2.00	2.00
Fuel Oil Port	10	12.81	22.80	292.01	-15.69	-200.97	0.44	5.57	161.00	61.00
Fuel Oil Stbd	10	12.81	22.80	292.01	15.69	200.97	0.44	5.57	161.00	61.00
Fresh Water Port	10	13.94	30.00	418.26	-15.57	-217.06	0.36	5.02	279.00	238.00
Fresh Water Stbd	10	13.94	30.00	418.26	15.57	217.06	0.36	5.02	279.00	238.00
Greywater	25	2.39	21.60	51.52	5.94	14.16	0.21	0.51	9.00	4.00
Dirty Oil	10	1.32	29.40	38.83	0.00	0.00	0.06	0.08	12.00	12.00
Lube Oil	25	1.73	25.80	44.71	0.90	1.56	0.15	0.26	2.00	6.00
Oily Water	25	1.90	25.80	49.14	-0.90	-1.71	0.15	0.29	2.00	7.00
TOTAL (Record here and on Vessel Loading Form)	0	525.59		26570.73		1641.58		1236.37	909.00	631.00

#### INSTRUCTIONS FOR THE TANK LOADING FORM

For each of the vessel's tanks that contain liquid, determined and enter the following on the Tank Loading Form:

1. Take soundings of each tank and enter the liquid level in each tank in column 0 of the TANK LOADING FORM.

2. Consult the TANK CAPACITY TABLES and enter the weight of the liquid in column 1, the LCG of the liquid in column 2, the TCG of the liquid in column 4, and the VCG of the liquid in column 6 corresponding to the sounding. Enter the transverse and longitudinal free surface moments into columns 8 and 9, respectively. If the actual sounding falls between two soundings listed the TANK CAPACITY TABLES, enter the values associated with the higher of the two soundings on the TANK LOADING FORM.

3. Sum the weights in column 1 to obtain the total weight of the liquids in the tanks. Enter this TOTAL on the TANK LOADING FORM and the VESSEL LOADING FORM. 4. Multiply each weight in column 1 by its corresponding LCG in column 2 to obtain the longitudinal moment of the weight and enter this value in column 3. Sum the longitudinal moments in column 3 to obtain the total longitudinal moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

5. Multiply each weight in column 1 by its corresponding TCG in column 4 to obtain the transverse moment of the weight and enter this value in column 5. Sum the transverse moments in column 5 to obtain the total transverse moment of the liquids in the tanks. Note the starboard moments are positive and the port moments are negative. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

6. Multiply each weight in column 1 by its corresponding VCG in column 6 to obtain the vertical moment of the weight and enter this value in column 7. Sum the vertical moments in column 7 to obtain the total vertical moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

7. Individually sum the free surface moments in columns 8 and 9 to obtain the total transverse and longitudinal free surface moments of the internal tanks. Enter the maximum of these two TOTALS on the TANK LOADING FORM. Add this value to the DECK TANKS MAX FSM TOTAL from the DECK CARGO LOADING FORM and enter this value into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

1/12/2024

# **CONDITION 2: 100 MT Load on Deck**

Condition: FALCON DIAMOND - (2) 100 MT on Deck COLUMN $\rightarrow$	1	2	3	4	5	6	7
	I	Z	3	4 TCG	5	0	
	WEIGHT	LCG	L-MOM	(m from CL,	T-Mom	VCG	V-MON
tem	(MT)	(m aft FRO)	(MT-m)	+STBD)	(MT-m)	(m ABL)	(MT-m
IGHTSHIP	5870.87	28.00	164,361	-0.50	-2,906	20.11	118086.
IGHTSHIP ADJUSTMENTS	4.00	31.25	125	0.00	0	8.15	33
CREW, EFFECTS, & STORES	5.00	17.43	87	0.00	0	13.60	68
					0		
DFFSHORE WORKERS, EFFECTS, & STORES TOTAL DECK CARGO (from DECK CARGO LOADING	20.00	17.43	349	0.00		13.60	272
FORM)	100.00	55.20	5,520	6.00	600	6.60	660
TANK LIQUIDS IN VESSEL'S TANKS (from TANK	100100	55120	0,020	0.00		0.00	
LOADING FORM)	628.89		29,324		2,349		1,344
TOTAL FSM OF ALL SLACK TANKS (from TANK LOADING			,				
FORM and DECK CARGO LOADING FORM)							909
TOTALS:	6,628.76		199,766		43		121,372
	امددما	Loading Calculat	ions	<u> </u>			, í
(1)   CC - (Tatal Cal 2 (Tatal Cal 1) - (1)   CC - (1		-		moft of FD	0		
(1) LCG = (Total Col. 3 / Total Col. 1) =		/ 6,628.76	= 30.14	m aft of FR			
(2) TCG = (Total Col. 5 / Total Col. 1) =	43	/ 6,628.76	= 0.01	m from CL (-	⊦STBD)		
(3) KG = VCG = (Total Col. 7 / Total Col. 1) =	121,372	/ 6,628.76	= 18.31	m ABL	NOTE: INCL	UDES FSE	
(4) DISPLACEMENT = Total	Column 1 =	6,628.76	MT				
(5) MEAN SW WATER DRAFT (from Hydrostatic Pr	operties) =	3.18	m ABL				
CHECK STABILITY:							
Does the loading condition's KG fall be	low the curv	es of "Allowable KO	G -vs- Displace	ment?"			
-					ments		
YES	x	_ Loading condition	on meets the st	ability require			
YES		Loading condition	on meets the st on DOES NOT n	ability requirent neet the stability	ty criteria.	action.	
YES	x	_ Loading condition	on meets the st on DOES NOT n d/or decrease dec	ability require neet the stabili k cargo or take ot	ty criteria.	action.	
YES	x	Loading condition	on meets the st on DOES NOT n d/or decrease dec rms and check KC	ability required neet the stabili k cargo or take ot again.	ty criteria. her corrective	action.	
YES	x	Loading condition	on meets the st on DOES NOT n d/or decrease dec rms and check KC	ability required neet the stabili k cargo or take ot again.	ty criteria. her corrective	action.	
YES	x	Loading condition Loading condition Increase ballast and Correct Loading for HEEL, AND DRAFTS	on meets the st on DOES NOT n d/or decrease dec rms and check KC	ability required neet the stabili k cargo or take ot again.	ty criteria. her corrective	action.	
YES	x  THE TRIM, F (6) LOA	Loading condition Loading condition Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40	on meets the st on DOES NOT n d/or decrease dec rms and check KC AT THE BOW	ability require neet the stabili k cargo or take ot a again. AND TRANSON	ty criteria. her corrective	action.	
YES NO	x : THE TRIM, F (6) LOA ydrostatics)	Loading condition Loading condition Increase ballast and Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.76	on meets the st on DOES NOT n d/or decrease dec rms and check KC AT THE BOW	ability require neet the stabili k cargo or take ot a again. AND TRANSON	ty criteria. her corrective	action.	
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H	X THE TRIM, F (6) LOA ydrostatics) rdrostatics)	Loading condition Loading condition Increase ballast and Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.76 = 12.35	on meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW m m m aft of FR	ability require neet the stabili k cargo or take ot a again. AND TRANSON	ty criteria. her corrective	action.	
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from H)	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics)	Loading condition Loading condition Increase ballast and Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.76 = 12.35	on meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW m m aft of FR MT-m	ability require neet the stabili k cargo or take ot a again. AND TRANSON	ty criteria. her corrective	action.	
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44	on meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW m m aft of FR MT-m m ABL	ability required neet the stabili k cargo or take ot 3 again. AND TRANSON	ty criteria. her corrective	action.	
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H	X THE TRIM, f (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics)	Loading condition Loading condition Increase ballast and Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m	ability required neet the stabili k cargo or take of 3 again. AND TRANSON	ty criteria. her corrective	action. Average Draf	fts
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H (12) TRIM LEVE	X THE TRIM, f (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) R = (1) - (7)	Loading condition Loading condition Increase ballast and Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63	m mets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR	ability required neet the stabili k cargo or take of 3 again. AND TRANSON	ty criteria. her corrective 7. Calculate 4		fts
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from H) (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) R = (1) - (7) (10) X 1000 ]	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40	m marked of the stand d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR m (+Aft/-Fw	ability required neet the stabili k cargo or take of 3 again. AND TRANSON	ty criteria. her corrective 7. Calculate 4	Average Draf	fts
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H (12) TRIM LEVE	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) ER = (1) - (7) (10) X 1000 ] X [(6) - (11)]	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40	m mets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR	ability required neet the stabili k cargo or take of 3 again. AND TRANSON	ty criteria. her corrective 7. Calculate 4	Average Draf	fts
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from H) (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [ (14) MEAN DRAFT @ BOW = (5) - (13) 2	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) ER = (1) - (7) (10) X 1000 ] X [(6) - (11)] (6)	Loading condition Loading condition Increase ballast and Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40 = 3.38	m mon meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR m (+Aft/-Fw m ABL	ability required neet the stabili k cargo or take of 3 again. AND TRANSON	ty criteria. her corrective 7. Calculate 4	Average Draf	íts
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from H) (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H (12) TRIM = (8) (13) TRIM = [(4) X (12)] / [ (14) MEAN DRAFT @ BOW = (5) - ( <u>13)</u> (15) MEAN DRAFT @ TRANSOM	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) ER = (1) - (7) (10) X 1000 ] X [(6) - (11)] (6) = (13) + (14)	Loading condition Loading condition Increase ballast and Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40 = 3.38 = 2.98	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL	ability required neet the stabili k cargo or take of 3 again. AND TRANSON	ty criteria. her corrective 7. Calculate 4	Average Draf	ŕts
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from H) (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [ (14) MEAN DRAFT @ BOW = (5) - (13) 2	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) ER = (1) - (7) (10) X 1000 ] X [(6) - (11)] (6) = (13) + (14)	Loading condition Loading condition Increase ballast and Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40 = 3.38 = 2.98	m mon meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR m (+Aft/-Fw m ABL	ability required neet the stabili k cargo or take of 3 again. AND TRANSON	ty criteria. her corrective 7. Calculate 4	Average Draf	íts
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from H) (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H (12) TRIM = (8) (13) TRIM = [(4) X (12)] / [ (14) MEAN DRAFT @ BOW = (5) - ( <u>13)</u> (15) MEAN DRAFT @ TRANSOM	x (6) LOA ydrostatics) ydrostatics) ydrostatics) ydrostatics) (10) X 1000 ] X [(6) - (11)] (6) = (13) + (14) ] + (14) + 0.9	Loading condition Loading condition Increase ballast and Correct Loading for Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40 = 3.38 = 2.98 = 3.90	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL	ability required neet the stabili k cargo or take of 3 again. AND TRANSON	ty criteria. her corrective 7. Calculate 4	Average Draf	fts
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from H) (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H (12) TRIM = [8) X [( (11) LCF (from H (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [ (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (15A)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4	x (6) LOA (7) LOA (7) Vdrostatics) (7) Vdrostatics) (7) Vdrostatics) (7)	Loading condition Loading condition Increase ballast ann Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40 = 3.38 = 2.98 = 3.90 = 39.60	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL	ability required neet the stabili k cargo or take of 3 again. AND TRANSON	ty criteria. her corrective 7. Calculate 4	Average Draf	îts
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from H (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H (12) TRIM = [4) X (12)] / [ (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (15A)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H	x (6) LOA (7) LOA (7) Vdrostatics) (7) Vdrostatics) (7) Vdrostatics) (7)	Loading condition Loading condition Increase ballast ann Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40 = 3.38 = 2.98 = 3.90 = 39.60 = 8.12	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m aft of FR MT-m m aft of FR m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL	ability required neet the stabili k cargo or take of 3 again. AND TRANSON	ty criteria. her corrective 7. Calculate 4	Average Draf	fts
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from H (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [ (14) MEAN DRAFT @ BOW = (5) - ( <u>13)</u> X (15) MEAN DRAFT @ TRANSOM (15A)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H (18) KMT (from Hy	x (6) LOA (7) Varostatics) (7) Varostatics)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40 = 3.38 = 2.98 = 3.90 = 8.12 = 50.25	on meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL	ability required neet the stabili k cargo or take of 3 again. AND TRANSON	ty criteria. her corrective 7. Calculate 4	Average Dra1 d TRANSOM	
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [ (14) MEAN DRAFT @ DOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (15A)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18)	x (6) LOA ydrostatics) ydrostatics) ydrostatics) ydrostatics) yerostatics) (10) X 1000 ] (10) X 1000 ] (10) X 1000 ] (10) X 1000 ] (11) + (14) (14) + (14) (16) BEAM ydrostatics) ydrostatics) ) - (3) ] / (18)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40 = 3.38 = 2.98 = 3.90 = 8.12 = 50.25 = 5.16	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m aft of FR MT-m m aft of FR MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m ABL m ABL	ability required neet the stability k cargo or take of 3 again. AND TRANSON 0 0 vd)	ty criteria. her corrective 7. Calculate 4	Average Dra1 d TRANSOM Calculate	Port & Stb
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from H (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [ (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (15A)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18) (20) HEEL LEV	x (6) LOA (7) LOA (7) Vdrostatics) (7) Vdrostatics) (7) Vdrostatics) (7)	Loading condition Loading condition Increase ballast anno Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40 = 3.38 = 2.98 = 3.90 = 39.60 = 8.12 = 50.25 = 5.16 = 0.01	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m ABL m ABL m ABL m ABL m ABL m ABL m ABL m ABL m from CL (	ability required neet the stability k cargo or take of 3 again. AND TRANSON 0 0 vd)	ty criteria. her corrective 7. Calculate 4	Average Draf d TRANSOM Calculate _ Drafts @ E	Port & Stb
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [ (14) MEAN DRAFT @ DOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (15A)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18)	x (6) LOA (7) LOA (7) Vdrostatics) (7) Vdrostatics) (7) Vdrostatics) (7)	Loading condition Loading condition Increase ballast and Correct Loading for 4EEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40 = 3.38 = 2.98 = 3.90 = 8.12 = 50.25 = 5.16 = 0.01 = 0.01	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m ABL m Frem m ABL m (+Stbd)	ability required neet the stability k cargo or take of again. AND TRANSON 0 0 vd) +Stbd)	ty criteria. her corrective: Calculate A @ BOW an	Average Dra1 d TRANSOM Calculate	Port & Stb
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [ (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (15A)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18 (20) HEEL LEV (21) HEEL = [(4) X (20)]/ (22) DRAFT @ BOW = (14) +/- (21) / 2:	x (6) LOA (7) LOA (7) Vdrostatics) (7) Vdrostatics) (7) Vdrostatics) (7)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 = 10.44 = 31.85 = -0.63 = -0.40 = 3.38 = 2.98 = 3.90 = 8.12 = 50.25 = 5.16 = 0.01 = 0.01 = 3.38	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m ABL m ABL m ABL m ABL m ABL m ABL m ABL m ABL m from CL (	Ability required neet the stability k cargo or take of again. AND TRANSON 0 0 vd) +Stbd) = <u>3.38</u>	ty criteria. her corrective 7. Calculate 4	Average Draf d TRANSOM Calculate _ Drafts @ E	Port & Stb
YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from H (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [ (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (15A)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18 (20) HEEL LEV (21) HEEL = [(4) X (20])/	x	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.05 10.44 = 31.85 = -0.63 = -0.40 = 3.38 = 2.98 = 3.90 = 8.12 = 50.25 = 5.16 = 0.01 = 0.01 = 3.38 = 2.98	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m ABL m ABL m (+Stbd) Port	Ability required neet the stability k cargo or take of again. AND TRANSON 0 0 vd) +Stbd) = 3.38 = 2.98	ty criteria. her corrective: Calculate A @ BOW an	Average Draf d TRANSOM Calculate _ Drafts @ E	Port & Stb

0

				TANK LOADI	NG FORM					
Condition: FALCON DIAMOND -	(2) 100 MT on D	)eck								
$COLUMN \rightarrow$	0	1	2	3	4	5	6	7	8	9
	FILL	WEIGHT	LCG m a	ft of FR 0	TCG (m +/	/- from CL)	VCG (m abo	ve BASELINE)	TRANS FSM	LONG'L FSM
TANK	(%)	(MT)	LCG	L-MOM	TCG (+Stbd)	T-MOM	VCG	V-MOM	(MT-m)	(MT-m)
	Enter Value	Enter Value	Enter Value	Col 1 X Col 4	Enter Value	Col 1 X Col 6	Enter Value	Col 1 X Col 2	Enter Value	Enter Value
Ballast #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Stbd	100	311.75	51.56	16,074.51	4.77	1,488.27	2.35	733.54	0.00	0.00
Ballast #4 Port	100	69.83	58.60	4,091.69	-14.46	-1,009.88	3.14	218.92	0.00	0.00
Ballast #4 Stbd	100	81.02	58.60	4,748.10	14.18	1,149.19	3.16	256.19	0.00	0.00
Zero Discharge #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Day Tank Port	35	3.77	24.00	90.44	-13.20	-49.74	2.78	10.50	2.00	2.00
Day Tank Stbd	35	3.77	24.00	90.44	13.20	49.74	2.78	10.50	2.00	2.00
Fuel Oil Port	27	34.58	22.80	788.44	-15.82	-547.15	0.78	26.92	161.00	61.00
Fuel Oil Stbd	27	34.58	22.80	788.44	15.82	547.15	0.78	26.92	161.00	61.00
Fresh Water Port	14	19.52	30.00	585.57	-15.66	-305.74	0.41	8.03	279.00	238.00
Fresh Water Stbd	45	62.74	30.00	1,882.18	16.15	1,013.29	0.82	51.51	279.00	238.00
Greywater	25	2.39	21.60	51.52	5.94	14.16	0.21	0.51	9.00	4.00
Dirty Oil	10	1.32	29.40	38.83	0.00	0.00	0.06	0.08	12.00	12.00
Lube Oil	25	1.73	25.80	44.71	0.90	1.56	0.15	0.26	2.00	6.00
Oily Water	25	1.90	25.80	49.14	-0.90	-1.71	0.15	0.29	2.00	7.00
TOTAL (Record here and on Vessel Loading Form)	0	628.89		29324.01		2349.13		1344.14	909.00	631.00

#### INSTRUCTIONS FOR THE TANK LOADING FORM

For each of the vessel's tanks that contain liquid, determined and enter the following on the Tank Loading Form:

1. Take soundings of each tank and enter the liquid level in each tank in column 0 of the TANK LOADING FORM.

2. Consult the TANK CAPACITY TABLES and enter the weight of the liquid in column 1, the LCG of the liquid in column 2, the TCG of the liquid in column 4, and the VCG of the liquid in column 6 corresponding to the sounding. Enter the transverse and longitudinal free surface moments into columns 8 and 9, respectively. If the actual sounding falls between two soundings listed the TANK CAPACITY TABLES, enter the values associated with the higher of the two soundings on the TANK LOADING FORM.

3. Sum the weights in column 1 to obtain the total weight of the liquids in the tanks. Enter this TOTAL on the TANK LOADING FORM and the VESSEL LOADING FORM. 4. Multiply each weight in column 1 by its corresponding LCG in column 2 to obtain the longitudinal moment of the weight and enter this value in column 3. Sum the longitudinal moments in column 3 to obtain the total longitudinal moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

5. Multiply each weight in column 1 by its corresponding TCG in column 4 to obtain the transverse moment of the weight and enter this value in column 5. Sum the transverse moments in column 5 to obtain the total transverse moment of the liquids in the tanks. Note the starboard moments are positive and the port moments are negative. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

6. Multiply each weight in column 1 by its corresponding VCG in column 6 to obtain the vertical moment of the weight and enter this value in column 7. Sum the vertical moments in column 7 to obtain the total vertical moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

7. Individually sum the free surface moments in columns 8 and 9 to obtain the total transverse and longitudinal free surface moments of the internal tanks. Enter the maximum of these two TOTALS on the TANK LOADING FORM. Add this value to the DECK TANKS MAX FSM TOTAL from the DECK CARGO LOADING FORM and enter this value into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

	-	1	DECKCARO	O LOADING						
Condition: FALCON DIAMOND - (2) 100 N	IT on Deck									
COLUMN>	• 1	2	3	4	5	6	7	8	9	10
ITEM	WEIGHT	LCG (m a	ft of FR 0 )	TCG (m +/	- from CL)	VCG above	MAIN DK	VCG (m ab	ove BL)	DECK TAN
(Include deck tanks & contents as	(MT)	LCG	L-MOM	TCG (+ STBD)	T-MOM	MAIN DECK	to BL	VCG	V-MOM	MAX FSN
separate line items)	Enter Value	Enter Value	Col 1 x Col 2	Enter Value	Col 1 x Col 4	Enter Value		Col 6 + Col 7		(MT-m)
Deck Cargo	100.00	55.20	5520.00	6.00	600.00	2.00	+ 4.6=	6.60	660.00	
							+ 4.6=			
							+ 4.6=			
							+ 4.6=		5	
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=	0		
							+ 4.6=			
							+4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
						<b>O</b>	+ 4.6=			
					(		+ 4.6=			
							+ 4.6=			
							+ 4.6=			
						2	+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
				-			+ 4.6=			
TOTAL (Record here and on Vessel Loading Form)	100.00		5520.00		600.00		1 4.0-		660.00	0.00

1. A complete list of non-tank cargoesis to be entered above with weight, LCG, TCG, and VCG for each item in columns 1, 2, 4 and 6.

2. Calculate the longitudinal moment for each cargo item by multiplying columns 1 and 2 for each item. Calculate the transverse moment for each cargo item by multiplying columns 1 and 4 for each item. Calculate the vertical moment for each cargo item by multiplying columns 1 and 8 for each item.

3. Sum columns 1, 3, 5, and 9 and enter the values in the TOTAL row. These totals are to be entered in the Deck Cargo Loading row of the VESSEL LOADING FORM.

4. Sum column 10 and enter the value in the TOTAL row. This total is to be be added to the TANK LOADING FORM FSC MOM TOTAL and entered into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

1/12/2024

# CONDITION 3A: 454 MT Variable Load

Condition: FALCON DIAMOND - (3A) LOADED CONDITIO							
COLUMN →	1	2	3	4	5	6	7
tem	WEIGHT (MT)	LCG (m aft FR0)	L-MOM (MT-m)	TCG (m from CL, +STBD)	T-Mom (MT-m)	VCG (m ABL)	V-MOM (MT-m)
IGHTSHIP				-			, ,
	5870.87	28.00	164,361 125	-0.50	-2,906 0	20.11	118086.
	4.00	31.25		0.00		8.15	33
REW, EFFECTS, & STORES	5.00	17.43	87	0.00	0	13.60	68
OFFSHORE WORKERS, EFFECTS, & STORES	20.00	17.43	349	0.00	0	13.60	272
ORM)	222.88	54.00	12,036	5.00	1,114	9.16	2,042
ANK LIQUIDS IN VESSEL'S TANKS (from TANK OADING FORM)	508.85	0 1100	22,208	5.00	1,830	5.10	859
OTAL FSM OF ALL SLACK TANKS (from TANK LOADING							
ORM and DECK CARGO LOADING FORM)							1,442
TOTALS:	6,631.60		199,165		38		122,802
	Vessel	Loading Calculat	ions	7			-
(1) LCG = (Total Col. 3 / Total Col. 1) =	199,165	/ 6,631.60	= 30.03	m aft of FR	0		
(2) TCG = (Total Col. 5 / Total Col. 1) =	38	/ 6,631.60	= 0.01	m from CL (+	-STBD)		
(3) KG = VCG = (Total Col. 7 / Total Col. 1) =		/ 6,631.60	= 18.52	-	NOTE: INCL		
		·			NOTE: INCL	ODESTSE	
(4) DISPLACEMENT = Total		6,631.60	MT				
(5) MEAN SW WATER DRAFT (from Hydrostatic Pr	operties) =	3.19	m ABL				
		es of "Allowable KG Loading condition Loading condition Increase ballast and Correct Loading for	on meets the st on DOES NOT n d/or decrease dec	ability requiren neet the stabilit k cargo or take otl	ty criteria.	action.	
Does the loading condition's KG fall be YES	x	Loading condition	on meets the st on DOES NOT n d/or decrease dec rms and check KC	ability requiren neet the stabili k cargo or take otl again.	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO	X	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS	on meets the st on DOES NOT n d/or decrease dec rms and check KC AT THE BOW	ability requiren neet the stabili k cargo or take otl again.	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO	x  THE TRIM, F (6) LOA	Loading condition     Loading condition     Increase ballast and     Correct Loading fo     IEEL, AND DRAFTS     E 62.40	on meets the st on DOES NOT n d/or decrease dec rms and check KC AT THE BOW	ability requirer neet the stabilit k cargo or take otl a again. AND TRANSOM	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H	X : THE TRIM, H (6) LOA ydrostatics)	Loading condition Loading condition Increase ballast and Correct Loading fo IEEL, AND DRAFTS  = 62.40 = 30.76	on meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR	ability requirer neet the stabilit k cargo or take otl a again. AND TRANSOM	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO	X THE TRIM, F (6) LOA ydrostatics) drostatics)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35	on meets the st on DOES NOT n d/or decrease dec rms and check KC AT THE BOW	ability requirer neet the stabilit k cargo or take otl a again. AND TRANSOM	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35	on meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m	ability requirer neet the stabilit k cargo or take otl a again. AND TRANSOM	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW m m aft of FR MT-m m ABL	ability requirer neet the stabili k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(1 (11) LCF (from Hy	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85	m mon meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR	ability requirer neet the stabilit k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective 1. Calculate /	Average Draf	íts
Does the loading condition's KG fall be YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(1 (11) LCF (from Hy (12) TRIM LEVE	X : THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) ER = (1) - (7)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73	m mon meets the st mon DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR	ability requirer neet the stability k cargo or take oth 3 again. AND TRANSOM 0	ty criteria. her corrective 1. Calculate /		fts
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(1 (11) LCF (from Hy (12) TRIM = ([4) X (12)] / [0]	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) ER = (1) - (7) (10) X 1000 ]	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73 = -0.47	m mon meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW m m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR m (+Aft/-Fv	ability requirer neet the stability k cargo or take oth 3 again. AND TRANSOM 0	ty criteria. her corrective 1. Calculate /	Average Draf	fts
Does the loading condition's KG fall be YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(1 (11) LCF (from Hy (12) TRIM LEVE	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) ER = (1) - (7) (10) X 1000 ]	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73 = -0.47	m mon meets the st mon DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR	ability requirer neet the stability k cargo or take oth 3 again. AND TRANSOM 0	ty criteria. her corrective 1. Calculate /	Average Draf	fts
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(1 (11) LCF (from Hy (12) TRIM = ([4) X (12)] / [0]	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) ER = (1) - (7) (10) X 1000 ] X [(6) - (11)] (6)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73 = -0.47 = 3.41	m mon meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW m m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR m (+Aft/-Fv	ability requirer neet the stability k cargo or take oth 3 again. AND TRANSOM 0	ty criteria. her corrective 1. Calculate /	Average Draf	íts
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X (( (11) LCF (from Hy (12) TRIM EVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) Y	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) ER = (1) - (7) (10) X 1000 ] X [(6) - (11)] (6) = (13) + (14)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73 = -0.47 = 3.41 = 2.95	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR m (+Aft/-Fw m ABL	ability requirer neet the stability k cargo or take oth 3 again. AND TRANSOM 0	ty criteria. her corrective 1. Calculate /	Average Draf	fts
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(4) (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(4) (14) MEAN DRAFT @ BOW = (5) - (13) Y (15) MEAN DRAFT @ TRANSOM	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) (10) X 1000 ] X [(6) - (11)] (6) = (13) + (14) ] + (14) + 0.9	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73 = -0.47 = 3.41 = 2.95 = <b>3.87</b>	m mon meets the st mon DOES NOT m d/or decrease dec mrms and check KC AT THE BOW // m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL	ability requirer neet the stability k cargo or take oth 3 again. AND TRANSOM 0	ty criteria. her corrective 1. Calculate /	Average Draf	fts
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from He (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from He (10) MT1mm CORRECTED = MT1mm = (8) X (( (11) LCF (from He (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ]	x (6) LOA (7) (6) LOA (7) (7) (7) (7) (7) (7) (7) (7) (7) (7)	Loading condition Loading condition Increase ballast ann Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73 = -0.73 = -0.47 = 3.41 = 2.95 = 39.60	m mon meets the st mon DOES NOT m d/or decrease dec ms and check KC AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL	ability requirer neet the stability k cargo or take oth 3 again. AND TRANSOM 0	ty criteria. her corrective 1. Calculate /	Average Draf	fts
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hi (10) MT1mm CORRECTED = MT1mm = (8) X (1 (11) LCF (from Hi (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [0 (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hi	x (6) LOA (7) (6) LOA (7) (6) LOA (7) (7) (7) (7) (7) (7) (7) (7) (7) (7)	Loading condition Loading condition Increase ballast anno Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73 = -0.73 = -0.47 = 3.41 = 2.95 = 3.87 = 39.60 = 8.12	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m aft of FR MT-m m aft of FR m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m MT-m	ability requirer neet the stability k cargo or take oth 3 again. AND TRANSOM 0	ty criteria. her corrective 1. Calculate /	Average Draf	fts
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(9) (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy	X THE TRIM, F (6) LOA ydrostatics) ydrostatics) ydrostatics) (10) X 1000 ] X [(6) - (11)] (6) = (13) + (14) ] + (14) + 0.9 (16) BEAM ydrostatics) ydrostatics)	Loading condition Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73 = -0.47 = 3.41 = 2.95 = 3.87 = 39.60 = 8.12 = 50.23	m mon meets the st mon DOES NOT m d/or decrease dec ms and check KC AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL	ability requirer neet the stability k cargo or take oth 3 again. AND TRANSOM 0	ty criteria. her corrective 1. Calculate /	Average Draf	
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hi (10) MT1mm CORRECTED = MT1mm = (8) X (1 (11) LCF (from Hi (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [0 (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hi	x (6) LOA (7) (6) LOA (7) (6) LOA (7) (7) (7) (7) (7) (7) (7) (7) (7) (7)	Loading condition Loading condition Increase ballast anno Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73 = -0.73 = -0.47 = 3.41 = 2.95 = 3.87 = 39.60 = 8.12 = 50.23 = 5.13	on meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL	ability requirem neet the stability k cargo or take oth 3 again. AND TRANSOM 0 0 vd)	ty criteria. her corrective 1. Calculate /	Average Draf d TRANSOM	Port & Stb
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(4) (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(4) (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18)	x (6) LOA (7) (6) LOA (7) (6) LOA (7) (7) (7) (7) (7) (7) (7) (7) (7) (7)	Loading condition Loading condition Increase ballast anno Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73 = -0.73 = -0.47 = 3.41 = 2.95 = 3.87 = 39.60 = 8.12 = 50.23 = 5.13 = 0.01	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m aft of FR MT-m m aft of FR MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m ABL m ABL	ability requirem neet the stability k cargo or take oth 3 again. AND TRANSOM 0 0 vd)	ty criteria. her corrective 1. Calculate /	Average Draf d TRANSOM Calculate	Port & Stb
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(9) (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(14) (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18) (20) HEEL LEV	x (6) LOA (7) (6) LOA (7) (6) LOA (7) (7) (7) (7) (7) (7) (7) (7) (7) (7)	Loading condition Loading condition Increase ballast anno Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73 = -0.73 = -0.47 = 3.41 = 2.95 = 3.87 = 39.60 = 8.12 = 50.23 = 5.13 = 0.01 = 0.01	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m aft of FR MT-m m aft of FR MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m from CL (	ability requirem neet the stability k cargo or take oth 3 again. AND TRANSOM 0 0 vd) +Stbd)	ty criteria. her corrective 1. Calculate /	Average Draf d TRANSOM Calculate Drafts @ E	Port & Stb
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(9) (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18) (20) HEEL LEV (21) HEEL = [(4) X (20)]/[	x (6) LOA (7) (6) LOA (7) (6) LOA (7) (7) (7) (7) (7) (7) (7) (7) (7) (7)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.35 = 118.01 10.42 = 31.85 = -0.73 = -0.47 = 3.41 = 2.95 = 3.87 = 39.60 = 8.12 = 50.23 = 5.13 = 0.01 = 0.01 = 3.42 = 2.95 = 3.42 = 2.95	m meets the st on DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m ABL m From CL ( m (+Stbd)	Ability requirem neet the stability k cargo or take oth again. AND TRANSOM 0 0 vd) +Stbd) = <u>3.41</u> = <u>2.94</u>	ty criteria. her corrective 1. Calculate / @ BOW an	Average Draf d TRANSOM Calculate Drafts @ E	Port & Stb

~

				TANK LOADI	NG FORM					
Condition: FALCON DIAMOND -	(3A) LOADED CO	NDITION AFLOA	AT, 454 MT VL							
COLUMN →	0	1	2	3	4	5	6	7	8	9
	FILL	WEIGHT	LCG m at	ft of FR 0	TCG (m +/	/- from CL)	VCG (m abo	ve BASELINE)	TRANS FSM	LONG'L FSM
TANK	(%)	(MT)	LCG	L-MOM	TCG (+Stbd)	T-MOM	VCG	V-MOM	(MT-m)	(MT-m)
	Enter Value	Enter Value	Enter Value	Col 1 X Col 4	Enter Value	Col 1 X Col 6	Enter Value	Col 1 X Col 2	Enter Value	Enter Value
Ballast #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Stbd	50	155.87	51.53	8,031.50	4.75	739.96	1.23	191.49	533.00	300.00
Ballast #4 Port	100	69.83	58.60	4,091.69	-14.46	-1,009.88	3.14	218.92	0.00	0.00
Ballast #4 Stbd	100	81.02	58.60	4,748.10	14.18	1,149.19	3.16	256.19	0.00	0.00
Zero Discharge #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Day Tank Port	35	3.77	24.00	90.44	-13.20	-49.74	2.78	10.50	2.00	2.00
Day Tank Stbd	35	3.77	24.00	90.44	13.20	49.74	2.78	10.50	2.00	2.00
Fuel Oil Port	35	44.82	22.80	1,022.05	-15.84	-710.07	0.94	42.16	161.00	61.00
Fuel Oil Stbd	35	44.82	22.80	1,022.05	15.84	710.07	0.94	42.16	161.00	61.00
Fresh Water Port	15	20.91	30.00	627.39	-15.68	-327.92	0.42	8.87	279.00	238.00
Fresh Water Stbd	55	76.68	30.00	2,300.45	16.49	1,264.25	1.01	77.38	279.00	238.00
Greywater	25	2.39	21.60	51.52	5.94	14.16	0.21	0.51	9.00	4.00
Dirty Oil	10	1.32	29.40	38.83	0.00	0.00	0.06	0.08	12.00	12.00
Lube Oil	25	1.73	25.80	44.71	0.90	1.56	0.15	0.26	2.00	6.00
Oily Water	25	1.90	25.80	49.14	-0.90	-1.71	0.15	0.29	2.00	7.00
TOTAL (Record here and on Vessel Loading Form)		508.85		22208.32		1829.60		859.29	1442.00	931.00

#### INSTRUCTIONS FOR THE TANK LOADING FORM

For each of the vessel's tanks that contain liquid, determined and enter the following on the Tank Loading Form:

1. Take soundings of each tank and enter the liquid level in each tank in column 0 of the TANK LOADING FORM.

2. Consult the TANK CAPACITY TABLES and enter the weight of the liquid in column 1, the LCG of the liquid in column 2, the TCG of the liquid in column 4, and the VCG of the liquid in column 6 corresponding to the sounding. Enter the transverse and longitudinal free surface moments into columns 8 and 9, respectively. If the actual sounding falls between two soundings listed the TANK CAPACITY TABLES, enter the values associated with the higher of the two soundings on the TANK LOADING FORM.

3. Sum the weights in column 1 to obtain the total weight of the liquids in the tanks. Enter this TOTAL on the TANK LOADING FORM and the VESSEL LOADING FORM. 4. Multiply each weight in column 1 by its corresponding LCG in column 2 to obtain the longitudinal moment of the weight and enter this value in column 3. Sum the longitudinal moments in column 3 to obtain the total longitudinal moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

5. Multiply each weight in column 1 by its corresponding TCG in column 4 to obtain the transverse moment of the weight and enter this value in column 5. Sum the transverse moments in column 5 to obtain the total transverse moment of the liquids in the tanks. Note the starboard moments are positive and the port moments are negative. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

6. Multiply each weight in column 1 by its corresponding VCG in column 6 to obtain the vertical moment of the weight and enter this value in column 7. Sum the vertical moments in column 7 to obtain the total vertical moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

7. Individually sum the free surface moments in columns 8 and 9 to obtain the total transverse and longitudinal free surface moments of the internal tanks. Enter the maximum of these two TOTALS on the TANK LOADING FORM. Add this value to the DECK TANKS MAX FSM TOTAL from the DECK CARGO LOADING FORM and enter this value into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

			DECK CARG	O LOADING	FORM					
CONDITION: FALCON DIAMOND - (3A) L		ITION AFLOA	r, 454 MT VL							
COLUMN>	• 1	2	3	4	5	6	7	8	9	10
ITEM	WEIGHT	LCG (m a	ft of FR 0 )	TCG (m +,	- from CL)	VCG above	MAIN DK	VCG (m ab	ove BL)	DECK TANK
(Include deck tanks & contents as	(MT)	LCG	L-MOM	TCG (+ STBD)	T-MOM	MAIN DECK	to BL	VCG	V-MOM	MAX FSM
separate line items)	Enter Value	Enter Value	Col 1 x Col 2	Enter Value	Col 1 x Col 4	Enter Value		Col 6 + Col 7		(MT-m)
Deck Cargo	222.88	54.00	12035.52	5.00	1114.40	4.56	+ 4.6=	9.16	2041.58	
							+ 4.6=			
							+ 4.6=			
							+ 4.6=		2	
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=	$\mathcal{O}$		
							+ 4.6=			
							+4.6=	r		
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
						$\mathbf{O}$	+ 4.6=			
							+ 4.6=			
							+ 4.6=			
						V	+ 4.6=			
							+ 4.6=			
							+ 4.6=			
				(			+ 4.6=			
							+ 4.6=			
							+ 4.6=			
				$\leftarrow$			+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
TOTAL (Record here and on Vessel Loading Form)	222.88		12035.52		1114.40				2041.58	0.00

For each of material carried by the vessel the following shall be determined and entered on the Deck Cargo Loading Form: 1. A complete list of non-tank cargoes is to be entered above with weight, LCG, TCG, and VCG for each item in columns 1, 2, 4 and 6.

2.Cal culate the longitudinal moment for each cargo item by multiplying columns 1 and 2 for each item. Calculate the transverse moment for each cargo item by multiplying columns 1 and 4 for each item. Calculate the vertical moment for each cargo item by multiplying columns 1 and 8 for each item.

3. Sum columns 1, 3, 5, and 9 and enter the values in the TOTAL row. These totals are to be entered in the Deck Cargo Loading row of the VESSEL LOADING FORM.

4. Sum column 10 and enter the value in the TOTAL row. This total is to be be added to the TANK LOADING FORM FSC MOM TOTAL and entered into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

1/12/2024

# CONDITION 3B: 709 MT Variable Load

ONDITION: FALCON DIAMOND - (3B) LOADED CONDITI							
COLUMN →	1	2	3	4	5	6	7
	WEIGHT (MT)	LCG (m aft FR0)	L-MOM (MT-m)	TCG (m from CL, +STBD)	T-Mom (MT-m)	VCG (m ABL)	V-MOM (MT-m)
tem IGHTSHIP			. ,				, ,
	5870.87	28.00	164,361	-0.50	-2,906	20.11	118086.
	4.00	31.25	125	0.00	0	8.15	33
REW, EFFECTS, & STORES	5.00	17.43	87	0.00	0	13.60	68
OFFSHORE WORKERS, EFFECTS, & STORES OTAL DECK CARGO (from DECK CARGO LOADING	20.00	17.43	349	0.00	0	13.60	272
OTAL DECK CARGO (ITOM DECK CARGO LOADING	530.74	54.00	28,660	4.00	2,123	9.16	4,862
CANK LIQUIDS IN VESSEL'S TANKS (from TANK OADING FORM)	149.26	0 1100	3,948		735		113
OTAL FSM OF ALL SLACK TANKS (from TANK LOADING							
ORM and DECK CARGO LOADING FORM)							909
TOTALS:	6,579.87		197,530		-48		124,343
	Vessel	Loading Calculat	ions	7			
(1) LCG = (Total Col. 3 / Total Col. 1) =	197,530	/ 6,579.87	= 30.02	m aft of FR	0		
(2) TCG = (Total Col. 5 / Total Col. 1) =	-48	/ 6,579.87	= -0.01	m from CL (+	STBD)		
(3) KG = VCG = (Total Col. 7 / Total Col. 1) =		/ 6,579.87	= 18.90		NOTE: INCL	UDES ESE	
(4) DISPLACEMENT = Total		6,579.87	MT			0020102	
(5) MEAN SW WATER DRAFT (from Hydrostatic Pr	operties) =	3.16	m ABL				
Does the loading condition's KG fall be YES		es of "Allowable K0 Loading conditio Loading conditio Increase ballast and Correct Loading fo	on meets the st on DOES NOT n d/or decrease dec	<b>ability requiren</b> neet the stability k cargo or take otl	ty criteria.	action.	
YES	x	Loading condition	on meets the st on DOES NOT n d/or decrease dec rms and check KC	<b>ability requiren</b> neet the stabili k cargo or take otl G again.	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO	x	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS	on meets the st on DOES NOT n d/or decrease dec rms and check KC AT THE BOW	<b>ability requiren</b> neet the stabili k cargo or take otl G again.	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO	X THE TRIM, F	Loading condition     Loading condition     Increase ballast and     Correct Loading fo  IEEL, AND DRAFTS      62.40	on meets the st on DOES NOT n d/or decrease dec rms and check KC AT THE BOW	tability requirer neet the stabilit k cargo or take ot 3 again. AND TRANSOM	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H	X THE TRIM, F (6) LOA ydrostatics)	Loading condition Loading condition Increase ballast and Correct Loading fo IEEL, AND DRAFTS  = 62.40 = 30.76	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR	tability requirer neet the stabilit k cargo or take ot 3 again. AND TRANSOM	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO	X THE TRIM, F (6) LOA ydrostatics) drostatics)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34	on meets the st on DOES NOT n d/or decrease dec rms and check KC AT THE BOW	tability requirer neet the stabilit k cargo or take ot 3 again. AND TRANSOM	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy	X THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m	tability requirer neet the stabilit k cargo or take ot 3 again. AND TRANSOM	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy	X THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 10.38	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW m m aft of FR MT-m m ABL	ability requirer neet the stabili k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective	action.	
Does the loading condition's KG fall be YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(1 (11) LCF (from Hy	X THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9) ydrostatics)	Loading condition Loading condition Increase ballast and Correct Loading for TEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 10.38 = 31.85	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR	ability requirer neet the stabilit k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective 1. Calculate /	Average Draf	ïts
Does the loading condition's KG fall be YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(1 (11) LCF (from Hy (12) TRIM LEVE	X THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) R = (1) - (7)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 10.38 = 31.85 = -0.74	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR	ability requirer neet the stability k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective 1. Calculate /		ïts
Does the loading condition's KG fall be YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(1 (11) LCF (from Hy	X THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) (10) X 1000 ]	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 10.38 = 31.85 = -0.74 = -0.47	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR	ability requirer neet the stability k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective 1. Calculate /	Average Draf	its
Does the loading condition's KG fall be YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(1 (11) LCF (from Hy (12) TRIM = [(4) X (12)] / [(1) [(1) [(4) X (12)] / [(1) [(1) [(1) [(1) [(1) [(1) [(1) [(1)	X THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) (10) X 1000 ]	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 10.38 = 31.85 = -0.74 = -0.47	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR m (+Aft/-Fv	ability requirer neet the stability k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective 1. Calculate /	Average Draf	its
Does the loading condition's KG fall be YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(4) (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(4) (14) MEAN DRAFT @ BOW = (5) - (13) Y (15) MEAN DRAFT @ TRANSOM	X THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) (10) X 1000 ] X [(6) - (11)] (6) = (13) + (14)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 10.38 = 31.85 = -0.74 = -0.47 = 3.39 = 2.93	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL	ability requirer neet the stability k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective 1. Calculate /	Average Draf	its
Does the loading condition's KG fall be YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [( (11) LCF (from Hy (12) TRIM EVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) Y	X THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) (10) X 1000 ] X [(6) - (11)] (6) = (13) + (14)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 10.38 = 31.85 = -0.74 = -0.47 = 3.39 = 2.93	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR m aft of FR m ABL	ability requirer neet the stability k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective 1. Calculate /	Average Draf	its
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(4) (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(4) (14) MEAN DRAFT @ BOW = (5) - (13) Y (15) MEAN DRAFT @ TRANSOM	X THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) (10) X 1000 ] X [(6) - (11)] (6) = (13) + (14) ] + (14) + 0.9	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 10.38 = 31.85 = -0.74 = -0.47 = 3.39 = 2.93 = 3.84	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL	ability requirer neet the stability k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective 1. Calculate /	Average Draf	ïts
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(4) (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(4) (14) MEAN DRAFT @ BOW = (5) - (13) Y (15) MEAN DRAFT @ TRANSOM	x (6) LOA (7) (6) LOA (7) (6) LOA (7) (7) (7) (7) (7) (7) (7) (7) (7) (7)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 = 10.38 = 31.85 = -0.74 = -0.74 = -0.47 = 3.39 = 2.93 = 3.84 = 39.60	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL	ability requirer neet the stability k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective 1. Calculate /	Average Draf	ïts
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from He (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from He (10) MT1mm CORRECTED = MT1mm = (8) X (( (11) LCF (from He (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ]	x (6) LOA (7) (6) LOA (7) (6) LOA (7) (7) (7) (7) (7) (7) (7) (7) (7) (7)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 = 10.38 = 31.85 = -0.74 = -0.74 = -0.47 = 3.39 = 2.93 = 3.84 = 39.60 = 8.12	m meets the st m DOES NOT m d/or decrease dec rms and check KC AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL	ability requirer neet the stability k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective 1. Calculate /	Average Draf	ïts
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X (( (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u> (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ]	x (6) LOA ydrostatics) ydrostatics) ydrostatics) ydrostatics) (10) X 1000 ] (10) X 1000 ] (10) X 1000 ] (10) X 1000 ] (16) = (13) + (14) ] + (14) + 0.9 (16) BEAM ydrostatics) ydrostatics)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 = 10.38 = 31.85 = -0.74 = -0.47 = 3.39 = 2.93 = 3.84 = 39.60 = 8.12 = 50.60	m meets the st m DOES NOT m d/or decrease dec mms and check KC AT THE BOW / m aft of FR MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m MT-m	ability requirer neet the stability k cargo or take otl 3 again. AND TRANSOM	ty criteria. her corrective 1. Calculate /	Average Draf	
Does the loading condition's KG fall be YES NO THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(6) (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18) (20) HEEL LEV	x (6) LOA (6) LOA (7) (6) LOA (7) (7) (7) (7) (7) (7) (7) (7) (7) (7)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 = 10.38 = 31.85 = -0.74 = -0.74 = -0.47 = 3.39 = 2.93 = 3.84 = 39.60 = 8.12 = 50.60 = 5.09 = -0.01	m meets the st m DOES NOT m d/or decrease dec mms and check KC AT THE BOW // m aft of FR MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m m from CL (	ability requirem meet the stability k cargo or take oth 3 again. AND TRANSOM 0 0 vd)	ty criteria. her corrective 1. Calculate /	Average Draf d TRANSOM Calculate Drafts @ E	Port & Stb
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(9) (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18) (20) HEEL LEV (21) HEEL = [(4) X (20)]/[	x (6) LOA (7) (6) LOA (7) (6) LOA (7) (7) (7) (7) (7) (7) (7) (7) (7) (7)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 = 10.38 = 31.85 = -0.74 = -0.74 = -0.47 = 3.39 = 2.93 = 3.84 = 39.60 = 8.12 = 50.60 = 5.09 = -0.01 = -0.01	m meets the st m DOES NOT m d/or decrease dec mms and check KC AT THE BOW // m aft of FR MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m ABL m from CL ( m (+Stbd)	Ability requirem meet the stability k cargo or take other again. AND TRANSOM 0 0 vd) +Stbd)	ty criteria. her corrective 1. Calculate / @ BOW an	Average Draf d TRANSOM Calculate	Port & Stb
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(9) (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18) (20) HEEL LEV (21) HEEL = [(4) X (20)]/[ (22) DRAFT @ BOW = (14) +/- (21) / 2:	x (6) LOA (6) LOA (7) (6) LOA (7) (7) (7) (7) (7) (7) (7) (7) (7) (7)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 = 10.38 = 31.85 = -0.74 = -0.74 = -0.47 = 3.39 = 2.93 = 3.84 = 39.60 = 8.12 = 50.60 = 5.09 = -0.01 = -0.01 = -0.01 = 3.39	m meets the st m DOES NOT m d/or decrease dec mms and check KC AT THE BOW // m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m from CL ( m (+Stbd) Port	Ability requirem neet the stability k cargo or take other again. AND TRANSOM 0 0 vd) +Stbd) = <u>3.40</u>	ty criteria. her corrective 1. Calculate <i>J</i> @ BOW an m ABL	Average Draf d TRANSOM Calculate Drafts @ E	Port & Stb
Does the loading condition's KG fall be YES NO HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hi (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(9) (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18) (20) HEEL LEV (21) HEEL = [(4) X (20)]/[	x (6) LOA (7) (6) LOA (7) (6) LOA (7) (7) (7) (7) (7) (7) (7) (7) (7) (7)	Loading condition Loading condition Increase ballast and Correct Loading for IEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.82 = 10.38 = 31.85 = -0.74 = -0.74 = -0.47 = 3.39 = 2.93 = 3.84 = 39.60 = 8.12 = 50.60 = 5.09 = -0.01 = -0.01 = 3.39 = 2.92	m meets the st m DOES NOT m d/or decrease dec mms and check KC AT THE BOW // m aft of FR MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m ABL m from CL ( m (+Stbd)	Ability requirem the stability k cargo or take oth 3 again. AND TRANSOM 0 0 0 vd) +Stbd) = <u>3.40</u> = <u>3.40</u>	ty criteria. her corrective 1. Calculate / @ BOW an	Average Draf d TRANSOM Calculate Drafts @ E	Port & Stb

				TANK LOADI	NG FORM					
CONDITION: FALCON DIAMOND	- (3B) LOADED C	ONDITION AFLO	AT, 709 MT VL							
COLUMN →	0	1	2	3	4	5	6	7	8	-9
	FILL	WEIGHT	LCG m at	ft of FR 0	TCG (m +/- from CL)		VCG (m above BASELINE)		TRANS FSM	LONG'L FSM
TANK	(%)	(MT)	LCG	L-MOM	TCG (+Stbd)	T-MOM	VCG	V-MOM	(MT-m)	(MT-m)
	Enter Value	Enter Value	Enter Value	Col 1 X Col 4	Enter Value	Col 1 X Col 6	Enter Value	Col 1 X Col 2	Enter Value	Enter Value
Ballast #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #4 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #4 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Day Tank Port	25	2.69	24.00	64.60	-13.20	-35.53	2.67	7.20	2.00	2.00
Day Tank Stbd	25	2.69	24.00	64.60	13.20	35.53	2.67	7.20	2.00	2.00
Fuel Oil Port	25	32.02	22.80	730.04	-15.82	-506.45	0.74	23.64	161.00	61.00
Fuel Oil Stbd	25	32.02	22.80	730.04	15.82	506.45	0.74	23.64	161.00	61.00
Fresh Water Port	10	13.94	30.00	418.26	-15.57	-217.06	0.36	5.02	279.00	238.00
Fresh Water Stbd	42	58.56	30.00	1,756.70	16.02	938.03	0.77	45.24	279.00	238.00
Greywater	25	2.39	21.60	51.52	5.94	14.16	0.21	0.51	9.00	4.00
Dirty Oil	10	1.32	29.40	38.83	0.00	0.00	0.06	0.08	12.00	12.00
Lube Oil	25	1.73	25.80	44.71	0.90	1.56	0.15	0.26	2.00	6.00
Oily Water	25	1.90	25.80	49.14	-0.90	-1.71	0.15	0.29	2.00	7.00
TOTAL (Record here and on Vessel Loading Form)	0	149.26		3948.45		734.98		113.07	909.00	631.00

#### INSTRUCTIONS FOR THE TANK LOADING FORM

For each of the vessel's tanks that contain liquid, determined and enter the following on the Tank Loading Form:

1. Take soundings of each tank and enter the liquid level in each tank in column 0 of the TANK LOADING FORM.

2. Consult the TANK CAPACITY TABLES and enter the weight of the liquid in column 1, the LCG of the liquid in column 2, the TCG of the liquid in column 4, and the VCG of the liquid in column 6 corresponding to the sounding. Enter the transverse and longitudinal free surface moments into columns 8 and 9, respectively. If the actual sounding falls between two soundings listed the TANK CAPACITY TABLES, enter the values associated with the higher of the two soundings on the TANK LOADING FORM.

3. Sum the weights in column 1 to obtain the total weight of the liquids in the tanks. Enter this TOTAL on the TANK LOADING FORM and the VESSEL LOADING FORM. 4. Multiply each weight in column 1 by its corresponding LCG in column 2 to obtain the longitudinal moment of the weight and enter this value in column 3. Sum the longitudinal moments in column 3 to obtain the total longitudinal moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

5. Multiply each weight in column 1 by its corresponding TCG in column 4 to obtain the transverse moment of the weight and enter this value in column 5. Sum the transverse moments in column 5 to obtain the total transverse moment of the liquids in the tanks. Note the starboard moments are positive and the port moments are negative. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

6. Multiply each weight in column 1 by its corresponding VCG in column 6 to obtain the vertical moment of the weight and enter this value in column 7. Sum the vertical moments in column 7 to obtain the total vertical moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

7. Individually sum the free surface moments in columns 8 and 9 to obtain the total transverse and longitudinal free surface moments of the internal tanks. Enter the maximum of these two TOTALS on the TANK LOADING FORM. Add this value to the DECK TANKS MAX FSM TOTAL from the DECK CARGO LOADING FORM and enter this value into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

				O LOADING	FORM					
CONDITION: FALCON DIAMOND - (3B) L	OADED COND	ITION AFLOA	T, 709 MT VL							
COLUMN>	> 1	2	3	4	5	6	7	8	9	10
ITEM	WEIGHT	LCG (m a	ft of FR 0 )	TCG (m +,	- from CL)	VCG above	MAIN DK	VCG (m ab	ove BL)	DECK TANK
(Include deck tanks & contents as	(MT)	LCG	L-MOM	TCG (+ STBD)	T-MOM	MAIN DECK	to BL	VCG	V-MOM	MAX FSM
separate line items)	Enter Value	Enter Value	Col 1 x Col 2	Enter Value	Col 1 x Col 4	Enter Value		Col 6 + Col 7		(MT-m)
Deck Cargo	530.74	54.00	28659.96	4.00	2122.96	4.56	+ 4.6=	9.16	4861.58	
							+ 4.6=			
							+ 4.6=			
							+ 4.6=		2	
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=	$\mathcal{O}$		
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
						V	+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
				ΚV			+ 4.6=			
							+ 4.6=			
			<b>.</b>	-			+ 4.6=			
							+ 4.0=			
TOTAL (Record here and on Vessel Loading Form)	530.74		28659.96		2122.96				4861.58	0.00

For each of material carried by the vessel the following shall be determined and entered on the Deck Cargo Loading Form: 1. A complete list of non-tank cargoes is to be entered above with weight, LCG, TCG, and VCG for each item in columns 1, 2, 4 and 6.

2.Cal culate the longitudinal moment for each cargo item by multiplying columns 1 and 2 for each item. Calculate the transverse moment for each cargo item by multiplying columns 1 and 4 for each item. Calculate the vertical moment for each cargo item by multiplying columns 1 and 8 for each item.

3. Sum columns 1, 3, 5, and 9 and enter the values in the TOTAL row. These totals are to be entered in the Deck Cargo Loading row of the VESSEL LOADING FORM.

4. Sum column 10 and enter the value in the TOTAL row. This total is to be be added to the TANK LOADING FORM FSC MOM TOTAL and entered into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

1/12/2024

\_

# **CONDITION 4: Load Line**

	VESS						
ondition: FALCON DIAMOND - (4) LOAD LINE							
$COLUMN \rightarrow$	1	2	3	4	5	6	7
				TCG			
	WEIGHT	LCG	L-MOM	(m from CL,	T-Mom	VCG	V-MOM
tem	(MT)	(m aft FRO)	(MT-m)	+STBD)	(MT-m)	(m ABL)	(MT-m)
GHTSHIP	5870.87	28.00	164,361	-0.50	-2,906	20.11	118086.
GHTSHIP ADJUSTMENTS	4.00	31.25	125	0.00	0	8.15	33
REW, EFFECTS, & STORES	5.00	17.43	87	0.00	0	13.60	68
FFSHORE WORKERS, EFFECTS, & STORES	20.00	17.43	349	0.00	0	13.60	272
OTAL DECK CARGO (from DECK CARGO LOADING			22.400				2 050
ORM)	462.08	48.00	22,180	3.00	1,386	6.60	3,050
ANK LIQUIDS IN VESSEL'S TANKS (from TANK DADING FORM)	1,240.55		51,044		1,163		2,848
OTAL FSM OF ALL SLACK TANKS (from TANK LOADING	1,240.33		51,044		1,105		2,040
ORM and DECK CARGO LOADING FORM)							909
TOTALS:	7,602.50		238,146		-357		125,266
	Vessel	Loading Calculat	<u>ions</u>				
(1) LCG = (Total Col. 3 / Total Col. 1) =	238,146	/ 7,602.50	= 31.32	m aft of FR	0		
(2) TCG = (Total Col. 5 / Total Col. 1) =	-357	/ 7,602.50	= -0.05	m from CL (+	+STBD)		
(3) KG = VCG = (Total Col. 7 / Total Col. 1) =	125.266	/ 7,602.50	= 16.48	m ABL	NOTE: INCL	UDES FSE	
(4) DISPLACEMENT = Total		7.602.50	мт	_			
(5) MEAN SW WATER DRAFT (from Hydrostatic Pro							
ECK STABILITY:	operties) =	3.576	m ABL				
Does the loading condition's KG fall be	low the curv						
YES	×	<ul> <li>Loading condition</li> </ul>	on meets the st	tability requirer	ments		
NO							
		Loading condition					
	Ō	Increase ballast an	d/or decrease dec	k cargo or take ot		action.	
	~	Increase ballast an Correct Loading fo	d/or decrease dec orms and check KG	k cargo or take ot Gagain.	her corrective	action.	
HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE	~	Increase ballast an Correct Loading fo	d/or decrease dec orms and check KG	k cargo or take ot Gagain.	her corrective	action.	
	THE TRIM, H	Increase ballast an Correct Loading fo	d/or decrease dec orms and check KG	k cargo or take ot Gagain.	her corrective	action.	
HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE	THE TRIM, H	Increase ballast an Correct Loading fo HEEL, AND DRAFTS = 62.40	d/or decrease dec orms and check KG AT THE BOW / m	k cargo or take ot 3 again. AND TRANSON	her corrective	action.	
HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H	THE TRIM, H (6) LOA (drostatics)	Increase ballast an Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.89	d/or decrease dec rms and check KC AT THE BOW / m m aft of FR	k cargo or take ot 3 again. AND TRANSON	her corrective	action.	
HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE	THE TRIM, H (6) LOA (drostatics) drostatics)	Increase ballast an Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56	d/or decrease dec orms and check KG AT THE BOW / m	k cargo or take ot 3 again. AND TRANSON	her corrective	action.	
HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy	THE TRIM, H (6) LOA (drostatics) (drostatics) ydrostatics)	Increase ballast an Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07	d/or decrease dec mms and check KG AT THE BOW / m m aft of FR MT-m	k cargo or take ot 3 again. AND TRANSON	her corrective	action.	
HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H (8) MOMENT TO TRIM 1mm, MTmm (from Hy	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics)	Increase ballast an Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59	d/or decrease dec mms and check KC M THE BOW / m aft of FR MT-m m ABL	k cargo or take ot 3 again. AND TRANSON	her corrective	action.	
HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(9)	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics)	Increase ballast an Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59	d/or decrease dec mrs and check KC m m m aft of FR MT-m m ABL MT-m	k cargo or take ot 3 again. AND TRANSON 0	And the corrective	action. Average Dra1	fts
HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H) (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from H) (12) TRIM LEVE	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (R = (1) - (7)	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43	d/or decrease dec imms and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR	k cargo or take ot 3 again. AND TRANSOM 0 0	An Calculate		
HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(9 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [(	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (r) (3) / (9) (r) (10) (10) (10) (10)	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.31	d/or decrease dec ms and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR m m (+Aft/-Fw	k cargo or take ot 3 again. AND TRANSOM 0 0	An Calculate A	Average Draf	
HE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H) (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from H) (12) TRIM LEVE	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (10) X 1000 (10) X 1000] ((6) - (11))	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.31	d/or decrease dec imms and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m aft of FR	k cargo or take ot 3 again. AND TRANSOM 0 0	An Calculate A	Average Draf	
(7) LCB (from H) (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u>	(6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (ref(ref(ref(ref(ref))) (ref(ref(ref))) (ref(ref(ref))) (ref(ref(ref))) (ref(ref))) (ref(ref)) (ref(ref))) (re	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.31 = 3.42	d/or decrease dec ms and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL	k cargo or take ot 3 again. AND TRANSOM 0 0	An Calculate A	Average Draf	
(7) LCB (from H) (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H) (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u> (15) MEAN HULL DRAFT @ TRANSOM	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (r) (r) (r) (r) (r) (r) (r) (r) (r) (r	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.43 = 0.31 = 3.42 = 3.73	d/or decrease dec ms and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL	k cargo or take ot 3 again. AND TRANSOM 0 0	An Calculate A	Average Draf	
(7) LCB (from H) (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H) (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u> (15) MEAN HULL DRAFT @ TRANSOM	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (r)	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.43 = 0.31 = 3.42 = 3.73	d/or decrease dec ms and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL	k cargo or take ot 3 again. AND TRANSOM 0 0	An Calculate A	Average Draf	
(7) LCB (from H) (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u>	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (r) (r) (r) (r) (r) (r) (r) (r) (r) (r	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.43 = 0.31 = 3.42 = 3.73 = 4.62	d/or decrease dec ms and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL	k cargo or take ot 3 again. AND TRANSOM 0 0	An Calculate A	Average Draf	
(7) LCB (from H) (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H) (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u> (15) MEAN HULL DRAFT @ TRANSOM	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (R = (1) - (7) (10) X 1000 ] ((6) - (11)] (6) = (13) + (14) (14) + 0.9 (17) BEAM	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.43 = 0.31 = 3.42 = 3.73 = 4.62 = 39.60	d/or decrease dec ms and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL	k cargo or take ot 3 again. AND TRANSOM 0 0	An Calculate A	Average Draf	
(7) LCB (from H) (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H) (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN HULL DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ]	THE TRIM, H (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) R = (1) - (7) (10) X 1000 ] ((10) X 1000 ] ((10) X 1000 ] ((10) X 1000 ] ((10) X 1000 ] ((11) X 100	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.43 = 0.31 = 3.42 = 3.73 = 4.62 = 39.60 = 8.16	d/or decrease dec mrs and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m	k cargo or take ot 3 again. AND TRANSOM 0 0	An Calculate A	Average Draf	
(7) LCB (from H) (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H) (10) MT1mm CORRECTED = MT1mm = (8) X [(9) (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN HULL DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (18) MOMENT TO HEEL 1mm, MH1mm (from H)	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (10) X 1000 ] (10) X 1000 ] (11) X 1000 ] (11) X 1000 ] (12) X 1000 ] (13) + (14) (14) + 0.9 (17) BEAM (drostatics) (drostatics)	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.43 = 0.31 = 3.42 = 3.73 = 4.62 = 39.60 = 8.16 = 44.47	d/or decrease dec mrs and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m MT-m	k cargo or take ot 3 again. AND TRANSOM 0 0	An Calculate A	Average Draf	
(7) LCB (from H) (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H) (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN HULL DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (18) MOMENT TO HEEL 1mm, MH1mm (from H) (19) KMT (from Hy	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (10) X 1000 ] ((10) X 1000 ] ((11) X 1000 ] ((11) X 1000 ] ((12) X 1000 ] ((12) X 1000 ] ((13) + (14) + (15) +	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.43 = 0.31 = 3.42 = 3.73 = 4.62 = 39.60 = 8.16 = 44.47 = 5.14	d/or decrease dec ms and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m MT-m m ABL m	k cargo or take ot 3 again. AND TRANSOM 0 0 vd)	An Calculate A	Average Dra1 d TRANSOM	Port & Stb
(7) LCB (from H) (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H) (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN HULL DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (18) MOMENT TO HEEL 1mm, MH1mm (from H) (19) KMT (from Hy (20) MH1mm CORRECTED = MH1mm = (18) X [(19)	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (10) X 1000 ] ((10) X 1000 ]	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.43 = 0.31 = 3.42 = 3.73 = 4.62 = 39.60 = 8.16 = 44.47 = 5.14 = -0.05	d/or decrease dec mrs and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL MT-m MT-m MT-m	k cargo or take ot 3 again. AND TRANSOM 0 0 vd)	An Calculate A	Average Dra1 d TRANSOM Calculate	Port & Stb
(7) LCB (from H) (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H) (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN HULL DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (18) MOMENT TO HEEL 1mm, MH1mm (from H) (19) KMT (from Hy (20) MH1mm CORRECTED = MH1mm = (18) X [(19) (21) HEEL LEV	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (10) X 1000 ] ((10) X 1000 ]	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.43 = 0.31 = 3.42 = 3.73 = 4.62 = 39.60 = 8.16 = 44.47 = 5.14 = -0.05 = -0.07	d/or decrease dec mrs and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m MT-m m ABL m From CL (	k cargo or take ot 3 again. AND TRANSOM 0 0 vd)	An Calculate A	Average Dra1 d TRANSOM Calculate Drafts @ B	Port & Stb
(7) LCB (from H) (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H) (10) MT1mm CORRECTED = MT1mm = (8) X [(2 (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN HULL DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (18) MOMENT TO HEEL 1mm, MH1mm (from H) (19) KMT (from Hy (20) MH1mm CORRECTED = MH1mm = (18) X [(19) (21) HEEL LEV (22) HEEL = [(4) X (21])/[	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (10) X 1000 ] ((10) X 1000 ] ((10) X 1000 ] ((10) X 1000 ] ((17) BEAM (drostatics) (drostatics) (drostatics) (- (3)] / (19) ER = TCG (2) (20) X 1000]	Increase ballast an Correct Loading for HEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 10.59 = 31.68 = 0.43 = 0.43 = 0.31 = 3.42 = 3.73 = 4.62 = 39.60 = 8.16 = 44.47 = 5.14 = -0.05 = -0.07 = 3.39	d/or decrease dec mrs and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m ABL m From CL ( m (+Stbd)	k cargo or take ot 3 again. AND TRANSOM 0 0 vd) (+Stbd) = <u>3.46</u>	ner corrective 1. Calculate / @ BOW an	Average Dra1 d TRANSOM Calculate Drafts @ B	Port & Stb
(7) LCB (from H) (7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from H) (10) MT1mm CORRECTED = MT1mm = (8) X [(2) (11) LCF (from H) (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN HULL DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (18) MOMENT TO HEEL 1mm, MH1mm (from H) (19) KMT (from Hy (20) MH1mm CORRECTED = MH1mm = (18) X [(19) (21) HEEL LEV (22) HEEL = [(4) X (21)]/[ (23) DRAFT @ BOW = (14) +/- (22) / 2:	THE TRIM, H (6) LOA (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (10) X 1000 ] (10) X 1000 ] (10) X 1000 ] (10) X 1000 ] (11) BEAM (drostatics) (17) BEAM (drostatics) (drostatics) (- (3)] / (19) ER = TCG (2) (20) X 1000] STBD	$\begin{array}{r} Increase ballast an Correct Loading for Correct Loading for Correct Loading for LEEL, AND DRAFTS = 62.40 = 30.89 = 12.56 = 105.07 = 31.68 = 31.68 = 0.43 = 0.43 = 0.31 = 3.42 = 3.73 = 4.62 = 39.60 = 8.16 = 44.47 = 5.14 = -0.05 = -0.07 = 3.39 = -0.07 = 3.39 = -0.07 = 3.39 = -0.07 = 3.70 = -0.07 = 3.70 = -0.07 = 3.70 = -0.07 = 3.70 = -0.07 = $	d/or decrease dec ms and check KG AT THE BOW / m aft of FR MT-m m ABL MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m MT-m m ABL MT-m m from CL ( m (+Stbd) PORT	k cargo or take ot 3 again. AND TRANSOM 0 0 vd) (+Stbd) = <u>3.46</u> = <u>3.45</u> 3.77	ner corrective 1. Calculate / @ BOW an	Average Dra1 d TRANSOM Calculate Drafts @ B	Port & Stb

				TANK LOADI	NG FORM					
Condition: FALCON DIAMOND -	(4) LOAD LINE									
$COLUMN \rightarrow$	0	1	2	3	4	5	6	7	8	9
	FILL	WEIGHT	LCG m a	ft of FR 0	TCG (m +/- from CL)		VCG (m above BASELINE)		TRANS FSM	LONG'L FSM
TANK	(%)	(MT)	LCG	L-MOM	TCG (+Stbd)	T-MOM	VCG	V-MOM	(MT-m)	(MT-m)
	Enter Value	Enter Value	Enter Value	Col 1 X Col 4	Enter Value	Col 1 X Col 6	Enter Value	Col 1 X Col 2	Enter Value	Enter Value
Ballast #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Port	100	311.75	51.56	16,074.51	-4.77	-1,488.27	2.35	733.54	0.00	0.00
Ballast #3 Stbd	100	311.75	51.56	16,074.51	4.77	1,488.27	2.35	733.54	0.00	0.00
Ballast #4 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #4 Stbd	100	81.02	58.60	4,748.10	14.18	1,149.19	3.16	256.19	0.00	0.00
Zero Discharge #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Day Tank Port	95	10.23	24.00	245.49	-13.20	-135.02	3.44	35.24	2.00	2.00
Day Tank Stbd	95	10.23	24.00	245.49	13.20	135.02	3.44	35.24	2.00	2.00
Fuel Oil Port	95	121.67	22.71	2,762.61	-16.09	-1,957.80	2.21	269.28	161.00	61.00
Fuel Oil Stbd	95	121.67	22.71	2,762.61	16.09	1,957.80	2.21	269.28	161.00	61.00
Fresh Water Port	95	132.45	30.00	3,973.50	-17.12	-2,268.15	1.94	257.44	279.00	238.00
Fresh Water Stbd	95	132.45	30.00	3,973.50	17.12	2,268.15	1.94	257.44	279.00	238.00
Greywater	25	2.39	21.60	51.52	5.94	14.16	0.21	0.51	9.00	4.00
Dirty Oil	10	1.32	29.40	38.83	0.00	0.00	0.06	0.08	12.00	12.00
Lube Oil	25	1.73	25.80	44.71	0.90	1.56	0.15	0.26	2.00	6.00
Oily Water	25	1.90	25.80	49.14	-0.90	-1.71	0.15	0.29	2.00	7.00
TOTAL (Record here and on Vessel Loading Form)	0	1240.55		51044.50		1163.19		2848.31	909.00	631.00

#### INSTRUCTIONS FOR THE TANK LOADING FORM

For each of the vessel's tanks that contain liquid, determined and enter the following on the Tank Loading Form:

1. Take soundings of each tank and enter the liquid level in each tank in column 0 of the TANK LOADING FORM.

2. Consult the TANK CAPACITY TABLES and enter the weight of the liquid in column 1, the LCG of the liquid in column 2, the TCG of the liquid in column 4, and the VCG of the liquid in column 6 corresponding to the sounding. Enter the transverse and longitudinal free surface moments into columns 8 and 9, respectively. If the actual sounding falls between two soundings listed the TANK CAPACITY TABLES, enter the values associated with the higher of the two soundings on the TANK LOADING FORM.

3. Sum the weights in column 1 to obtain the total weight of the liquids in the tanks. Enter this TOTAL on the TANK LOADING FORM and the VESSEL LOADING FORM. 4. Multiply each weight in column 1 by its corresponding LCG in column 2 to obtain the longitudinal moment of the weight and enter this value in column 3. Sum the longitudinal moments in column 3 to obtain the total longitudinal moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM and the VESSEL LOADING FORM.

5. Multiply each weight in column 1 by its corresponding TCG in column 4 to obtain the transverse moment of the weight and enter this value in column 5. Sum the transverse moments in column 5 to obtain the total transverse moment of the liquids in the tanks. Note the starboard moments are positive and the port moments are negative. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

6. Multiply each weight in column 1 by its corresponding VCG in column 6 to obtain the vertical moment of the weight and enter this value in column 7. Sum the vertical moments in column 7 to obtain the total vertical moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

7. Individually sum the free surface moments in columns 8 and 9 to obtain the total transverse and longitudinal free surface moments of the internal tanks. Enter the maximum of these two TOTALS on the TANK LOADING FORM. Add this value to the DECK TANKS MAX FSM TOTAL from the DECK CARGO LOADING FORM and enter this value into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

			DECK CARG	O LOADING	FORM					
CONDITION: FALCON DIAMOND - (4) LO	AD LINE									
COLUMN>	· 1	2	3	4	5	6	7	8	9	10
ITEM	WEIGHT	LCG (m a	ft of FR 0 )	TCG (m +,	′- from CL)	VCG above	MAIN DK	VCG (m ab	ove BL)	DECK TANKS
(Include deck tanks & contents as	(MT)	LCG	L-MOM	TCG (+ STBD)	T-MOM	MAIN DECK	to BL	VCG	V-MOM	MAX FSM
separate line items)	Enter Value	Enter Value	Col 1 x Col 2	Enter Value	Col 1 x Col 4	Enter Value		Col 6 + Col 7		(MT-m)
Deck Cargo	462.08	48.00	22179.84	3.00	1386.24	2.00	+ 4.6=	6.60	3049.73	
							+ 4.6=			
							+ 4.6=			
							+ 4.6=		9	
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=	0		
							+ 4.6=			
							+ 4.6=			
							+4.6=			
							+ 4.6=			
							+ 4.6=			
						<b>O</b>	+ 4.6=			
							+ 4.6=			
							+ 4.6=			
						×	+ 4.6=			
						ľ.	+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
TOTAL (Record here and on Vessel Loading Form)	462.08		22179.84		1386.24				3049.73	0.00

#### INSTRUCTIONS FOR THE DECK CARGO LOADING FORM

For each of material carried by the vessel the following shall be determined and entered on the Deck Cargo Loading Form:

1. A complete list of non-tank cargoes is to be entered above with weight, LCG, TCG, and VCG for each item in columns 1, 2, 4 and 6. 2.Cal culate the longitudinal moment for each cargo item by multiplying columns 1 and 2 for each item. Calculate the transverse moment for each cargo item by multiplying columns 1 and 4 for each item. Calculate the vertical moment for each cargo item by multiplying columns 1 and 8 for each item.

3. Sum columns 1, 3, 5, and 9 and enter the values in the TOTAL row. These totals are to be entered in the Deck Cargo Loading row of the VESSEL LOADING FORM.

4. Sum column 10 and enter the value in the TOTAL row. This total is to be be added to the TANK LOADING FORM FSC MOM TOTAL and entered into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

# **CONDITION 5A: 454 MT Variable Load + Helicopter**

ondition: FALCON DIAMOND - (5A) LOADED CONDIT		154 MT VI + H					
COLUMN -		2	3	4	5	6	7
		2	5	TCG	5	0	$\mathbf{D}^{\prime}$
	WEIGHT	LCG	L-MOM	(m from CL,	T-Mom	VCG	V-MON
em	(MT)	(m aft FRO)	(MT-m)	+STBD)	(MT-m)	(m ABL)	(MT-m
GHTSHIP	5870.87	28.00	164,361	-0.50	-2,906	20.11	118086.
GHTSHIP ADJUSTMENTS	4.00	31.25	125	0.00	0	8.15	33
REW, EFFECTS, & STORES	5.00	17.43	87	0.00	0	13.60	68
FFSHORE WORKERS, EFFECTS, & STORES	20.00	17.43	349	0.00	0	13.60	272
OTAL DECK CARGO (from DECK CARGO LOADING							
ORM)	229.68	52.03	11,951	4.85	1,114	9.44	2,168
ANK LIQUIDS IN VESSEL'S TANKS (from TANK							0.50
OADING FORM) OTAL FSM OF ALL SLACK TANKS (from TANK LOADING	508.85		22,208		1,830		859
ORM and DECK CARGO LOADING FORM)							1,442
TOTALS	: 6,638.40		199,081		38		122,929
		Loading Calculat		_			
(1) LCG = (Total Col. 3 / Total Col. 1) =	= 199,081	/ 6,638.40	= 29.99	m aft of FR	0		
(2) TCG = (Total Col. 5 / Total Col. 1) =	38	/ 6,638.40	= 0.01	m from CL (	+STBD)		
(3) KG = VCG = (Total Col. 7 / Total Col. 1) =	= 122,929	/ 6,638.40	= 18.52	m ABL	NOTE: INCLU	JDES FSE	
(4) DISPLACEMENT = Total	Column 1 =	6,638.40	MT	_			
(5) MEAN SW WATER DRAFT (from Hydrostatic P	Properties) =	3.19	m ABL				
HECK STABILITY:							
HE FOLLOWING OPTIONAL CALCULATIONS DETERMIN	IE THE TRIM, H	Correct Loading fo		-	Л.		
				_			
(7) LCB (from +	(6) LOA		m maft of FR	<u> </u>			
(7) LCB (ITOTH F (8) MOMENT TO TRIM 1mm, MTmm (from H			MT-m				
(9) KML (from F			m ABL				
(10) MT1mm CORRECTED = MT1mm = (8) X [							
		10.41	MT-m				
(, (	Hydrostatics)			D			
		= 31.84	MT-m m aft of FR	0	Calculate A	werage Drat	fts
(12) TRIM LEV	/ER = (1) - (7)	= <u>31.84</u> = -0.78	MT-m m aft of FR m	-		werage Drat d TRANSOM	fts
(12) TRIM LEV (13) TRIM = [(4) X (12)] /	/ER = (1) - (7) [(10) X 1000 ]	= <u>31.84</u> = -0.78 = -0.49	MT-m m aft of FR m m (+Aft/-Fw	-		-	fts
(12) TRIM LEV	/ER = (1) - (7) [(10) X 1000 ] X [(6) - (11)]	= <u>31.84</u> = -0.78 = -0.49	MT-m m aft of FR m	-		-	fts
(12) TRIM LEV (13) TRIM = [(4) X (12)] /	$\frac{7}{(2R = (1) - (7)}{(10) \times 1000}$ $\frac{X [(6) - (11)]}{(6)}$	= <u>31.84</u> = <u>-0.78</u> = <u>-0.49</u> = <u>3.43</u>	MT-m m aft of FR m m (+Aft/-Fw	-		-	fts
(12) TRIM LEV (13) TRIM = [(4) X (12)] / (14) MEAN DRAFT @ BOW = (5) - ( <u>13)</u>	$\frac{4}{(10)} = \frac{1}{(10)} = 1$	= <u>31.84</u> = <u>-0.78</u> = <u>-0.49</u> = <u>3.43</u> = <u>2.94</u>	MT-m m aft of FR m m (+Aft/-Fw m ABL	-		-	fts
(12) TRIM LEV (13) TRIM = [(4) X (12)] / (14) MEAN DRAFT @ BOW = (5) - <u>(13)</u> (15) MEAN DRAFT @ TRANSOM	$\frac{4}{(10)} = \frac{1}{(10)} = 1$	= <u>31.84</u> = <u>-0.78</u> = <u>-0.49</u> = <u>3.43</u> = <u>2.94</u>	MT-m m aft of FRI m (+Aft/-Fw m ABL m ABL	-		-	fts
(12) TRIM LEV (13) TRIM = [(4) X (12)] / (14) MEAN DRAFT @ BOW = (5) - (13) (15) MEAN DRAFT @ TRANSON (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4	$\frac{2}{2} (1) - (7) = (10) \times 1000 = \frac{1}{2} \times \frac{1}{2} (10) \times 1000 = \frac{1}{2} \times \frac{1}{2} $	= <u>31.84</u> = <u>-0.78</u> = <u>-0.49</u> = <u>3.43</u> = <u>2.94</u> = <u>3.85</u> = <u>39.60</u>	MT-m m aft of FRI m (+Aft/-Fw m ABL m ABL m ABL m	-		-	fts
(12) TRIM LEV (13) TRIM = [(4) X (12)] / (14) MEAN DRAFT @ BOW = (5) - (13) (15) MEAN DRAFT @ TRANSON (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H	$\frac{YER = (1) - (7)}{[(10) \times 1000]} \\ \frac{X [(6) - (11)]}{(6)} \\ A = (13) + (14) \\ A = 1 + (14) + 0.9 \\ (16) BEAM \\ Hydrostatics)$	= 31.84 $= -0.78$ $= -0.49$ $= 3.43$ $= 2.94$ $= 3.85$ $= 39.60$ $= 8.12$	MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m MT-m	-		-	fts
(12) TRIM LEV (13) TRIM = [(4) X (12)] / (14) MEAN DRAFT @ BOW = (5) - (13) (15) MEAN DRAFT @ TRANSON (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H (18) KMT (from H	$\frac{YER = (1) - (7)}{[(10) \times 1000]} \\ \frac{X [(6) - (11)]}{(6)} \\ A = (13) + (14) \\ A = (13) + (14) + 0.9 \\ (16) BEAM \\ Hydrostatics) \\ Hydrostatics)$	= 31.84 $= -0.78$ $= -0.49$ $= 3.43$ $= 2.94$ $= 385$ $= 39.60$ $= 8.12$ $= 50.19$	MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m MT-m m ABL	-		H TRANSOM	
(12) TRIM LEV (13) TRIM = [(4) X (12)] / (14) MEAN DRAFT @ BOW = (5) - (13) (15) MEAN DRAFT @ TRANSON (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H (18) KMT (from H (19) MH1mm CORRECTED = MH1mm = (17) X [(12)	$\begin{array}{l} & (2R = (1) - (7) \\ & (10) \times 1000 \\ & (10) \times 1000 \\ \hline & (10$	= 31.84 $= -0.78$ $= -0.49$ $= 3.43$ $= 2.94$ $= 385$ $= 39.60$ $= 8.12$ $= 50.19$ $= 5.12$	MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m MT-m m ABL MT-m	rd)		d TRANSOM	Port & Stb
(12) TRIM LEV (13) TRIM = [(4) X (12)] / (14) MEAN DRAFT @ BOW = (5) - (13) (15) MEAN DRAFT @ TRANSON (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H (18) KMT (from H (19) MH1mm CORRECTED = MH1mm = (17) X [(12) (20) HEEL LET	$\begin{array}{l} \label{eq:constraints} & \mbox{YER} = (1) - (7) \\ [(10) X 1000] \\ \hline X [(6) - (11)] \\ \hline (6) \\ \mbox{M} = (13) + (14) \\ \mbox{H} = (13) + (14$	= 31.84 $= -0.78$ $= -0.49$ $= 3.43$ $= 2.94$ $= 39.60$ $= 8.12$ $= 50.19$ $= 5.12$ $= 0.01$	MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL MT-m m ABL MT-m m from CL (	rd)		Calculate Drafts @ E	Port & Stb
(12) TRIM LEV (13) TRIM = [(4) X (12)] / (14) MEAN DRAFT @ BOW = (5) - (13) (15) MEAN DRAFT @ TRANSON (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H (18) KMT (from H (19) MH1mm CORRECTED = MH1mm = (17) X [(12) (20) HEEL LEF (21) HEEL = [(4) X (20)],	$\frac{YER = (1) - (7)}{[(10) \times 1000]} \\ \frac{X [(6) - (11)]}{(6)} \\ A = (13) + (14) + (14) \\ A = (14) + (14$	= 31.84 $= -0.78$ $= -0.49$ $= 3.43$ $= 2.94$ $= 39.60$ $= 8.12$ $= 50.19$ $= 5.12$ $= 0.01$ $= 0.01$	MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL m MT-m m ABL MT-m	rd) +Stbd)		d TRANSOM	Port & Stb
(12) TRIM LEV (13) TRIM = [(4) X (12)] / (14) MEAN DRAFT @ BOW = (5) - (13) (15) MEAN DRAFT @ TRANSON (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 (17) MOMENT TO HEEL 1mm, MH1mm (from H (18) KMT (from H (19) MH1mm CORRECTED = MH1mm = (17) X [(12) (20) HEEL LET	$\begin{array}{l} & (2  \text{R} = (1) - (7) \\ & (10) \times 1000 \\ & (10) \times 1000 \\ \hline & (10) \times (10) \\ \hline$	= 31.84 $= -0.78$ $= -0.49$ $= 3.43$ $= 2.94$ $= 39.60$ $= 8.12$ $= 50.19$ $= 5.12$ $= 0.01$ $= 0.01$ $= 3.43$	MT-m m aft of FR m (+Aft/-Fw m ABL m ABL m ABL MT-m m ABL MT-m m from CL ( m (+Stbd)	+Stbd) = <u>3.43</u>	@ BOW and	Calculate Drafts @ E	Port & Stb

				TANK LOADI	NG FORM					
Condition: FALCON DIAMOND -	(5A) LOADED CO	NDITION AFLOA	T, 454 MT VL + I	1						
$COLUMN \rightarrow$	0	1	2	3	4	5	6	7	8	_9
	SOUNDING	WEIGHT	LCG m at	ft of FR 0	TCG (m +/- from CL)		VCG (m above BASELINE)		TRANS FSM	LONG'L FSM
TANK	(%)	(MT)	LCG	L-MOM	TCG (+Stbd)	T-MOM	VCG	V-MOM	(MT-m)	(MT-m)
	Enter Value	Enter Value	Enter Value	Col 1 X Col 4	Enter Value	Col 1 X Col 6	Enter Value	Col 1 X Col 2	Enter Value	Enter Value
Ballast #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Stbd	50	155.87	51.53	8,031.50	4.75	739.96	1.23	191.49	533.00	300.00
Ballast #4 Port	100	69.83	58.60	4,091.69	-14.46	-1,009.88	3.14	218.92	0.00	0.00
Ballast #4 Stbd	100	81.02	58.60	4,748.10	14.18	1,149.19	3.16	256.19	0.00	0.00
Zero Discharge #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Day Tank Port	35	3.77	24.00	90.44	-13.20	-49.74	2.78	10.50	2.00	2.00
Day Tank Stbd	35	3.77	24.00	90.44	13.20	49.74	2.78	10.50	2.00	2.00
Fuel Oil Port	35	44.82	22.80	1,022.05	-15.84	-710.07	0.94	42.16	161.00	61.00
Fuel Oil Stbd	35	44.82	22.80	1,022.05	15.84	710.07	0.94	42.16	161.00	61.00
Fresh Water Port	15	20.91	30.00	627.39	-15.68	-327.92	0.42	8.87	279.00	238.00
Fresh Water Stbd	55	76.68	30.00	2,300.45	16.49	1,264.25	1.01	77.38	279.00	238.00
Greywater	25	2.39	21.60	51.52	5.94	14.16	0.21	0.51	9.00	4.00
Dirty Oil	10	1.32	29.40	38.83	0.00	0.00	0.06	0.08	12.00	12.00
Lube Oil	25	1.73	25.80	44.71	0.90	1.56	0.15	0.26	2.00	6.00
Oily Water	25	1.90	25.80	49.14	-0.90	-1.71	0.15	0.29	2.00	7.00
TOTAL (Record here and on Vessel Loading Form)		508.85		22208.32		1829.60		859.29	1442.00	931.00

#### INSTRUCTIONS FOR THE TANK LOADING FORM

For each of the vessel's tanks that contain liquid, determined and enter the following on the Tank Loading Form:

1. Take soundings of each tank and enter the liquid level in each tank in column 0 of the TANK LOADING FORM.

2. Consult the TANK CAPACITY TABLES and enter the weight of the liquid in column 1, the LCG of the liquid in column 2, the TCG of the liquid in column 4, and the VCG of the liquid in column 6 corresponding to the sounding. Enter the transverse and longitudinal free surface moments into columns 8 and 9, respectively. If the actual sounding falls between two soundings listed the TANK CAPACITY TABLES, enter the values associated with the higher of the two soundings on the TANK LOADING FORM.

3. Sum the weights in column 1 to obtain the total weight of the liquids in the tanks. Enter this TOTAL on the TANK LOADING FORM and the VESSEL LOADING FORM. 4. Multiply each weight in column 1 by its corresponding LCG in column 2 to obtain the longitudinal moment of the weight and enter this value in column 3. Sum the longitudinal moments in column 3 to obtain the total longitudinal moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

5. Multiply each weight in column 1 by its corresponding TCG in column 4 to obtain the transverse moment of the weight and enter this value in column 5. Sum the transverse moments in column 5 to obtain the total transverse moment of the liquids in the tanks. Note the starboard moments are positive and the port moments are negative. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

6. Multiply each weight in column 1 by its corresponding VCG in column 6 to obtain the vertical moment of the weight and enter this value in column 7. Sum the vertical moments in column 7 to obtain the total vertical moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

7. Individually sum the free surface moments in columns 8 and 9 to obtain the total transverse and longitudinal free surface moments of the internal tanks. Enter the maximum of these two TOTALS on the TANK LOADING FORM. Add this value to the DECK TANKS MAX FSM TOTAL from the DECK CARGO LOADING FORM and enter this value into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

### Operating Manual Doc No: 0722-010-005-C5

			DECK CARG	O LOADING	FORM					
Condition: FALCON DIAMOND - (5A) LO	ADED CONDIT	TION AFLOAT,	454 MT VL + I	Н						
COLUMN>	1	2	3	4	5	6	7	8	9	10
ITEM	WEIGHT	LCG (m a	ft of FR 0 )	TCG (m +,	- from CL)	VCG above	MAIN DK	VCG (m ab	ove BL)	DECK TANKS
(Include deck tanks & contents as	(MT)	LCG	L-MOM	TCG (+ STBD)	T-MOM	MAIN DECK	to BL	VCG	V-MOM	MAX FSM
separate line items)	Enter Value	Enter Value	Col 1 x Col 2	Enter Value	Col 1 x Col 4	Enter Value		Col 6 + Col 7		(MT-m)
Deck Cargo	222.88	54.00	12035.52	5.00	1114.40	4.56	+ 4.6=	9.16	2041.58	
Agusta AW-139 Chopper	6.80	-12.43	-84.50	0.00	0.00	14	+ 4.6=	18.60	126.48	
							+ 4.6=			
							+ 4.6=		5	
							+ 4.6=		2	
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=	$\mathcal{O}$		
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
						$\mathbf{O}$	+ 4.6=			
							+ 4.6=			
						V	+ 4.6=			
							+ 4.6=			
					0		+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
			X				+ 4.6=			
TOTAL (Record here and on Vessel Loading Form)	229.68		11951.02		1114.40				2168.06	0.00

INSTRUCTIONS FOR THE DECK CARGO LOADING FORM

For each of material carried by the vessel the following shall be determined and entered on the Deck Cargo Loading Form: 1. A complete list of non-tank cargoesis to be entered above with weight, LCG, TCG, and VCG for each item in columns 1, 2, 4 and 6.

2.Calculate the longitudinal moment for each cargo item by multiplying columns 1 and 2 for each item. Calculate the transverse moment for each cargo item by multiplying columns 1 and 4 for each item. Calculate the transverse moment for each cargo item by multiplying columns 1 and 4 for each item.

3. Sum columns 1, 3, 5, and 9 and enter the values in the TOTAL row. These totals are to be entered in the Deck Cargo Loading row of the VESSEL LOADING FORM.

4. Sum column 10 and enter the value in the TOTAL row. This total is to be be added to the TANK LOADING FORM FSC MOM TOTAL and entered into the TOTAL FSM OF ALL

SLACK TANKS row of the VESSEL LOADING FORM.

# CONDITION 5B: 709 MT Variable Load + Helicopter VESSEL LOADING FORM

Condition: FALCON DIAMOND - (5B) LOADED CONDITIO	ON AFLOAT,	709 MT VL + H					
$COLUMN \rightarrow$	1	2	3	4	5	6	7
				TCG			
	WEIGHT	LCG	L-MOM	(m from CL,	T-Mom	VCG	V-MOM
tem	(MT)	(m aft FRO)	(MT-m)	+STBD)	(MT-m)	(m ABL)	(MT-m)
IGHTSHIP	5870.87	28.00	164,361	-0.50	-2,906	20.11	118086.
IGHTSHIP ADJUSTMENTS	4.00	31.25	125	0.00	0	8.15	33
CREW, EFFECTS, & STORES	5.00	17.43	87	0.00	0	13.60	68
OFFSHORE WORKERS, EFFECTS, & STORES	20.00	17.43	349	0.00	0	13.60	272
TOTAL DECK CARGO (from DECK CARGO LOADING							
FORM)	537.54	53.16	28,575	3.95	2,123	9.28	4,988
TANK LIQUIDS IN VESSEL'S TANKS (from TANK							
LOADING FORM)	149.26		3,948		735		113
TOTAL FSM OF ALL SLACK TANKS (from TANK LOADING FORM and DECK CARGO LOADING FORM)							909
· · ·							
TOTALS:	6,586.67		197,446		-48		124,469
	Vessel	Loading Calculati	ons_	ノ			
(1) LCG = (Total Col. 3 / Total Col. 1) =	197,446	/ 6,586.67	= 29.98	m aft of FR	0		
(2) TCG = (Total Col. 5 / Total Col. 1) =	-48	/ 6,586.67	= -0.01	m from CL (+	-STBD)		
(3) KG = VCG = (Total Col. 7 / Total Col. 1) =	124.469	/ 6,586.67	= 18.90	m ABL	NOTE: INCL	UDES FSE	
(4) DISPLACEMENT = Total		6,586.67	MT				
(5) MEAN SW WATER DRAFT (from Hydrostatic Pro CHECK STABILITY:	operties) =	3.17	m ABL				
NO		_ Loading condition	l/or decrease decl	cargo or take ot	•	action.	
THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE		Increase ballast and Correct Loading fo	d/or decrease deck rms and check KG	c cargo or take ot again.	her corrective	action.	
		Increase ballast and Correct Loading fo	d/or decrease deck rms and check KG	c cargo or take ot again.	her corrective	action.	
		Increase ballast and Correct Loading fo	d/or decrease deck rms and check KG	c cargo or take ot again.	her corrective	action.	
THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy	(6) LOA (7) the trim, f	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76	d/or decrease deck rms and check KG AT THE BOW A m m aft of FR(	a cargo or take ot again. AND TRANSON	her corrective	action.	
THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy	THE TRIM, F (6) LOA ydrostatics) drostatics)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34	d/or decrease deck rms and check KG AT THE BOW A m m aft of FR( MT-m	a cargo or take ot again. AND TRANSON	her corrective	action.	
THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy	THE TRIM, F (6) LOA (drostatics) (drostatics) (drostatics)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71	d/or decrease deck ms and check KG AT THE BOW A m m aft of FR( MT-m m ABL	a cargo or take ot again. AND TRANSON	her corrective	action.	
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5)	THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38	d/or decrease deck ms and check KG AT THE BOW A m m aft of FR( MT-m m ABL MT-m	x cargo or take ot again. IND TRANSON	her corrective	action.	
THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE (7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy	THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38	d/or decrease deck ms and check KG AT THE BOW A m m aft of FR( MT-m m ABL	x cargo or take ot again. NND TRANSON	her corrective.		free
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5)	THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9) ydrostatics)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85	d/or decrease deck ms and check KG AT THE BOW A m m aft of FR( MT-m m ABL MT-m	x cargo or take ot again. NND TRANSON	And the corrective of the corr	Average Draf	fts
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy	THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) R = (1) - (7)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78	d/or decrease deck ms and check KG AT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR(	x cargo or take ot again. IND TRANSON	And the corrective of the corr		fts
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE	(6) LOA (6) LOA (drostatics) (d	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.50	l/or decrease deck rms and check KG MT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m	x cargo or take ot again. IND TRANSON	And the corrective of the corr	Average Draf	fts
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u>	(6) LOA (6) LOA (drostatics) (d	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.50	i/or decrease deck rms and check KG MT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m m (+Aft/-Fw	x cargo or take ot again. IND TRANSON	And the corrective of the corr	Average Draf	fts
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u> (15) MEAN DRAFT @ TRANSOM 5	THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) R = (1) - (7) (10) X 1000 ] <u>([(6) - (11)]</u> (6) = (13) + (14)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.78 = -0.50 = 3.41 = 2.91	l/or decrease deck rms and check KG AT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m m (+Aft/-Fw m ABL m ABL	x cargo or take ot again. IND TRANSON	And the corrective of the corr	Average Draf	fts
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u>	THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) 9) - (3)] / (9) ydrostatics) R = (1) - (7) (10) X 1000 ] <u>([(6) - (11)]</u> (6) = (13) + (14)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.78 = -0.50 = 3.41 = 2.91	l/or decrease deck rms and check KG AT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m m (+Aft/-Fw m ABL	x cargo or take ot again. IND TRANSON	And the corrective of the corr	Average Draf	fts
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u> (15) MEAN DRAFT @ TRANSOM 5	THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) (10) $(1)$ (9) ydrostatics) R = (1) - (7) (10) $\times$ 1000 ] (10) $\times$ 1000 ] (10) $\times$ 1000 ] (10) $\times$ 1000 ] (11) $\times$ 1000 ]	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.78 = -0.50 = 3.41 = 2.91 = 3.83	l/or decrease deck rms and check KG AT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m m (+Aft/-Fw m ABL m ABL m ABL	x cargo or take ot again. IND TRANSON	And the corrective of the corr	Average Draf	fts
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u> (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ]	THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) (10) x 1000 ] (10) x 1000 ] (1	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.78 = -0.50 = 3.41 = 2.91 = 3.83 = 39.60	l/or decrease deck rms and check KG AT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m m (+Aft/-Fw m ABL m ABL m ABL m	x cargo or take ot again. IND TRANSON	And the corrective of the corr	Average Draf	fts
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u> (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy	THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) (10) x 1000 ] (10) x 1000 ] (11) x 1000 ] (11) x 1000 ] (12) x 1000 ] (13) x 1000 ] (14) x 1000 ] (15) x 1000 ] (16) BEAM ydrostatics)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.78 = -0.78 = -0.50 = 3.41 = 2.91 = 3.83 = 39.60 = 8.12	l/or decrease deck rms and check KG AT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m m (+Aft/-Fw m ABL m ABL m ABL	x cargo or take ot again. IND TRANSON	And the corrective of the corr	Average Draf	fts
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - ( <u>13) X</u> (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ]	THE TRIM, F (6) LOA ydrostatics) drostatics) ydrostatics) (10) x 1000 ] (10) x 1000 ] (11) x 1000 ] (12) x 1000 ] (13) x 1000 ] (14) x 1000 ] (15) x 1000 ] (16) BEAM ydrostatics) drostatics)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.78 = -0.78 = -0.50 = 3.41 = 2.91 = 3.83 = 39.60 = 8.12 = 50.55	l/or decrease deck rms and check KG AT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m m (+Aft/-Fw m ABL m ABL m ABL m MT-m	x cargo or take ot again. IND TRANSON	And the corrective of the corr	Average Draf	
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy	THE TRIM, H (6) LOA ydrostatics) drostatics) ydrostatics) (10) x 1000 ] (10) x 1000 ] (11) x 1000 ] (11) x 1000 ] (12) x 1000 ] (13) + (14) + 0.9 (16) BEAM ydrostatics) drostatics) - (3) ] / (18)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.78 = -0.50 = 3.41 = 2.91 = 3.83 = 39.60 = 8.12 = 50.55 = 5.08	l/or decrease deck rms and check KG AT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m (+Aft/-Fw m ABL m ABL m ABL m MT-m m ABL	d)	And the corrective of the corr	Average Dra1 d TRANSOM	Port & Stb
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18)	THE TRIM, F (6) LOA (drostatics) drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (10) X 1000 ] (10) X 1000 ] (10) X 1000 ] (10) X 1000 ] (10) X 1000 ] (11) X 1000 ] (12) X 1000 ] (13) + (14) (14) + 0.9 (16) BEAM (drostatics) drostatics) (13) / (18) ER = TCG (2)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.78 = -0.50 = 3.41 = 2.91 = 3.83 = 39.60 = 8.12 = 50.55 = 5.08 = -0.01	l/or decrease deck rms and check KG AT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m m (+Aft/-Fw m ABL m ABL m ABL m MT-m m ABL MT-m	d)	And the corrective of the corr	Average Dra1 d TRANSOM Calculate	Port & Stb
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18) (20) HEEL LEVE	THE TRIM, F (6) LOA (drostatics) drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (10) X 1000 ] (10) X 1000 ] (10) X 1000 ] (10) X 1000 ] (10) X 1000 ] (11) X 1000 ] (12) X 1000 ] (13) + (14) (14) + 0.9 (16) BEAM (drostatics) drostatics) (13) / (18) ER = TCG (2)	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.78 = -0.78 = -0.50 = 3.41 = 2.91 = 3.83 = 39.60 = 8.12 = 50.55 = 5.08 = -0.01 = -0.01	l/or decrease deck rms and check KG AT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m (+Aft/-Fw m ABL m ABL m ABL m MT-m m ABL MT-m m ABL	x cargo or take of again. IND TRANSON () (d) +Stbd)	And the corrective of the corr	Average Draf d TRANSOM Calculate _Drafts @ E	Port & Stb
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18) (20) HEEL LEVI (21) HEEL = [(4) X (20])/[	THE TRIM, H (6) LOA ydrostatics) drostatics) ydrostatics) (10) x 1000 ] (10) x 1000 ] (10) x 1000 ] (16) = (11)] (6) = (13) + (14)   + (14) + 0.9 (16) BEAM ydrostatics) drostatics) - (3)] / (18) ER = TCG (2) (19) X 1000]	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.78 = -0.78 = -0.78 = -0.50 = 3.41 = 3.83 = 39.60 = 8.12 = 50.55 = 5.08 = -0.01 = -0.01 = 3.40	l/or decrease deck rms and check KG AT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m From CL (- m (+Stbd)	<pre>cargo or take of again. IND TRANSON ) d) =</pre>	And Calculate A @ BOW an	Average Draf d TRANSOM Calculate _Drafts @ E	Port & Stb
(7) LCB (from Hy (8) MOMENT TO TRIM 1mm, MTmm (from Hy (9) KML (from Hy (10) MT1mm CORRECTED = MT1mm = (8) X [(5 (11) LCF (from Hy (12) TRIM LEVE (13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) X (15) MEAN DRAFT @ TRANSOM (16)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ] (17) MOMENT TO HEEL 1mm, MH1mm (from Hy (18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18) (20) HEEL LEVI (21) HEEL = [(4) X (20])/[ (22) DRAFT @ BOW = (14) +/- (21) / 2:	THE TRIM, F (6) LOA (drostatics) drostatics) (drostatics) (drostatics) (drostatics) (drostatics) (10) X 1000 ] (10) X 1000 ] (10) EEAM (16) BEAM (drostatics) (16) BEAM (drostatics) (17) (18) ER = TCG (2) (19) X 1000] STBD	Increase ballast and Correct Loading fo HEEL, AND DRAFTS = 62.40 = 30.76 = 12.34 = 118.71 = 10.38 = 31.85 = -0.78 = -0.78 = -0.78 = -0.78 = -0.78 = 3.41 = 2.91 = 3.83 = 39.60 = 8.12 = 50.55 = 5.08 = -0.01 = -0.01 = 3.40 = 2.91	l/or decrease deck rms and check KG AT THE BOW A m aft of FR( MT-m m ABL MT-m m aft of FR( m (+Aft/-Fw m ABL m ABL m ABL m ABL m ABL m ABL m from CL (- m (+Stbd) Port =	<pre>c cargo or take of again. IND TRANSON ) d) d) = 3.41 = 2.92</pre>	ner corrective . 1. Calculate A @ BOW an M ABL	Average Draf d TRANSOM Calculate _Drafts @ E	Port & Stb

				TANK LOADI	NG FORM					
Condition: FALCON DIAMOND	(5B) LOADED CO	NDITION AFLOA	AT, 709 MT VL + I	Η						
COLUMN →	0	1	2	3	4	5	6	7	8	9
	FILL	WEIGHT	LCG m a	ft of FR 0	TCG (m +/	/- from CL)	VCG (m abo	ve BASELINE)	TRANS FSM	LONG'L FSM
TANK	(%)	(MT)	LCG	L-MOM	TCG (+Stbd)	T-MOM	VCG	V-MOM	(MT-m)	(MT-m)
	Enter Value	Enter Value	Enter Value	Col 1 X Col 4	Enter Value	Col 1 X Col 6	Enter Value	Col 1 X Col 2	Enter Value	Enter Value
Ballast #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #3 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #4 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Ballast #4 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #1 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #1 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Port	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Zero Discharge #2 Stbd	0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Day Tank Port	25	2.69	24.00	64.60	-13.20	-35.53	2.67	7.20	2.00	2.00
Day Tank Stbd	25	2.69	24.00	64.60	13.20	35.53	2.67	7.20	2.00	2.00
Fuel Oil Port	25	32.02	22.80	730.04	-15.82	-506.45	0.74	23.64	161.00	61.00
Fuel Oil Stbd	25	32.02	22.80	730.04	15.82	506.45	0.74	23.64	161.00	61.00
Fresh Water Port	10	13.94	30.00	418.26	-15.57	-217.06	0.36	5.02	279.00	238.00
Fresh Water Stbd	42	58.56	30.00	1,756.70	16.02	938.03	0.77	45.24	279.00	238.00
Greywater	25	2.39	21.60	51.52	5.94	14.16	0.21	0.51	9.00	4.00
Dirty Oil	10	1.32	29.40	38.83	0.00	0.00	0.06	0.08	12.00	12.00
Lube Oil	25	1.73	25.80	44.71	0.90	1.56	0.15	0.26	2.00	6.00
Oily Water	25	1.90	25.80	49.14	-0.90	-1.71	0.15	0.29	2.00	7.00
TOTAL (Record here and on Vessel Loading Form)	0	149.26		3948.45		734.98		113.07	909.00	631.00

### INSTRUCTIONS FOR THE TANK LOADING FORM

For each of the vessel's tanks that contain liquid, determined and enter the following on the Tank Loading Form:

1. Take soundings of each tank and enter the liquid level in each tank in column 0 of the TANK LOADING FORM.

2. Consult the TANK CAPACITY TABLES and enter the weight of the liquid in column 1, the LCG of the liquid in column 2, the TCG of the liquid in column 4, and the VCG of the liquid in column 6 corresponding to the sounding. Enter the transverse and longitudinal free surface moments into columns 8 and 9, respectively. If the actual sounding falls between two soundings listed the TANK CAPACITY TABLES, enter the values associated with the higher of the two soundings on the TANK LOADING FORM.

3. Sum the weights in column 1 to obtain the total weight of the liquids in the tanks. Enter this TOTAL on the TANK LOADING FORM and the VESSEL LOADING FORM. 4. Multiply each weight in column 1 by its corresponding LCG in column 2 to obtain the longitudinal moment of the weight and enter this value in column 3. Sum the longitudinal moments in column 3 to obtain the total longitudinal moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

5. Multiply each weight in column 1 by its corresponding TCG in column 4 to obtain the transverse moment of the weight and enter this value in column 5. Sum the transverse moments in column 5 to obtain the total transverse moment of the liquids in the tanks. Note the starboard moments are positive and the port moments are negative. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

6. Multiply each weight in column 1 by its corresponding VCG in column 6 to obtain the vertical moment of the weight and enter this value in column 7. Sum the vertical moments in column 7 to obtain the total vertical moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

7. Individually sum the free surface moments in columns 8 and 9 to obtain the total transverse and longitudinal free surface moments of the internal tanks. Enter the maximum of these two TOTALS on the TANK LOADING FORM. Add this value to the DECK TANKS MAX FSM TOTAL from the DECK CARGO LOADING FORM and enter this value into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

### **Operating Manual** Doc No: 0722-010-005-C5

			DECK CARG	O LOADING	FORM					
Condition: FALCON DIAMOND - (5B) LO	ADED CONDI	TION AFLOAT,	709 MT VL +	Н						
COLUMN>	1	2	3	4	5	6	7	8	9	10
ITEM	WEIGHT	LCG (m a	ft of FR 0)	TCG (m +,	- from CL)	VCG above	MAIN DK	VCG (m ab	ove BL)	DECK TANKS
(Include deck tanks & contents as	(MT)	LCG	L-MOM	TCG (+ STBD)	T-MOM	MAIN DECK	to BL	VCG	V-MOM	MAX FSM
separate line items)	Enter Value	Enter Value	Col 1 x Col 2	Enter Value	Col 1 x Col 4	Enter Value		Col 6 + Col 7		(MT-m)
Deck Cargo	530.74	54.00	28659.96	4.00	2122.96	4.56	+ 4.6=	9.16	4861.58	
Agusta AW-139 Chopper	6.80	-12.43	-84.50	0.00	0.00	14	+ 4.6=	18.60	126.48	
							+ 4.6=			
							+ 4.6=		5	
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=	$\mathcal{O}$		
							+ 4.6=	1		
							+4.6=			
							+4.6=			
							+ 4.6=			
							+ 4.6=			
						$\mathbf{O}$	+ 4.6=			
					(		+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
			4	-			+ 4.6=			
TOTAL (Record here and on Vessel Loading Form)	537.54		28575.46		2122.96				4988.06	0.00

### INSTRUCTIONS FOR THE DE

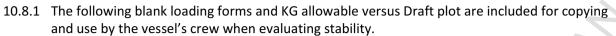
For each of material carried by the vessel the following shall be determined and entered on the Deck Cargo Loading Form: 1. A complete list of non-tank cargoes is to be entered above with weight, LCG, TCG, and VCG for each item in columns 1, 2, 4 and 6.

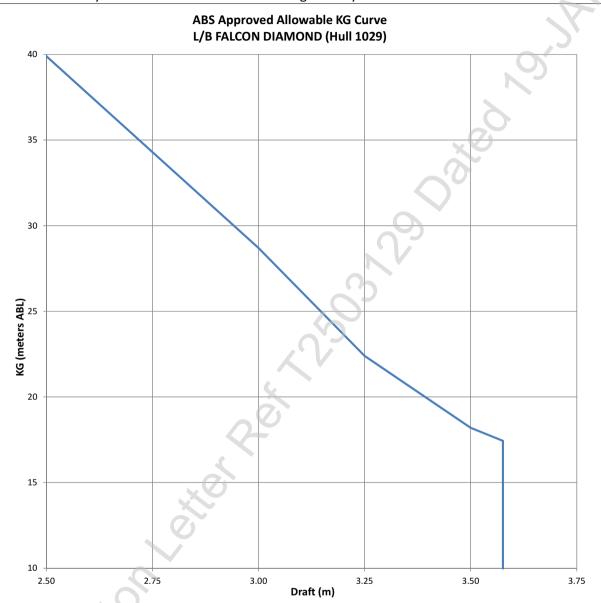
2.Cal culate the longitudinal moment for each cargo i tem by multiplying columns 1 and 2 for each i tem. Calculate the transverse moment for each cargo i tem by multiplying  $columns 1 and 4 for each item. \ Calculate the vertical moment for each cargo item by multiplying columns 1 and 8 for each item.$ 

3. Sum columns 1, 3, 5, and 9 and enter the values in the TOTAL row. These totals are to be entered in the Deck Cargo Loading row of the VESSEL LOADING FORM.

4. Sum column 10 and enter the value in the TOTAL row. This total is to be be added to the TANK LOADING FORM FSC MOM TOTAL and entered into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

### 10.8 Blank Example Forms and KG Allowable Curves





### Figure 10-3: ABS Allowable KG Curves

ALLOWABLE KG CURVE						
Displacement	DRAFT	KG <sub>A</sub>				
(MT)	(m)	(m)				
4941	2.50	39.9				
6173	3.00	28.7				
6792	3.25	22.4				
7413	3.50	18.2				
7602	3.576	17.44				

1/12/2024

### VESSEL LOADING FORM

Condition:							
COLUMN →	1	2	3	4	5	6	7
				TCG			
	WEIGHT	LCG	L-MOM	(m from CL,	T-Mom	VCG	V-MOM
Item	(MT)	(m aft FRO)	(MT-m)	+STBD)	(MT-m)	(m ABL)	(MT-m)
LIGHTSHIP							
LIGHTSHIP ADJUSTMENTS							
CREW, EFFECTS, & STORES							
OFFSHORE WORKERS, EFFECTS, & STORES							
TOTAL DECK CARGO (from DECK CARGO LOADING					.75		
FORM) TANK LIQUIDS IN VESSEL'S TANKS (from TANK							
LOADING FORM)							
TOTAL FSM OF ALL SLACK TANKS (from TANK LOADING							
FORM and DECK CARGO LOADING FORM)							
TOTALS:			C				
	Vessel	Loading Calculat	ions				
(1) LCG = (Total Col. 3 / Total Col. 1) =	<u></u>			m aft of FR	0		
(2) TCG = (Total Col. 5 / Total Col. 1) =				m from CL (-			
				-			
(3) KG = VCG = (Total Col. 7 / Total Col. 1) =				m ABL	NOTE: INCL	UDES FSE	
(4) DISPLACEMENT = Total			MT				
(5) MEAN SW WATER DRAFT (from Hydrostatic Pr	operties) =		m ABL				
		Correct Loading fo		-			
THE FOLLOWING OPTIONAL CALCULATIONS DETERMINE	THE TRIM, H	EEL, AND DRAFTS	AT THE BOW A	AND TRANSON	1.		
(7) LCD /frage 1	(6) LOA		m m = ft = f ED(				
(7) LCB (from H) (8) MOMENT TO TRIM 1mm, MTmm (from Hy			m aft of FRO MT-m				
(8) MOMENT TO TRIM IMM, MITHIN (1011 Hy (9) KML (from Hy			m ABL				
(10) MT1mm CORRECTED = MT1mm = (8) X [(9			MT-m				
(11) LCF (from H		=	m aft of FRO	b l			
Q			-	_	Calculate A	Average Dra	fts
(12) TRIM LEVE			m		@ BOW an	d TRANSOM	
(13) TRIM = [(4) X (12)] / [( (14) MEAN DRAFT @ BOW = (5) - (13) >			_ m (+Aft/-Fw m ABL				
	(6)	-	III ADL				
(15) MEAN DRAFT @ TRANSOM	. ,	=	m ABL				
(15A)* MEAN NAV. DRAFT @ FR 50 = (13) X [ 60 / 62.4 ]			m ABL				
6							
	(16) BEAM		m				
(17) MOMENT TO HEEL 1mm, MH1mm (from Hy			MT-m				
(18) KMT (from Hy (19) MH1mm CORRECTED = MH1mm = (17) X [(18)			m ABL MT-m			Calculate	Port & Stbd
(13) MATHINI CORRECTED - MATHINI - (17) X [(18) (20) HEEL LEV			m from CL (-	+Stbd)		Drafts @ I	
(21) HEEL = [(4) X (20)]/[			m (+Stbd)	,	۲ ۲	TRANSOM	
(22) DRAFT @ BOW = (14) +/- (21) / 2:	STBD		Port =		m ABL		
(22) DRAFT @ TRANSOM = (15) +/- (21) / 2:	STBD	=	Port =		m ABL		
(24) NAV. DRAFT @ FR 50 = (16) +/- (22) / 2:	STBD	=	PORT =	=	m ABL		
* STERN THRUSTER EXTENDS 0.87 m BELOW BASELINE,				G OF NO77LF			

C

1/12/2024

				TANK LOADI	NG FORM					
Condition:										
COLUMN →	0	1	2	3	4	5	6	7	8	9
	FILL	WEIGHT	LCG m a	ft of FR 0	TCG (m +,	/- from CL)	VCG (m abo	ve BASELINE)	TRANS FSM	LONG'L FSM
TANK	(%)	(MT)	LCG	L-MOM	TCG (+Stbd)	T-MOM	VCG	V-MOM	(MT-m)	(MT-m)
	Enter Value	Enter Value	Enter Value	Col 1 X Col 4	Enter Value	Col 1 X Col 6	Enter Value	Col 1 X Col 2	Enter Value	Enter Value
Ballast #1 Port										
Ballast #1 Stbd									$\sim$	
Ballast #2 Port										
Ballast #2 Stbd										
Ballast #3 Port								Ć		
Ballast #3 Stbd								0.		
Ballast #4 Port										
Ballast #4 Stbd										
Zero Discharge #1 Port										
Zero Discharge #1 Stbd										
Zero Discharge #2 Port										
Zero Discharge #2 Stbd										
Day Tank Port										
Day Tank Stbd										
Fuel Oil Port										
Fuel Oil Stbd					C					
Fresh Water Port						J				
Fresh Water Stbd										
Greywater										
Dirty Oil										
Lube Oil										
Oily Water					V					
TOTAL (Record here and on Vessel Loading Form)				8						

### INSTRUCTIONS FOR THE TANK LOADING FORM

For each of the vessel's tanks that contain liquid, determined and enter the following on the Tank Loading Form:

1. Take soundings of each tank and enter the liquid level in each tank in column 0 of the TANK LOADING FORM.

2. Consult the TANK CAPACITY TABLES and enter the weight of the liquid in column 1, the LCG of the liquid in column 2, the TCG of the liquid in column 4, and the VCG of the liquid in column 6 corresponding to the sounding. Enter the transverse and longitudinal free surface moments into columns 8 and 9, respectively. If the actual sounding falls between two soundings listed the TANK CAPACITY TABLES, enter the values associated with the higher of the two soundings on the TANK LOADING FORM.

3. Sum the weights in column 1 to obtain the total weight of the liquids in the tanks. Enter this TOTAL on the TANK LOADING FORM and the VESSEL LOADING FORM. 4. Multiply each weight in column 1 by its corresponding LCG in column 2 to obtain the longitudinal moment of the weight and enter this value in column 3. Sum the longitudinal moments in column 3 to obtain the total longitudinal moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

5. Multiply each weight in column 1 by its corresponding TCG in column 4 to obtain the transverse moment of the weight and enter this value in column 5. Sum the transverse moments in column 5 to obtain the total transverse moment of the liquids in the tanks. Note the starboard moments are positive and the port moments are negative. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

6. Multiply each weight in column 1 by its corresponding VCG in column 6 to obtain the vertical moment of the weight and enter this value in column 7. Sum the vertical moments in column 7 to obtain the total vertical moment of the liquids in the tanks. Enter this value on the TANK LOADING FORM and the VESSEL LOADING FORM.

7. Individually sum the free surface moments in columns 8 and 9 to obtain the total transverse and longitudinal free surface moments of the internal tanks. Enter the maximum of these two TOTALS on the TANK LOADING FORM. Add this value to the DECK TANKS MAX FSM TOTAL from the DECK CARGO LOADING FORM and enter this value into the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

### Operating Manual Doc No: 0722-010-005-C5

			DECK CARG	O LOADING	FORM					
ONDITION:										
COLUMN>	> 1	2	3	4	5	6	7	8	9	10
ITEM	WEIGHT	LCG (m a	ft of FR 0 )	TCG (m +/	′- from CL)	VCG above	MAIN DK	VCG (m abo	ove BL)	DECK TAN
(Include deck tanks & contents as	(MT)	LCG	L-MOM	TCG (+ STBD)	T-MOM	MAIN DECK	to BL	VCG	V-MOM	MAX FS
separate line items)	Enter Value	Enter Value	Col 1 x Col 2	Enter Value	Col 1 x Col 4	Enter Value		Col 6 + Col 7		(MT-m)
							+ 4.6=			
							+ 4.6=			
							+ 4.6=		9	
							+ 4.6=		P.	
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=	$\mathcal{O}$		
							+ 4.6=	1		
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
						$\mathbf{\mathbf{\nabla}}$	+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
					(h)		+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
							+ 4.6=			
			X				+ 4.6=			
							+ 4.6=			
TOTAL (Record here and on Vessel			h							
Loading Form)										

### INSTRUCTIONS FOR THE DECK CARGO LOADING FORM

For e ach of material carried by the vessel the following shall be determined and entered on the Deck Cargo Loading Form: 1. A complete list of non-tank cargoes is to be entered above with weight, LCG, TCG, and VCG for each item in columns 1, 2, 4 and 6.

2. Calculate the longitudinal moment for each cargo item by multiplying columns 1 and 2 for each item. Calculate the transverse moment for each cargo item by multiplying columns 1 and 4 for each item. Calculate the vertical moment for each cargo item by multiplying columns 1 and 8 for each item.

3. Sum columns 1, 3, 5, and 9 and enter the values in the TOTAL row. These totals are to be entered in the Deck Cargo Loading row of the VESSEL LOADING FORM.

4. Sum column 10 and enter the value in the TOTAL row. This total is to be be added to the TANK LOADING FORM FSC MOM TOTAL and entered in to the TOTAL FSM OF ALL SLACK TANKS row of the VESSEL LOADING FORM.

1/12/2024

### DECK TANK FSM CALCULATION WORKSHEET

CONDITION:				
Temporary Tank Description:				1
(1) Tank Dimensions: (2) Fluid Density:	(1a) L = D =	m t/m <sup>3</sup>	(1b) W = (2a) Fluid SG =	m t/m³
		• • •	) Fluid Density, D = (2a) x 1 t/m <sup>3</sup> =	t/m
	$W^{3} = (1b)^{3} =$	m³		
(4) Tank FSM = D x L x W <sup>3</sup> = (2	) x (1a) x (3) =	m-ton	Record here and on Deck Cargo	Loading Form

### Instructions for Deck Tank FSM Determination

1) When carrying temporary deck tanks, the weight of the empty tank and the liquid weights should be entered as separate line items on the Deck Cargo Loading Form. This worksheet aids in determining the FSM of common tank geometries to be entered in the appropriate column on the Deck Cargo Loading Form. 2) The maximum free surface moment of the temporary deck tank may be determined for rectangular or cylindrical tanks oriented as shown on the attached sketch, as follows:

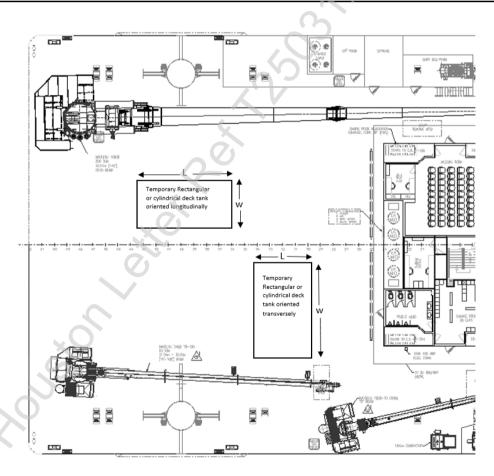
a) Determine L, the maximum longitudinal dimension of the tank. See the accompanying sketch. Enter this value on teh worksheet, line (1a).
b) Determine W, the maximum transverse dimension of the tank. See the accompanying sketch. Enter this value on teh worksheet, line (1b).

c) Determine D, the density of the liquid in the tank. This value is often provided as a specific gravity (SG). The density can be determined from the SG using the

calculations in lines (2a) and (2b). Enter the density, D, on the worksheet, line (2).

d) Cube the width dimension, W, and enter this value on the worksheet, line (3).

e) Determine the FSM using the calculation in line (4). Enter this value on the worksheet and on the Deck Cargo Loading Form.



MAIN DECK PLAN

1/12/2024

### EXAMPLE DECK TANK CALCULATION

D	ECK TANK FSM CALCU	LATION WC	DRKSHEET	
CONDITION: Example Temporary Tank				
Temporary Tank Description: 3m x 4m rec	tangular tank carrying	salt water		
(1) Tank Dimensions:	(1a) L = 3	m	(1b) W = 4	m
(2) Fluid Density:	D = 1.02500	t/m <sup>3</sup>	(2a) Fluid SG =	N
		(2	(b) Fluid Density, D = (2a) x 1 t/m <sup>3</sup> =	ton/m <sup>3</sup>
	(3) $W^3 = (1b)^3 = 64$	m³		
(4) Tank FSM = D x L x $W^3$ =	(2) x (1a) x (3) = 196.8	m-ton	Record here and on Deck Cargo Load	ding Form
			0	

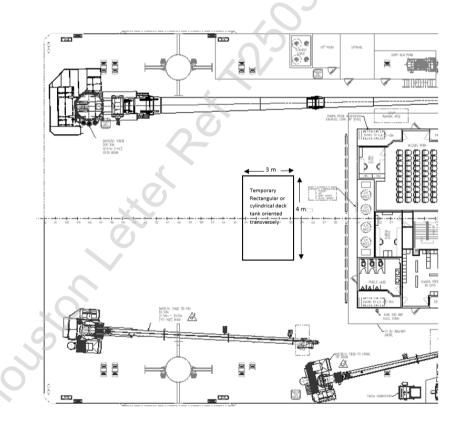
### Instructions for Deck Tank FSM Determination

1) When carrying temporary deck tanks, the weight of the empty tank and the liquid weights should be entered as separate line items on the Deck Cargo Loading Form. This worksheet aids in determining the FSM of common tank geometries to be entered in the appropriate column on the Deck Cargo Loading Form.
 The maximum free surface moment of the temporary deck tank may be determined for rectangular or cylindrical tanks oriented as shown on the attached sketch, as follows

a) Determine L, the maximum longitudinal dimension of the tank. See the accompanying sketch. Enter this value on teh worksheet, line (1a).
b) Determine W, the maximum transverse dimension of the tank. See the accompanying sketch. Enter this value on teh worksheet, line (1b).
c) Determine D, the density of the liquid in the tank. This value is often provided as a specific gravity (SG). The density can be determined from the SG using the

d) Cube the width dimension, W, and enter this value on the worksheet, line (2).
 d) Cube the width dimension, W, and enter this value on the worksheet, line (3).

e) Determine the FSM using the calculation in line (4). Enter this value on the worksheet and on the Deck Cargo Loading Form.



MAIN DECK PLAN

### 10.9 Downflooding Points

10.9.1 The following is a list of unprotected downflooding points. Where required, watertight closures are provided for doors and hatches and should be secured at all times. Air pipes (see drawing 0722-503-001 Vents Fills and Sounds (Appendix H) for locations and arrangements) and other such openings are protected by manual or automatic weathertight closures which are to be secured as required.

	X (m)	Y (m)	Z (m)	8
POINT	+ AFT of FP	+ Stbd OCL	+ABL	DESCRIPTION
*EXH	36.00	-18.75	10.72	ER Exhaust Stack
*INP	28.20	-4.20	9.10	ER Air Intake, Port Extent
*INS	28.20	4.20	9.10	ER Air Intake, Stbd Extent
*VENFP	25.20	-9.09	9.10	ER Exhaust Air, Forward Port
*VENAP	28.80	-9.09	9.10	ER Exhaust Air, Aft Port
*VENFS	25.20	9.09	9.10	ER Exhaust Air, Forward Stbd
*VENAS	28.80	9.09	9.10	ER Exhaust Air, Aft Stbd

ter Rei Vi

1/12/2024

### **11 Crane Capacity Tables**

All lifts shall comply with the following load charts, regulatory restrictions, latest API standards, and any crane manufacturer's specifications contained in the crane-specific operations manual. Cranes shall not be used unless the vessel is in the elevated condition.

# Nautilus Model 1000B-140

# 181.44 t max capacity

# 42.67 m Boom length

MiNO Marine, LLC

# Nautilus Model 340BT-70/100

# 54.43 t max capacity

# 21.34 m-30.48 m Boom length

# Nautilus Model 180B-70

# 22.68 t max capacity

21.34 m Fixed Boom

SON

### **12 Tank Sounding Tables**

12.1 Tank sounding tables are provided as Appendix A.

13.2 The sounding tables provide capacities; the vertical, longitudinal, and transverse centers of gravity for each 0.05 m interval of sounding as well as free surface data of each tank.

13.3 The sounding tables provide the capacities and center of gravity for each void. Each void is provided with permanently installed bilge suction, as seen in Appendix E.

# Houston Letter Ret 1200 200 Dates Agend **13 Location of Stored Dangerous Substances**

The vessel has no designated storage areas for dangerous substances.

### **14 General Arrangement**

Please See Appendix B for General Arrangement drawing.

Operating Manual Doc No: 0722-010-005-C5

### **15 Fire and Safety Plan**

15.1 The Fire Control Plan is provided in Appendix C.

This plan is located on the vessel in the following locations:

- 1. Meeting Room; 05 Level
- 2. Fwd Side of Stairtower Exterior; 04 Level
- 3. Fwd Side of Stairtower Exterior; 03 Level
- 4. Fwd Side of Stairtower Exterior; 02 Level
- 5. Forward End of Deckhouse Near CL; Foclse Deck
- 6. Near Change Room (Port side of Deckhouse) Door; Main Deck
- 7. Near aft side of stack; Main Deck
- 8. ECC; Hold Level
- 15.2 The Safety Plan is provided in Appendix D.

This plan is located on the vessel in the following locations:

- 1. Meeting Room; 05 Level
- 2. Fwd end of Mess Room; Main Deck
- 3. ECC; Hold Level
- 15.3 Inner Joiner Doors
- 15.3.1 Where inner joiner doors are provided in the same location as exterior watertight or weathertight doors, the joiner doors shall be locked open in normal operating conditions.

### **16** List of Shutdown Locations

### 16.1 Shutdown Appliance Table

Shutdown Appliance	E-Stop # (from H1028- 438-001-60)	Location	Equipment
	01	ECC Room near ER Door	MCC #1 (port) emergency shutdown shunt
Port Engine	03	Meeting Rm Mn Dk ER Door	trip, Port engine room supply
Room	07	Pilothouse Aft Console	fan #1 & #2 - damper control, Port engine room exhaust fan #1 & #2 - damper control,
	10	Pilothouse Forward Console	Port fuel suction valve shutdown
	02	ECC Room near ER Door	Mcc #2 (stbd) emergency shutdown shunt trip,
Stbd Engine	04	Change Room Outside ER Door	Stbd engine room supply fan #1 & #2 - damper control, Stbd engine room exhaust fan #1 & #2
Room	08	Pilothouse Aft Console	- damper control, Stbd fuel suction valve
	12	Pilothouse Forward Console	shutdown
Emorgonov	13	Pilothouse Aft Console	Emergency generator exhaust fan
Emergency Generator	14	Pilothouse Forward Console	Emergency generator exhaust fan, Emergency generator room intake damper
room	15	Main Deck House Wall Across from Egen Room	control
	05	Mess Outside Galley Door	P407 galley equipment emergency shutdown
	06	Passage Outside Pantry	shunt trip
Galley	Ansul Release Station	Galley Hood	Galley supply fan - damper control galley exhaust fan - damper control
	09	Pilothouse Aft Console	P202-10 FAMU shunt trip P209 220v central ventilation emergency
Central Ventilation	11	Pilothouse Forward Console	shutdown shunt trip, P408 480 central ventilation emergency shutdown shunt trip
Jacking System		Bridge Control Panel	Jacking System
Hose Reel HPU		Main Deck	Hose Reel HPU
Water Makers	× 0	Port Engine Room	Water Makers
Port Thruster	S	Pilothouse	Port Thruster
	5	ECC Room	
Starboard		Pilothouse	Starboard Thruster
Thruster		ECC Room	Starboard Thruster
Bow Thrustors		Pilothouse	Pow Thrustors (2)
Bow Thrusters		ECC Room	Bow Thrusters (2)

Port Main Generators (2)	Port Engine Room	Port Main Generators (2)
Stbd Main Generators (2)	Starboard Engine Room	Starboard Main Generators (2)
Emergency Generator	Emergency Generator Room	Emergency Generator
Fuel Oil	Main Deck Discharge	Fuel Oil Transfer Pump
Transfer	ECC Room Outside ER Door	

Table 16-1: Shutdown Appliance Locations

### 16.2 Guidance on Restarting after Shutdowns

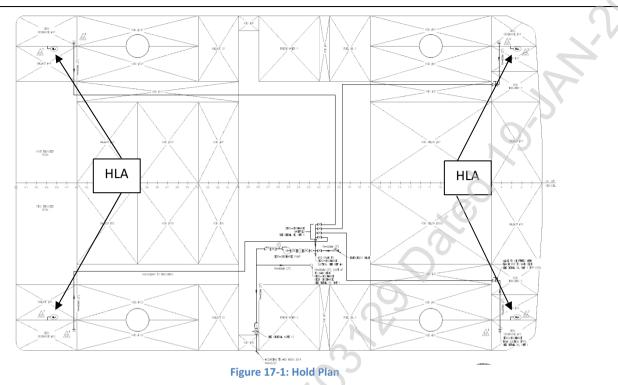
Low Contraction of the second second

16.2.1 After a shutdown, the cause of the shutdown shall be determined and corrected. After the causes of the shutdown and any equipment damage are corrected, the shutdown appliances shall be reset to their normal operation mode, and the affected equipment can be restarted using normal starting procedures.

### **17** Dewatering and Ballasting

### 17.1 General

- 17.1.1 The vessel is equipped with a bilge/ballast/fire system. See Appendix E for system diagram.
- 17.1.2 This system includes two 41.5 kW bilge/ballast/fire pumps, two submersible 58 kW ballast/fire pumps on hose reels for use while elevated, and one 3.5 kW zero discharge pump. The hull bilge and void suctions are routed through a bilge manifold, and each ballast tank uses a combined fill/discharge pipe routed through a ballast manifold. The manifold and pump start/stop controls are located in the engine rooms and the pilot house. In general, the engine room controls should be used when operating the system in the bilge and ballast mode. Each port and starboard engine room contains one bilge/ballast/fire pump and one bilge manifold and one ballast manifold corresponding to the tanks on that side of the vessel. The manifolds' suctions and discharges are cross connected between engine rooms. The zero discharge pump is located in the starboard engine room, and the two submersible pumps and hose reels are located on the 01 deck port side above the generator room, at frames 15 and 34.
- 17.1.3 The vessel is equipped with bilge high level alarms to sound when unexpected flooding occurs. The location of the flood alarms are indicated in Figure 17-1. Bilge sensors are also located in the all crane pedestals, thruster compartment P/S, engine room P/S and bow thruster compartment P/S.
- 17.1.4 All ballast operations are to be in accordance with the requirements of the Ballast Water Management Plan. Refer to MiNO Document 0916-841-002.



17.1.5 When afloat, one of the bilge/ballast/fire pumps shall be readily available for use as a fire pump at all times.

### 17.2 Bilge System Description & Operating Guidance

17.2.1 The engine rooms, bow thruster compartments, thruster compartments, HPU compartments, and below deck voids can be dewatered through the bilge manifold using one of the bilge/ballast/fire pumps. Each engine room also has an independent bilge suction that can be utilized independently of the bilge manifold.

Discharge of the bilge or void contents is directed to the overboard discharge, port or starboard, to the oily water bilge tank, or routed through the ballast manifold to a ballast tank for storage. To prevent accidental discharge of machinery space bilge water, the overboard discharge valves, port and starboard, shall be normally closed. No bilge contents from machinery spaces shall be discharged to any ballast tanks. The maximum flow rate for one bilge line to be discharged overboard is 73 m<sup>3</sup>/hr.

All machinery space bilges (including P&S engine rooms, P&S bow thruster compartments, P&S thruster compartments, and P&S HPU compartments) are to normally be discharged to the oily water tank. Bilge water from any machinery space is only to be discharged directly overboard only in the event of an emergency where there is immediate danger to the vessel. In the event that the un-treated bilge water from any machinery space is discharged directly overboard, such discharged is to be recorded in the vessels Oil Record Book as required by MARPOL Annex I (regulation 17). The contents of the oily water bilge tank shall be treated by the Oily Water Separator prior to discharging overboard. Machinery space bilges are to be pumped consistent with applicable regulatory pollution prevention regulations, MARPOL Annex I.

- 17.2.2 To prevent progressive flooding, the sliding watertight door between engine rooms must be closed. All other doors are normally closed with proper alarms and indication.
- 17.3 Ballast System Description and Operating Guidance
- 17.3.1 The ballast system can draw external water from the port and starboard seachests when afloat, or using the submersible ballast/fire pumps when elevated.
- 17.3.2 The ballast manifolds can be configured to draw suction from any ballast tank and discharge into any other ballast tank, overboard, or to the port deck discharge.

### **18** Propulsion Equipment Description

### 18.1 General

- 18.1.1 The vessel has a diesel electric power plant consisting of four (4) generators with two (2) in each engine room. The power management system determines the number and type of generators providing power to the system.
- 18.1.2 The propulsors consist of two (2) 360 degree azimuthing 1,566 kW Steerprop SP-20 D thrusters in the stern and two (2) 405 kW CAT (Berg) tunnel bow thrusters. The stern thrusters are located in the stern thruster compartments accessed via a passageway from the machinery room. The bow thrusters are located in the forward thruster compartments and are accessed via deck hatches. The drives for both motors are located in the ECC room. The bow thruster motors are located in the bow thruster compartments and the drives are located in the ECC room. All thrusters can be controlled from the pilothouse and from the ECC room in an emergency.
- 18.1.3 Please see Appendix G for the arrangement of the thrusters and associated equipment. Please see Appendix F for the electrical system schematics. Additional information may be found in information provided by vendors. See Table 18-1 below for a listing of the primary propulsion equipment.

Equipment	Vendor	Manufacturer	Model	Location
Main Gensets	Tractors Singapore	Caterpillar/KATO	CAT 3512C/	Port / Stbd
Main Gensets	Tractors Singapore		DSG86L1/4	Engine Room
Emergency Genset	Tractors Singapore	Caterpillar	CAT C9	Port Main Deck
Linergency Genset	Tractors Singapore	Caterpinar	CATES	Compartment
Stern Thruster Drives	RAACI Division Trident Marine Services	RAACI / Siemens	-	ECC Room
Stern Thruster Motors	Tractors Singapore	Marelli	B5J 500 LB4	Port / Stbd Thruster Room
Stern Thrusters	Tractors Singapore	Steerprop	SP-20 D	Port / Stbd Thruster Room
Bow Thruster Drives	RAACI, Inc.	RAACI / Siemens	-	ECC Room
Bow Thruster Motors	Tractors Singapore	Marelli	B4J 355 LB4	Port / Stbd Bow Thruster Compartment
Bow Thrusters	Tractors Singapore	CAT (Berg) Propulsion	BTT113	Port / Stbd Bow Thruster Compartment

Table 18-1:	Propulsion	Main	Equipment

٢.

### 18.2 Dynamic Positioning

- 18.2.1 This vessel is equipped with an integrated Dynamic Positioning system, class DP-2. The system integrates control of the thrusters and takes inputs from sensors to maintain the desired position/heading. The system features:
  - a. Two (2) x Operator Stations (Workstations)
  - b. Two (2) x 3-axis Joystick
  - c. Two (2) x Differential GPS Units
  - d. Three (3) x Wind Sensors w/ Display
  - e. Two (2) x Controller Cabinets
  - f. One (1) x Laser Reference System
  - g. Three (3) x Vertical Reference Units
  - h. One (1) x Duplex Changeover Switch
  - i. Three (3) x Gyro Compass Units
  - j. Two (2) x Printer
  - k. Two (2) x Uninterruptable Power Supply
- 18.2.2 Limiting Conditions are given in capability plots found in the DP system manual. The worst-case design scenario was given with a current of 2.5kts from 90 degrees with legs up, and legs down. Capability plots for each of these cases are shown below. See Reference [3] for DP Plots with other environmental conditions.

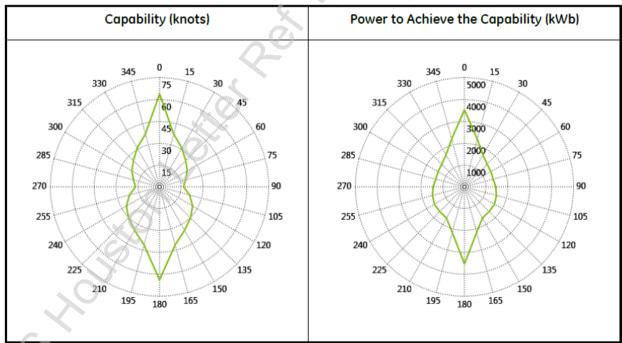
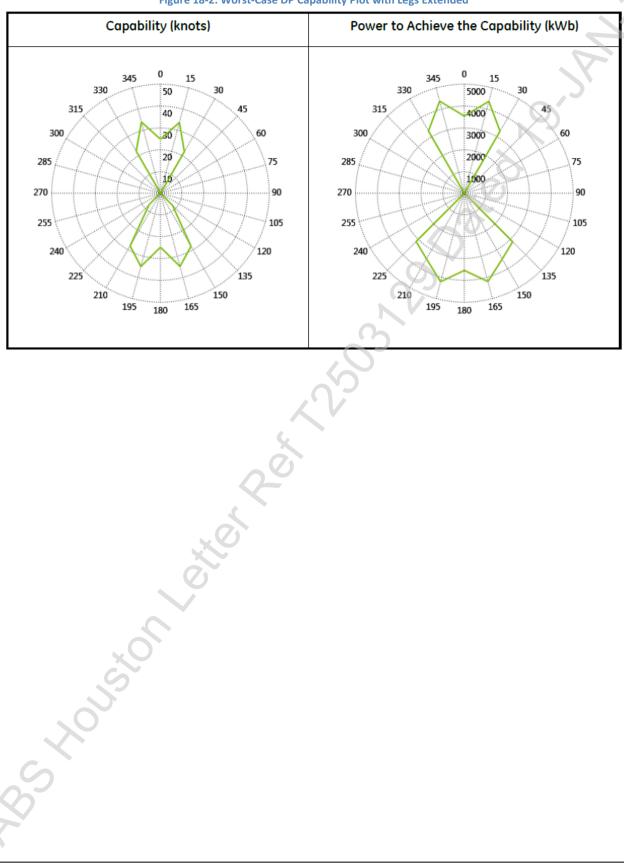


Figure 18-1: Worst-Case DP Capability Plot with Legs Retracted

### Operating Manual Doc No: 0722-010-005-C5



### Figure 18-2: Worst-Case DP Capability Plot with Legs Extended

### **19** Jacking System Description & Operation

### 19.1 General

- 19.1.1 The vessel's jacking system is electro-hydraulic and located in two rooms P&S on the hold deck. The port leg's gears are fed from the Hydraulic Power Units (HPU) located in the port jacking system room. The starboard legs are fed from the Hydraulic Power Units (HPU) located in the starboard jacking system room. The jacking control station is located in the pilothouse.
- 19.1.2 Each leg tower includes seventeen (17) Hydraquip CSI S60 liftboat planetary gearboxes.
- 19.1.3 Each jacking power unit consists of two (2) 300 HP electric motors driving hydraulic pumps.

Starboard FWD Leg Jacking System	0
STBD FWD Motor 1 Primary Circuit:	601-6
STBD FWD Motor 2 Primary Circuit:	602-6
(	<i>h</i>
	)
Port FWD Leg Jacking System	
PORT FWD Motor 1 Primary Circuit:	601-4
PORT FWD Motor 2 Primary Circuit:	602-4
0 C	
Starboard Aft Leg Jacking System	
STBD AFT Motor 1 Primary Circuit:	601-5
STBD AFT Motor 2 Primary Circuit:	602-5
Port Aft Leg Jacking System	
PORT AFT Motor 1 Primary Circuit:	601-3
PORT AFT Motor 2 Primary Circuit:	602-3

705

### **20** Helideck Operations

### 20.1 General

20.1.1 The vessel has a helideck cantilevered off the forecastle deck and transversely centered on the ship. This helideck can accommodate the helicopters listed in Table 20-1 as well as any helicopter with D-values and weights smaller than the maximums shown, subject to restrictions on maximum take-off weight depending on the mode of the vessel (elevated or afloat).

### 20.2 Maximum Take-Off Weight Restrictions

- 20.2.1 When elevated, the maximum take-off weight for a helicopter is: 12,600 kg
- 20.2.2 When afloat, the maximum take-off weight for a helicopter is: 11,000 kg

Турө	D-value (metres)	Perimeter 'D' marking	Rotor diameter (metres)	Max weight (kg)	′t′ valu∍
Bolkow Bo 105D	12.00	12	9.90	2400	2.4t
EC 135	12.10	12	10.20	2720	2.7t
Bolkow 117	13.00	13	11.00	3200	3.2t
Agusta A109	13.05	13	11.00	2600	2.6t
Dauphin SA 365N2	13.68	14	11.93	4250	4.3t
EC 155B1	14.30	14	12.60	4850	4.9t
Sikorsky S76	16.00	16	13.40	5307	5.3t
Agusta/Westland AW 139 <sup>1</sup>	16.66	17	13.80	6400	6.4t
Bell 412	17.13	17	14.02	5397	5.4t
Bell 212	17.46	17	14.63	5080	5.1t
Super Puma AS332L	18.70	19	15.00	8599	8.6t
Bell 214ST	18.95	19	15.85	7936	8.0t
Super Puma AS332L2	19.50	20	16.20	9300	9.3t
EC 225	19.50	20	16.20	11000	11.0t
Sikorsky S92 <sup>1</sup>	20.88	21	17.17	12020	12.0t
Sikorsky S61N	22.20	22	18.90	9298	9.3t

### Table 20-1: Typical Helicopter Dimensions

Maximum D-Value: 22.2 meters [72 feet]

Maximum Take-off Weight (Elevated): 12,600 kg [27,778.2 lbs]

Maximum Take-off Weight (Afloat): 11,000 kg [24,250.8 lbs]

### 20.3 Helideck Operations

- 20.3.1 Prior to any landing or take-off, the helideck perimeter lighting must be illuminated.
- 20.3.2 Additionally, while any helicopter operations are taking place the DIFF system pump must be activated to arm the deck integrated firefighting system required for helicopter operations.
- 20.3.3 The ship's rescue boat should be ready for immediate lowering.
- 20.3.4 There are no facilities onboard for helicopter refueling.
- 20.3.5 Helicopter arrival and departure procedures are to be consistent with the helicopter operator's preferences and practices. Refer to the ICS (International Chamber of Shipping) Guide to Helicopter/Ship Operations for recommendations on helicopter operating practices. The vessel's master shall be satisfied that the following conditions are satisfied prior to take-off or landing:
  - 20.3.5.1 Radio contact with the helicopter must be made prior to landing or take-off. Refer to the ICS Guide or helicopter operator's practices in the event radio contact is lost.
  - 20.3.5.2 An officer shall be on watch near the helideck DIFF system control panel during landings and takeoffs
- 20.3.6 If the helideck is used while the vessel is afloat, the following restrictions must be observed:
  - 20.3.6.1 Vessel forward speed should be 2.5 knots or as requested by helicopter pilot
  - 20.3.6.2 Wave heights shall not exceed 1.22m (4.0 feet) from any heading
  - 20.3.6.3 Wind speed shall be appropriate for helicopter take-off or landing but must not exceed70 knots under any circumstances
  - 20.3.6.4 Pitch, Roll, and Heavy Limitations can vary according to helicopter type. The vessel's master should check specific helicopter limits with the helicopter operator. As guidance, pitch, roll, and heave rate should be limited as shown in Table 20-2, reproduced from the Helideck Certification Agency (HCA) Helideck Limitations List (HLL)
     Part C. Limitations are given for a Category 1 helideck. The inclination limits refer to any initial list or trim of the vessel.

### **Operating Manual** Doc No: 0722-010-005-C5

		Table 20	0-2: Pitch,	Roll and H	leave Limitatio	ns		
A         DAY         ±3         3.5         1.3         5           Might         ±2         2.5         1.0         4           A         DAY         ±4         3.5         1.3         5           A         DAY         ±4         3.5         1.3         5           A         DAY         ±4         3.5         1.3         5           A         Night         ±2         2.5         1.0         4           Aircraft Categories         Might         ±3         2.5         1.0         4           A=         S92, EC225, AS332 Series, AW189         A=         A=         S92, EC25, AS335 Series, AW189           A=         EC145, EC155, EC175, AW169         EC145, EC155, EC175, AW169         EC145, EC155, EC175, AW169	Aircraft Cate	gory		H				
A         DAY         ±3         3.5         1.3         5           Night         ±2         2.5         1.0         4           B         DAY         ±4         3.5         1.3         5           A         Night         ±2         2.5         1.0         4           B         DAY         ±4         3.5         1.3         5           Aircraft Categories         -         -         -         -         -           A =         S92, EC225, AS332 Series, AW189         -         -         -         -           A =         S92, EC225, AS335 Series, B212, B412, EC135, B         -         -         -         -           B =         EC145, EC155, EC175, AW169         -         -         -         -		8 <i>1</i>	Pitch/Roll Inclination Heave H					
Night         ±2         2.5         1.0         4           B         DAY         ±4         3.5         1.3         5           Aircraft Categories         Night         ±3         2.5         1.0         4           A:         S92, EC225, AS332 Series, AW189         A         A         AM139, S76 series, AS365 Series, B212, B412, EC135, B =         EC145, EC155, EC175, AW169								
B         DAY         ±4         3.5         1.3         5           Aircraft Categories         A         S92, EC225, AS332 Series, AW189         A           A =         S92, EC225, AS332 Series, AW189         AW139, S75 series, AS365 Series, B212, B412, EC135, B         B           B =         EC145, EC155, EC175, AW169         AW130, S75 series, AS365 Series, B212, B412, EC135, B         B	Α	DA	λY	±3	3.5	1.3	5	
Night         ±3         2.5         1.0         4           A =         S92, EC225, AS332 Series, AW189         AW139, S76 series, AS365 Series, B212, B412, EC135, B =         EC145, EC155, EC175, AW169           B =         EC145, EC155, EC175, AW169         EC145, EC156, EC175, AW169         EC145, EC156, EC175, AW169				±2	2.5			
Aircraft Categories         A=           S92, EC225, AS332 Series, AW189         AW139, S76 series, BS12, B412, EC135, EC145, EC155, EC175, AW169           B =         EC145, EC155, EC175, AW169	В	1						
A = 592, EC225, AS332 Series, AW189 AW139, 576 series, AS365 Series, B212, B412, EC135, EC145, EC155, EC175, AW169			ght	±3	2.5	1.0	4	╡
AW139, 576 series, AS365 Series, B212, B412, EC135, EC145, EC135, EC175, AW169		1						-
B= EC145, EC155, EC175, AW169	A =					242 5442 5	C125	-
Rest outsion letter Rest Asian Contraction of the section of the s	R –					3212, B412, E	C135,	
Mino Marine, LLC Page							Done	
	MiNO Marine, LLC						Page	! <b>1</b>

### **21** Evacuating & Embarkation/Disembarkation Procedures

### 21.1 General

- 21.1.1 Primary and secondary escape routes leading to muster stations are indicated on the vessel Safety Plan (Appendix D).
- 21.1.2 When the vessel is afloat and experiences a situation in which the vessel needs to be evacuated

or abandoned, the following procedures will apply:

- 21.1.2.1 The Master will sound the abandon ship alarm over the vessel's general alarm bell and will inform the crew of the situation over the vessel's public address (PA) system.
- 21.1.2.2 The master will instruct crew members and persons in addition to crew to report to their assigned muster stations.
- 21.1.2.3 Once all onboard personnel are accounted for, the Master will then give instructions to the vessel crew to board the lifeboats or launch the life rafts.
- 21.1.2.4 If lifeboats are used to abandon ship, the vessel's crew will assist in the boarding of the lifeboats.
- 21.1.2.5 Once all persons have boarded the lifeboats, instructions will be given to launch the lifeboats.
- 21.1.2.6 If instructions are given to launch the life rafts, the vessel's crew will launch the life rafts and assist in the boarding of the life rafts.
- 21.1.3 When the vessel is elevated and experiences a situation in which the vessel needs to be

evacuated or abandoned, the following procedures will apply:

- 21.1.3.1 The Master will sound the abandon ship alarm over the vessel's general alarm bell and will inform the crew of the situation over the vessel's public address (PA) system.
- 21.1.3.2 The master will instruct crew members and persons in addition to crew to report to their assigned muster stations.
- 21.1.3.3 Once all onboard personnel are accounted for, the Master will then give instructions to evacuate to the offshore installation.
- 21.1.3.4 Once aboard the offshore installation, a head count will occur to account for all persons aboard.
- 21.1.3.5 In the event the vessel is in the elevated state and not adjacent to an offshore installation the procedure for evacuating/abandon ship while afloat will be utilized.
- 21.1.4 The following procedures must be followed when hoisting personnel:
  - 21.1.4.1 All cranes used to transfer personnel will have an operable anti two block device installed.
  - 21.1.4.2 All hooks used for support of personnel must have a closed safety latch.
  - 21.1.4.3 The load must be under control in both up and down directions.
  - 21.1.4.4 Those riding personnel baskets must wear Personal Floatation Devices.

- 21.1.4.5 When transferring personnel the operator should raise the personnel basket only high enough off the deck to clear all obstructions; swing the personnel basket over the water; raise or lower it in such a manner as to minimize swinging; position it slightly above the landing area; and gently lower it to the deck.
- 21.1.4.6 A loaded personnel carrier should only be raised or lowered over the water, minimizing the time suspended above a deck.
- 21.1.5 A listing of useful plans and schematics for emergency situations is as follows:
  - 1. 0722-801-001 General Arrangement
  - 2. 0722-831-001-Fire Control Plan
  - 3. 0722-831-002-Fire Boundary Plan
  - 4. 0722-832-001-Safety Plan
  - 5. 0722-833-001-Damage Control Plan
  - 6. 0722-521-001-Firemain System
  - 7. 0722-529-001-Bilge System
  - 8. 0722-092-001-Emergency Towing Procedure
  - 9. H1028-438-001-60-Emergency Shutdowns

### **22 Alarms and Monitoring**

### 22.1 Fire Alarm

- 22.1.1 The vessel is equipped with a fire alarm system utilizing addressable call points and an audible and visual alarm.
- 22.1.2 The fire alarm is a continuous siren with flashing strobe light with alarm stations distributed throughout the ship, including in each cabin.

### 22.2 General Alarm

- 22.2.1 The vessel is equipped with a general alarm system activated from the pilothouse, utilizing an audible alarm.
- 22.2.2 The general alarm plays an alarm tone through the same siren as the fire alarm, but in the pattern of 7 short tones followed by 1 long.

### 22.3 Abandon Ship Alarm

22.3.1 The abandon ship alarm plays an alarm tone through the same siren as the fire alarm, but in the pattern of 1 short tone followed by 1 long.

### **23** Exemption Requests

Several letters documenting interpretations in the 2009 IMO MODU were presented to the International Registries Technical Branch regarding the M300-4 Liftboat (Triyards SSY Hulls 1028/1029). These letters and responses are included in the following Appendices:

### Appendix K: Letter to the Marshall Islands 0722-MI-001 and Response

This letter is submitted to introduce a newbuild vessel project and explore any existing precedent for interpretations of operational service limitations (that is, an interpretation of "normal operating conditions" for offshore service with regards to design wind speeds as) beyond those explicitly enumerated in the IMO MODU Code for a vessel built to the Code and flagged with the Republic of the Marshall Islands (RMI).

### Appendix L: Letter to the Marshall Islands 0722-MI-002 and Response

The letter was submitted to request approval for limited dispensations from the access opening size requirements per the IMO MODU Code Section 2.2.4.

### Appendix M: Letter to the Marshall Islands 0722-MI-003 and Response

The letter was submitted to request approval for further limited dispensations from the access opening size requirements per the IMO MODU Code Section 2.2.4.

### Appendix N: Letter to the Marshall Islands 0722-MI-004 and Response

This letter is submitted to request approval for exemption from having a handrail support (bracket/stay) at every third stanchion on removable type handrails per the IMO Load Line Convention LL47.

### Appendix O: Letter to the Marshall Islands 0722-MI-006 and Response

The letter was submitted to request approval for further limited dispensations from the access opening size requirements per the IMO MODU Code Section 2.2.4.

### 24 Lightship Monitoring Procedure and Record

### 24.1 General

- 24.1.1 A record of all changes to machinery, structure, outfitting and equipment that affect the lightship data should be maintained in the operating manual or in a lightship data alterations log and be taken into account in daily operations.
- 24.1.2 Lightship is the weight of the vessel complete in all respects, but does not include consumables, stores, cargo, crew and their effects. It does not include any liquids onboard expect machinery fluids, such as lubricants and hydraulics, at operating levels.
- 24.1.3 Changes in lightship must be tracked and the vessel re-inclined if the weight change exceeds 1% of the lightship at the time of incline. If a weight is added please enter the changes in the lightship log below. These values will then be entered as line items in the stability and elevated loading forms. If a weight is removed please use a negative number in the weight column. If the changes include many individual items, please use a copy of the blank form provided in Section 24.1.5 to consolidate the items.

Date	Item No.	Description	Weight (MT)	LCG (m aft F0)	TCG (m +Stbd)	VCG (m ABL)
	1	Helideck drain tank structure	1.345	-1.85	-3.595	9.64
	2	FW pump foundation	0.018	27.205	12.19	1.555
	3	Kingpost foundation ONLY	1	55.2	19.8	15.35
	4	RO unit sub pump foundation and pump locking	0.932	18.16	-18.615	7.65
	5	Louver coaming modification	0.143	20.39	-16.48	6.13
	6	Gearbox access ladder	1.58	30.6	0	8.3
	7	Helideck drain tank foundation	0.764	-1.85	-3.595	7.65
	8	Signal mast modification	0.085	19.23	0	27.78
	9	Superstructure reinforcement	0.219	28.8	0	5.3
	10	Access ladder for accomm. vent flaps	1.816	17.26	0.2	15.2
	11	TV antenna foundation	0.023	21	-4.2	25.21
	12	AUX seawater system	0.784	19.17	-12.35	3.1
	13	FW transfer pump	0.068	26.9	14.58	2.9
	14	Helideck drain piping	1.41	-8.9	-3.8	14.16
	15	FW pump line	0.02	29.451	10.72	2.9
	16	RO unit sub pump line	0.03	18.54	-14.4	2.69
	17	FW pump	0.094	27.205	12.19	1.947
	18	RO unit sub pump	1.627	17.84	-19.09	8.64
	19	2 Gearboxes FWD (P&S)	2	13.5	0	<del>11</del> 8.15
	20	2 Gearboxes AFT (P&S)	2	49	0	<del>11</del> 8.15

24.1.4	Please inform Seaco	r Marine. Inc	of all change	s to the lights	ship weight.
	i lease inform seace		i or an onange		

	(7s)			ىلە
Table 24-1:	Light ship	data	alterations log	Ť

- 24.1.5 Light Ship Alterations Survey Form:
- 24.1.6 The following form is useful for consolidating several lightship changes that occurred at the same time into one log entry in the operations manual. The item number listed on this form should match the item number it is used to consolidate in the light ship log. This form should be kept with the operations manual for record keeping. If an item is removed from the vessel that is considered lightship weight, use a negative weight in column one.

Item Number: Date:		vessel'	s lightship	• Table 24-1 h • characterist • onsidered ligh	ics. Items	19 and 20 i	n Table
Prepared By:			Loading F		itsiiip auju		ule
Column Number	1	2	3	4	5	6	7
Description	Weight (MT)	LCG (m aft FP)	LMom (MT-m)	TCG (m from CL, +STBD)	TMom (MT-m)	VCG (m ABL)	VMom (MT-m)

### **Operating Manual** Doc No: 0722-010-005-C5

				7	
			2		
			0		
		5			
Total (sum)					

Lightship Adjustment	Value	Units
Weight = Total Col 1.	0.5	MT
LCG = (Total Col 3. / Total Col 1.)	XV	m aft FP
TCG = (Total Col 5. / Total Col 1.)		m from CL, + STBD
VCG = (Total Col 7. / Total Col 1.)		m ABL

JU MIND Marine, " Enter the results in the above cells into the Lightship data log in the operations manual.

Table 24-2: Light Ship Alterations Survey Form

### 25 Additional Entry Requirements for Tanks with Special Access Openings

### 25.1 General

- 25.1.1 Vessel crew and other personnel should observe confined space entry practices when entering any tank, void, or similar compartment onboard the vessel.
- 25.1.2 Several compartments with special access openings are present throughout the vessel. The access openings into these compartments satisfy IMO MODU code requirements, but due to the nature of compartment structure, some interior openings are smaller. The Republic of the Marshall Islands has authorized exemption of these smaller openings from the MODU Code requirements. However, special care should be taken to minimize the risks to persons required to enter these tanks.

The compartments with special access openings include (indicated in Figure 25-1 and 25-2).

- Double Bottom Tanks below engine room and public spaces
- Voids in way of leg tower foundations
- Structure in way of 200t (1000B) crane foundation

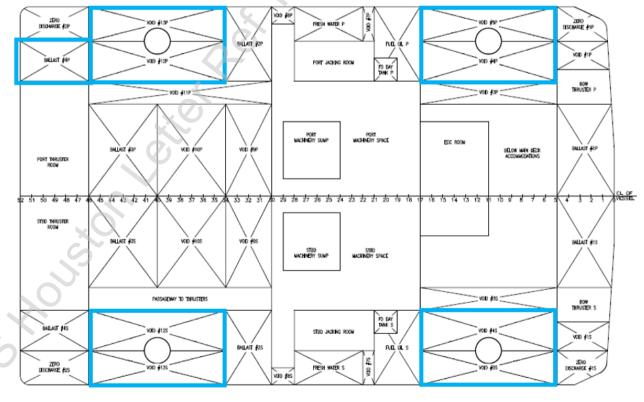


Figure 25-1: Hold Plan

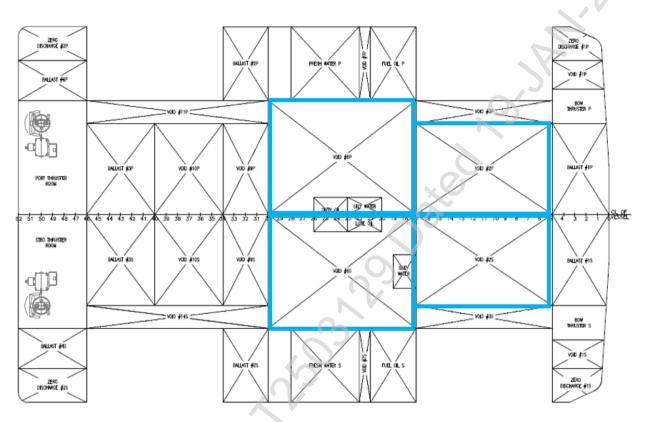


Figure 25-2: Double Bottom Plan

- 25.1.3 Access in these areas is only permitted for authorized entrants with an attendant present.Tanks and voids should not be entered without the Master's approval.
- 25.1.4 Prior to entry to any tank, both manholes are to be fully opened (small double bottom tanks have only one manhole). Forced ventilation by means of blower or other powered equipment is to be used to bring fresh air into the space.
- 25.1.5 A chemist or other qualified person should ensure that the tank is gas-free and has as safe atmosphere prior to entry.
- 25.1.6 An authorized entrant is required to:
  - 1. Know space hazards, including information on the means of exposure such as inhalation or dermal absorption, signs of symptoms and consequences of the exposure
  - 2. Use appropriate personal protective equipment properly
  - 3. Maintain communication with attendants as necessary to enable them to monitor the entrant's status and alert the entrant to evacuate when necessary;

- 4. Alert the attendant when a prohibited condition exists or when warning signs or symptoms of exposure exist.
- 25.1.7 An attendant is required to:
  - 1. Remain outside the permit space during entry operations unless relieved by another authorized attendant
  - 2. Maintain communication with and keep an accurate account of those workers entering the permit space
  - 3. Summon rescue and other services during an emergency

1/12/2024

### Index

### Α

afloat, 15, 16, 19, 23, 24, 33, 35, 38, 39, 41, 51, 84, 85 Allowable VCG, 42, 46

### В

ballast, 24, 31, 32, 33, 41, 83, 84, 85 bilge, 83, 84 bow thruster, 84 bulkheads, 41

### С

captain, 15, 16 cargo, 23, 26, 38, 41, 42, 44, 45 corrective action, 23, 32, 33, 38, 41 crane, 68 cranes, 23, 33, 36, 38, 41 Crew, Effects, and Stores, 25, 44 Current, 19

### D

damage, 36, 39, 82 dangerous substances, 78 deck cargo, 6, 13, 26, 33, 36, 38, 41, 43, 45, 46 Deck cargo, 13 displacement, 6, 13, 40, 42, 44, 45 draft, 7, 13, 15, 39, 40, 42, 45, 46

### Ε

emergency, 16, 38, 39 engine room, 41, 83, 84

### F

J

flooding, 13, 38, 39, 41, 83 FORM, 25, 26, 42, 43, 44, 45, 46 free surface moment, 43, 44

Inclining Experiment, 41

Jacking, 24, 31, 33

### L

LCG, 6, 32, 42, 43, 44 leg strength, 20 list, 38, 41, 42 load charts, 68 loading conditions, 13, 38, 46, 51 loadline, 40 Loadline, 10, 15, 40

Master, 13, 24, 31, 33, 35, 38, 40, 41, 42

### Ρ

S

safe refuge, 17, 35, 36, 39, 40 sea state, 35 shutdown, 82 Soil, 20 Stability, 24, 38, 40, 42, 43 Storm, 17 Survival, 17

pump, 31, 83,

### Т

tank, 26, 41, 42, 43, 44, 45, 83, 84, 85 tanks, 24, 38, 39, 41, 42, 43, 44, 45 TCG, 7, 25, 26, 32, 42, 43, 44, 45 Temperature, 19 trim, 32, 33, 38, 41, 42, 46

### U

USCG, 14, 23, 38

### V

variable load, 6, 10, 17 VCG, 6, 7, 42, 43, 44, 46, 51 voids, 38, 39, 41, 84

### W

water depth, 10, 35 wave, 10, 15, 17, 23, 24, 31, 35, 36, 38 weather, 13, 15, 33, 35, 36, 37, 40